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STORMWATER DETENTION ANALYSIS  
PREPARED BY: BAX ENGINEERING CO., INC.

INDIAN SPRINGS SUBDIVISION - O'FALLON  
BAX PROJECT NO. 97-8861  
MARCH 11, 1997 - REVISED MARCH 14, 1997

**INTRODUCTION:**

The tract of land is presently an undeveloped site located in the City of O'Fallon, Missouri. It is proposed that the tract, consisting of 44.69 acres, be developed into a residential subdivision. The site can be divided into three watersheds which drain to the North, South and West. Two dry stormwater detention basins will be constructed for the North and West watersheds and a lake will be constructed for the South watershed. These basins will provide detention for the development when considering the increased runoff for the site as required by the City of O'Fallon. The storage volume and outflow rates will be proportioned to insure that the peak rate of runoff leaving each watershed under post-developed conditions is less than or equal to the peak rate of runoff under pre-developed conditions for the required design storms. The basins have been analyzed for the 2, 5, 15, and 25 year frequency - 20 minute duration design storm and checked for safe passage of the 100 year frequency - 20 minute design storm.

**GENERAL SITE DATA AND RUNOFF CALCULATIONS:**

The pre-developed P.I. factors to be used for the analysis are:  
20 minute storms cfs/ac. (assumed 5% impervious):

2 year	1.15
5 year	1.41
15 year	1.87
25 year	2.31

The post-developed P.I. factors to be used for the analysis are:  
20 minute storms cfs/ac. (residential on-site and off-site):

2 year	1.61
5 year	1.98
15 year	2.64
25 year	3.26
100 year	4.17

BAX ENGINEERING CO., INC.  
1052 South Cloverleaf Drive  
St. Peters, MO 63376-6445  
314-928-5552 FAX 928-1718



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TIME OF CONCENTRATION:

**North** Of the inflows to the north basin, the most remote point of origin lies to the north. It will flow approximately 900 feet overland to the basin. Time of concentration is estimated as follows:

T(overland) : L = 900 feet  
Elevation difference = 628 - 604 = 24 feet  
T(overland) = 12 minutes : See figure 1  
Total time = 12.0 use 12 minutes.

**South** Of the inflows to the south basin, the most remote point of origin lies to the northwest near Treaty Ct. It will flow approximately 200 feet overland to an area-inlet then an additional 700 feet via the storm sewer to the detention basin. Time of concentration is estimated as follows:

T(overland) : L = 200 feet  
Elevation difference = 626 - 620 = 6 feet  
T(overland) = 3.4 minutes : See figure 1  
T(stormpipe) : L = 700 feet  
Estimated velocity 7 feet/second  
T(stormpipe) = 700 feet / 7 feet/sec.  
= 100 sec. >> 1.7 minutes  
Total time = 5.1 use 5 minutes.

**West** Of the inflows to the west basin, the most remote point of origin lies to the northwest approximately 300 feet west of Gray Wolf Dr. It will flow approximately 200 feet overland to an area-inlet then an additional 700 feet via the storm sewer to the detention basin. Time of concentration is estimated as follows:

T(overland) : L = 200 feet  
Elevation difference = 638 - 635 = 3 feet  
T(overland) = 4.6 minutes : See figure 1  
T(stormpipe) : L = 700 feet  
Estimated velocity 7 feet/second  
T(stormpipe) = 700 feet / 7 feet/sec.  
= 100 sec. >> 1.7 minutes  
Total time = 6.3 use 6 minutes.



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**BASIN PEAK INFLOW:**

Inflows to the basin have been estimated from the drainage area map of the project. (see construction plans)

**North**

<u>Storm</u>	<u>PI</u> <u>cfs/ac</u>	<u>On-site</u> <u>40% imp.</u> <u>17.37 ac</u> <u>cfs</u>	<u>Off-site</u> <u>40% imp.</u> <u>11.98 ac</u> <u>cfs</u>	<u>Total</u> <u>cfs</u>
2	1.61	27.97	19.29	47.25
5	1.98	34.39	23.72	58.11
15	2.64	45.86	31.63	77.48
25	3.26	56.62	39.05	95.68
100	4.17	72.43	49.96	122.39

**South**

<u>Storm</u>	<u>PI</u> <u>cfs/ac</u>	<u>On-site</u> <u>40% imp.</u> <u>14.29 ac</u> <u>cfs</u>	<u>Off-site</u> <u>40% imp.</u> <u>4.40 ac</u> <u>cfs</u>	<u>Total</u> <u>cfs</u>
2	1.61	23.01	7.08	30.09
5	1.98	28.29	8.72	37.01
15	2.64	37.73	11.62	49.34
25	3.26	46.59	14.34	60.93
100	4.17	59.60	18.35	77.94

**West**

<u>Storm</u>	<u>PI</u> <u>cfs/ac</u>	<u>On-site</u> <u>40% imp.</u> <u>6.03 ac</u> <u>cfs</u>	<u>Off-site</u> <u>40% imp.</u> <u>0.36 ac</u> <u>cfs</u>	<u>Total</u> <u>cfs</u>
2	1.61	9.71	0.58	10.29
5	1.98	11.94	0.71	12.65
15	2.64	15.92	0.95	16.87
25	3.26	19.66	1.17	20.83
100	4.17	25.15	1.50	26.65





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REQUIRED ATTENUATION: 20 minute storms  
(see attached pre and post-developed site drainage maps)

North

<u>Storm</u>	Post Dev. <u>Ac.</u>	x	Post Dev. <u>PI</u>	-	Pre Dev. <u>Ac.</u>	x	Pre Dev. <u>PI</u>		
2	17.56		1.61		16.32		1.15	=	9.50 cfs
5	17.56		1.98		16.32		1.41	=	11.76 cfs
15	17.56		2.64		16.32		1.87	=	15.84 cfs
25	17.56		3.26		16.32		2.31	=	19.55 cfs

South

<u>Storm</u>	Post Dev. <u>Ac.</u>	x	Post Dev. <u>PI</u>	-	Pre Dev. <u>Ac.</u>	x	Pre Dev. <u>PI</u>		
2	19.05		1.61		19.84		1.15	=	7.85 cfs
5	19.05		1.98		19.84		1.41	=	9.75 cfs
15	19.05		2.64		19.84		1.87	=	13.19 cfs
25	19.05		3.26		19.84		2.31	=	16.27 cfs

West

<u>Storm</u>	Post Dev. <u>Ac.</u>	x	Post Dev. <u>PI</u>	-	Pre Dev. <u>Ac.</u>	x	Pre Dev. <u>PI</u>		
2	8.07		1.61		8.53		1.15	=	3.18 cfs
5	8.07		1.98		8.53		1.41	=	3.95 cfs
15	8.07		2.64		8.53		1.87	=	5.35 cfs
25	8.07		3.26		8.53		2.31	=	6.60 cfs



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PERMITTED RELEASE RATE:

The permitted release rate of the basin is found by subtracting the required attenuation from the peak inflow to the basin for the design storm. Inflows to the basin have been estimated from the drainage area map of the project.

North

<u>Storm</u>	<u>Peak Inflow cfs</u>	-	<u>Required Attenuation cfs</u>	=	
2	47.25		9.50	=	37.75 cfs
5	58.11		11.76	=	46.35 cfs
15	77.48		15.84	=	61.64 cfs
25	95.68		19.55	=	76.13 cfs

South

<u>Storm</u>	<u>Peak Inflow cfs</u>	-	<u>Required Attenuation cfs</u>	=	
2	30.09		7.85	=	22.24 cfs
5	37.01		9.75	=	27.26 cfs
15	49.34		13.19	=	36.15 cfs
25	60.93		16.27	=	44.66 cfs

West

<u>Storm</u>	<u>Peak Inflow cfs</u>	-	<u>Required Attenuation cfs</u>	=	
2	10.29		3.18	=	7.11 cfs
5	12.65		3.95	=	8.70 cfs
15	16.87		5.35	=	11.52 cfs
25	20.83		6.60	=	14.23 cfs



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### STORM ROUTING CALCULATIONS AND RESULTS:

A computer program, PONDPACK, was used in routing the 20-minute design storms through the basin. As found in the routing calculations, the results are as follows:

#### North

<u>20 MIN STORM</u>	<u>PERMITTED RELEASE RATE</u>	<u>CALCULATED RELEASE RATE</u>	<u>PEAK ELEVATION</u>
2	37.75 cfs	37.03 cfs	602.79
5	46.35 cfs	44.56 cfs	603.09
15	61.64 cfs	57.54 cfs	603.57
25	76.13 cfs	67.20 cfs	603.96

#### South

<u>20 MIN STORM</u>	<u>PERMITTED RELEASE RATE</u>	<u>CALCULATED RELEASE RATE</u>	<u>PEAK ELEVATION</u>
2	22.24 cfs	16.26 cfs	593.43
5	27.26 cfs	22.20 cfs	593.65
15	36.15 cfs	32.84 cfs	593.99
25	44.66 cfs	43.04 cfs	594.29

#### West

<u>20 MIN STORM</u>	<u>PERMITTED RELEASE RATE</u>	<u>CALCULATED RELEASE RATE</u>	<u>PEAK ELEVATION</u>
2	7.11 cfs	4.12 cfs	613.44
5	8.70 cfs	4.48 cfs	613.97
15	11.52 cfs	5.01 cfs	614.83
25	14.23 cfs	5.37 cfs	615.55

As shown above, the calculated release rates are less than the permitted release rates as required for the detention basins.



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## CHECK 100-YEAR OUTFLOW

### North

$$\text{Wier Flow: } Q = C \times L \times H^{(3/2)}$$

where: 100 yr	Q =	122.39 cfs
	C =	3.0
	L =	15.7 ft
	H =	1.89 ft

overflow sill =	604.00
100-yr h/w =	605.89

### South

$$\text{Wier Flow: } Q = C \times L \times H^{(3/2)}$$

where: 100 yr	Q =	77.94 cfs
	C =	3.0
	L =	20.0 ft
	H =	1.19 ft

overflow sill =	594.50
100-yr h/w =	595.69

### West

$$\text{Wier Flow: } Q = C \times L \times H^{(3/2)}$$

where: 100 yr	Q =	26.65 cfs
	C =	3.0
	L =	11.7 ft
	H =	0.83 ft

overflow sill =	616.00
100-yr h/w =	616.83



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**SUMMARY**

**North - "OS LL"**

2 year-20min H.W.	602.79 ft.
5 year-20min H.W.	603.09 ft.
15 year-20min H.W.	603.57 ft.
25 year-20min H.W.	603.96 ft.
100 year-20min H.W. (low flow blocked)	605.89 ft.
LOW-FLOW OUTLET 1	48" WIDE x 19" HIGH
LOW-FLOW SILL ELEVATION	601.75 ft.
LOW-FLOW OUTLET 2	40" WIDE x 12" HIGH
LOW-FLOW SILL ELEVATION	600.00 ft.
OVERFLOW SILL ELEVATION (60" standpipe)	604.00 ft.
TOP OF BERM	607.00 ft.

**South - "OS B"**

2 year-20min H.W.	593.43 ft.
5 year-20min H.W.	593.65 ft.
15 year-20min H.W.	593.99 ft.
25 year-20min H.W.	594.29 ft.
100 year-20min H.W. (low flow blocked)	595.69 ft.
LOW-FLOW OUTLET	72" WIDE x 24" HIGH
LOW-FLOW SILL ELEVATION (Normal Pool)	592.50 ft.
OVERFLOW SILL ELEVATION	594.50 ft.
TOP OF BERM	597.00 ft.

**West - "OS W"**

2 year-20min H.W.	613.44 ft.
5 year-20min H.W.	613.97 ft.
15 year-20min H.W.	614.83 ft.
25 year-20min H.W.	615.55 ft.
100 year-20min H.W. (low flow blocked)	616.83 ft.
LOW-FLOW OUTLET	6" WIDE x 12" HIGH
LOW-FLOW SILL ELEVATION	610.00 ft.
OVERFLOW SILL ELEVATION (standard A.I.)	616.00 ft.
TOP OF BERM	618.00 ft.





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Additional cap.  
needed is provided  
in the rest of the  
basin

SEDIMENT STORAGE CALCULATIONS  
INDIAN SPRINGS - SOUTH BASIN  
BAX PROJECT NO. 96-8861  
APRIL 11, 1997

Sediment storage will be provided by over excavation of the lake bottom. The following calculations are based on an attached nomograph provided by the City of O'Fallon.

Total disturbed area tributary to lake: 14.29 AC.  
Rational Method "C" Factor: 0.40%

FROM FIGURE 1:

The required volume for 5 year construction period:

$$5 \times \overset{165}{118} \text{ Cu.Ft./Ac.} \times 14.29 \text{ Ac.} = 8,430 \text{ Cu.Ft.} \\ = 11,789$$

Volume Calculation:

ELEVATION	AREA	VOLUME	TOTAL VOLUME
586.0	9,195 s.f.	0 c.f.	0 c.f.
585.0	8,010 s.f.	8,603 c.f.	8,603 c.f.

Based on the above calculations the lake will be required to be over-excavated 1.00' (8,603 c.f.) to provide storage for the anticipated sediment run-off.

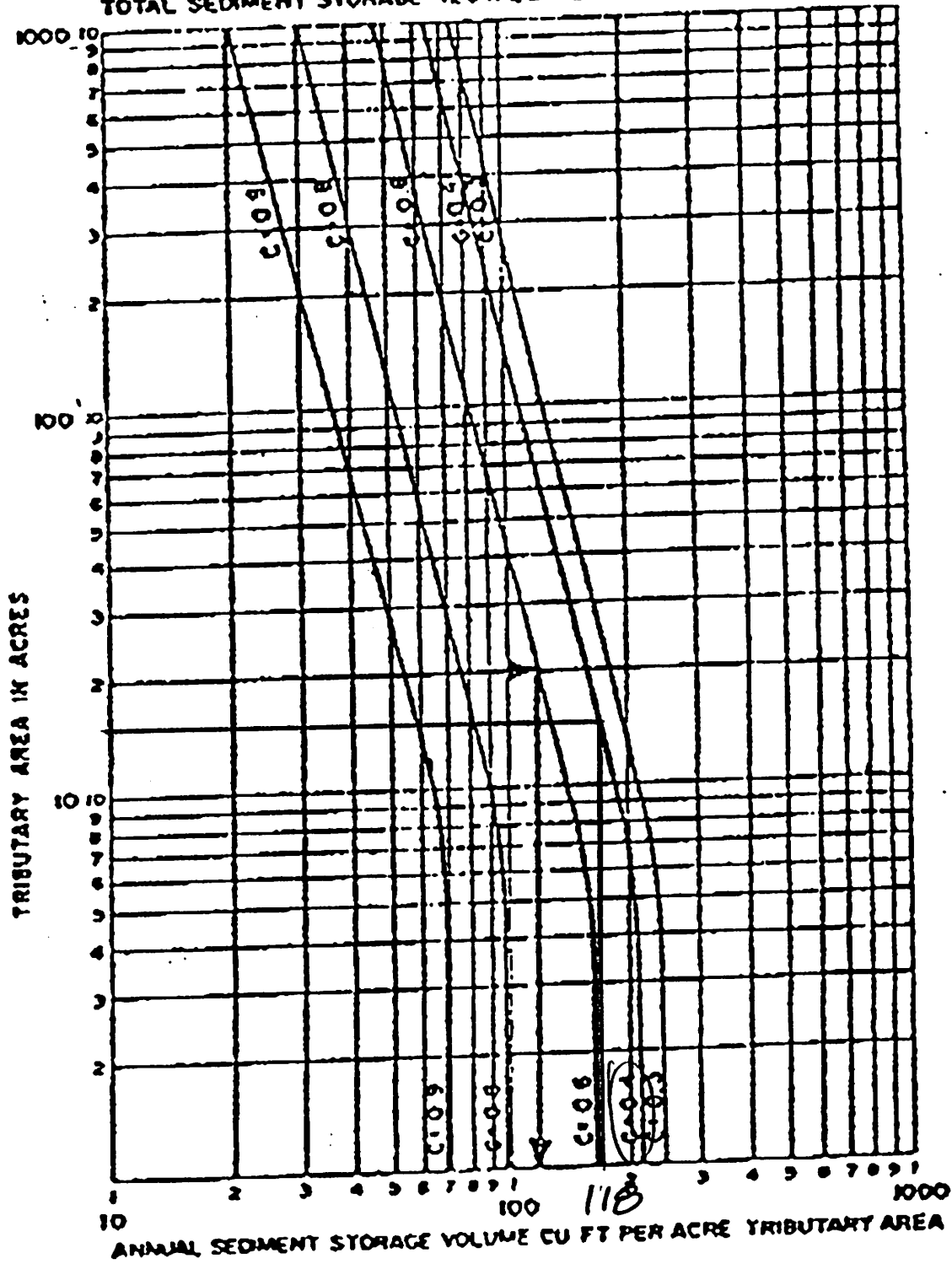
EXAMPLE:

TRIBUTARY AREA - 20 ACRES

RATIONAL METHOD RUNOFF COEFFICIENT "C" = 0.6

SEDIMENT STORAGE = 120 CU. FT. PER ACRE PER YEAR

TOTAL SEDIMENT STORAGE = 120 X 20 = 2400 CU. FT. PER YEAR.



ANNUAL SEDIMENT STORAGE

FIG. 1



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SEDIMENT STORAGE CALCULATIONS  
INDIAN SPRINGS - NORTH BASIN  
BAX PROJECT NO. 96-8861  
APRIL 11, 1997

Sediment storage will be provided by over excavation of the lake bottom. The following calculations are based on an attached nomograph provided by the City of O'Fallon.

Total disturbed area tributary to lake: 17.37 AC.  
Rational Method "C" Factor: 0.40%

FROM FIGURE 1:

The required volume for 5 year construction period:

5 x ~~117~~ Cu.Ft./Ac. x 17.37 Ac. = 10,160 Cu.Ft.

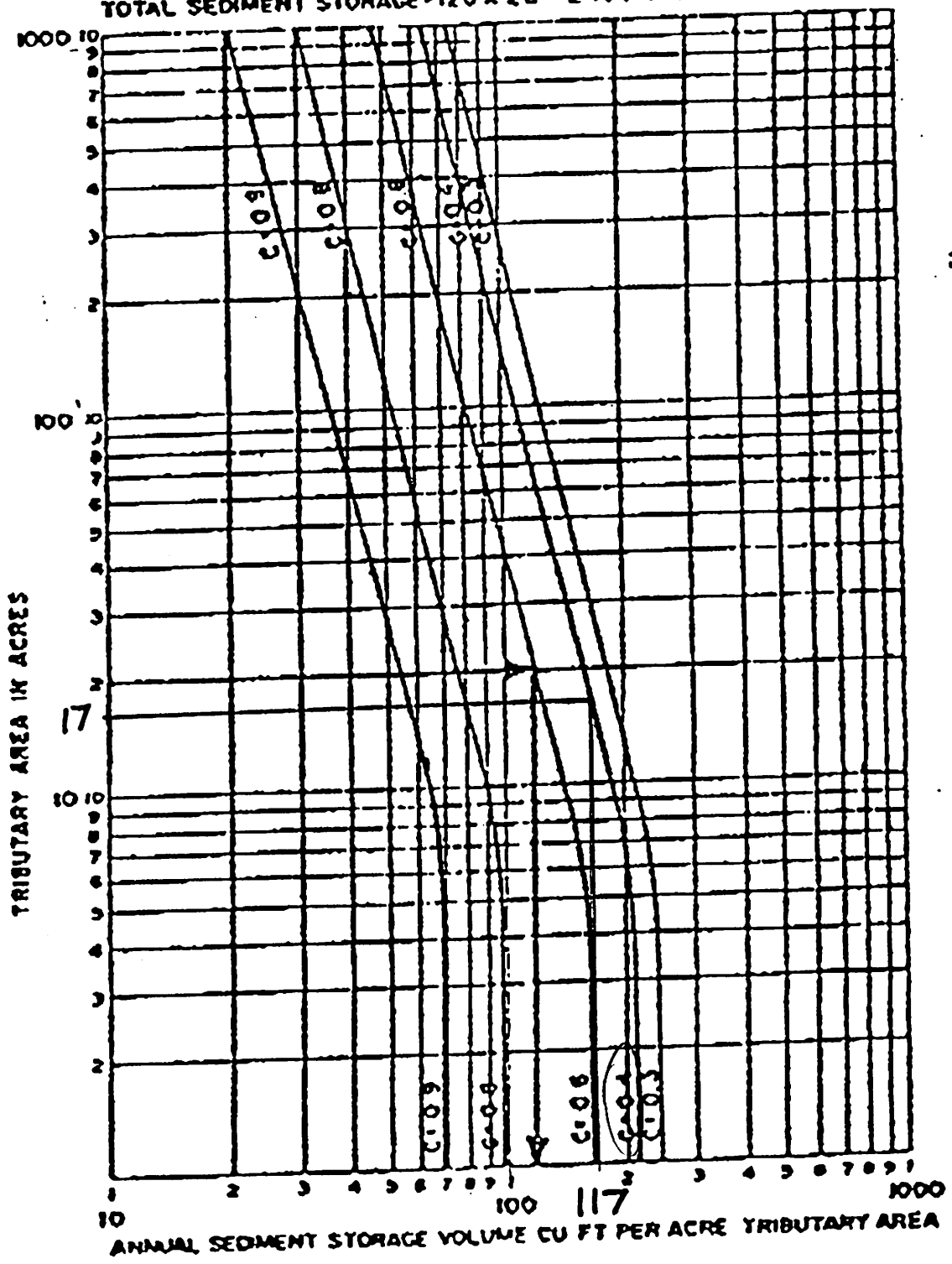
Volume Calculation: <sup>160</sup> 12,896

ELEVATION	AREA	VOLUME	TOTAL VOLUME
602.0	10,038 s.f.	0 c.f.	0 c.f.
601.0	8,810 s.f.	9,424 c.f.	9,424 c.f.
600.0	7,659 s.f.	8,235 c.f.	17,659 c.f.

11,482

Based on the above calculations the lake will be required to be over-excavated 1.25' (11,590 c.f.) to provide storage for the anticipated sediment run-off.

EXAMPLE:  
TRIBUTARY AREA = 20 ACRES  
RATIONAL METHOD RUNOFF COEFFICIENT "C" = 0.6  
SEDIMENT STORAGE = 120 CU. FT. PER ACRE PER YEAR  
TOTAL SEDIMENT STORAGE = 120 X 20 = 2400 CU. FT. PER YEAR.



ANNUAL SEDIMENT STORAGE

FIG. 1





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SEDIMENT STORAGE CALCULATIONS  
INDIAN SPRINGS - WEST BASIN  
BAX PROJECT NO. 96-8861  
APRIL 11, 1997

Sediment storage will be provided by over excavation of the lake bottom. The following calculations are based on an attached nomograph provided by the City of O'Fallon.

Total disturbed area tributary to lake: 6.03 AC.  
Rational Method "C" Factor: 0.40%

FROM FIGURE 1:

The required volume for 5 year construction period:

$$5 \times \frac{120}{220} \text{ Cu.Ft./Ac.} \times 6.03 \text{ Ac.} = 3,620 \text{ Cu.Ft.}$$

*6,633*

Volume Calculation:

ELEVATION	AREA	VOLUME	TOTAL VOLUME
612.0	3,319 s.f.	0 c.f.	0 c.f.
611.0	2,650 s.f.	2,985 c.f.	2,985 c.f.
610.0	2,052 s.f.	2,351 c.f.	5,336 c.f.

Based on the above calculations the lake will be required to be over-excavated 1.25' (3,629 c.f.) to provide storage for the anticipated sediment run-off.

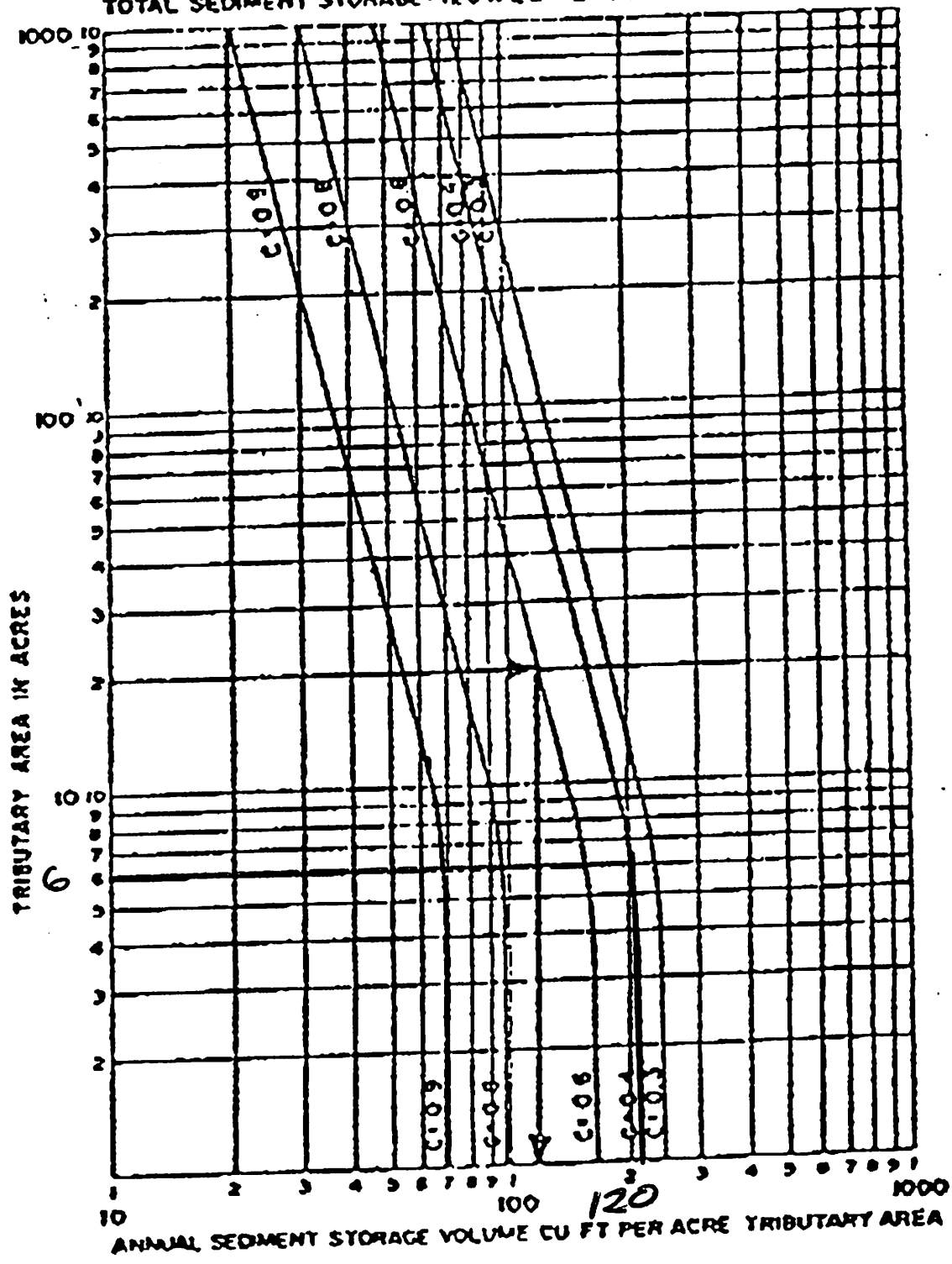
EXAMPLE:

TRIBUTARY AREA - 20 ACRES

RATIONAL METHOD RUNOFF COEFFICIENT "C" = 0.6

SEDIMENT STORAGE = 120 CU. FT. PER ACRE PER YEAR

TOTAL SEDIMENT STORAGE = 120 X 20 = 2400 CU. FT. PER YEAR.



ANNUAL SEDIMENT STORAGE

FIG. 1



DAVID W. HOUSE  
FIRE CHIEF

## O'FALLON FIRE PROTECTION DISTRICT

119 EAST ELM STREET, O'FALLON, MISSOURI 63366-2600

(314) 272-3493

240-5312

FAX 272-7857

June 18, 1997

Mr. David Jones  
Bax Engineering  
1052 South Cloverleaf Drive  
St. Peters, Missouri 63376-6445

RE: Indian Springs Water Improvement Plan

Dear Mr. Jones:

Our office has reviewed and approved the Water Improvement Plan (dated 3-12-97) for the proposed Indian Springs subdivision .

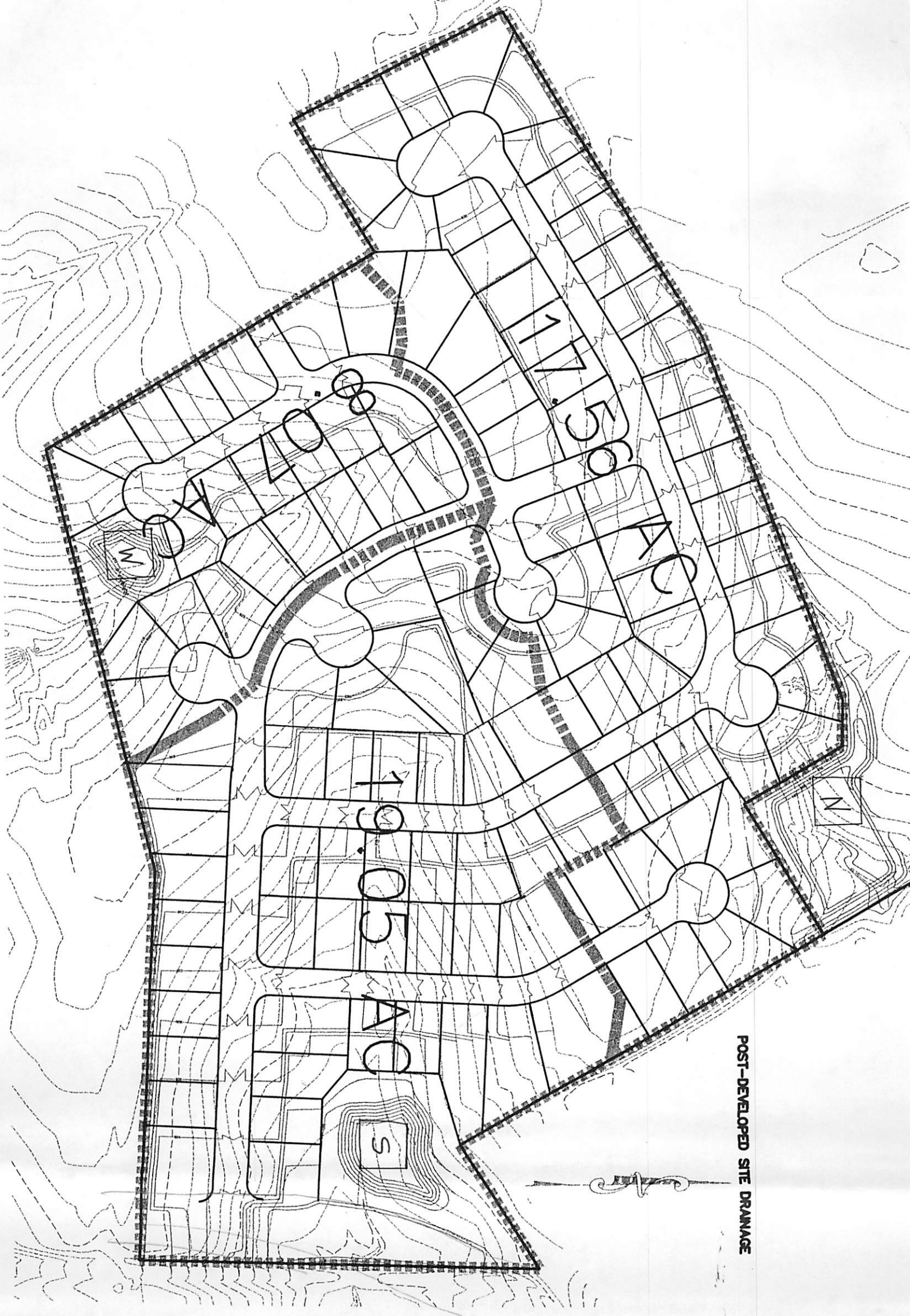
Should you have any questions concerning the above please do not hesitate to contact our office.

Sincerely,

A handwritten signature in black ink, appearing to read "D. W. House", written over a horizontal line.

David W. House  
Fire Chief

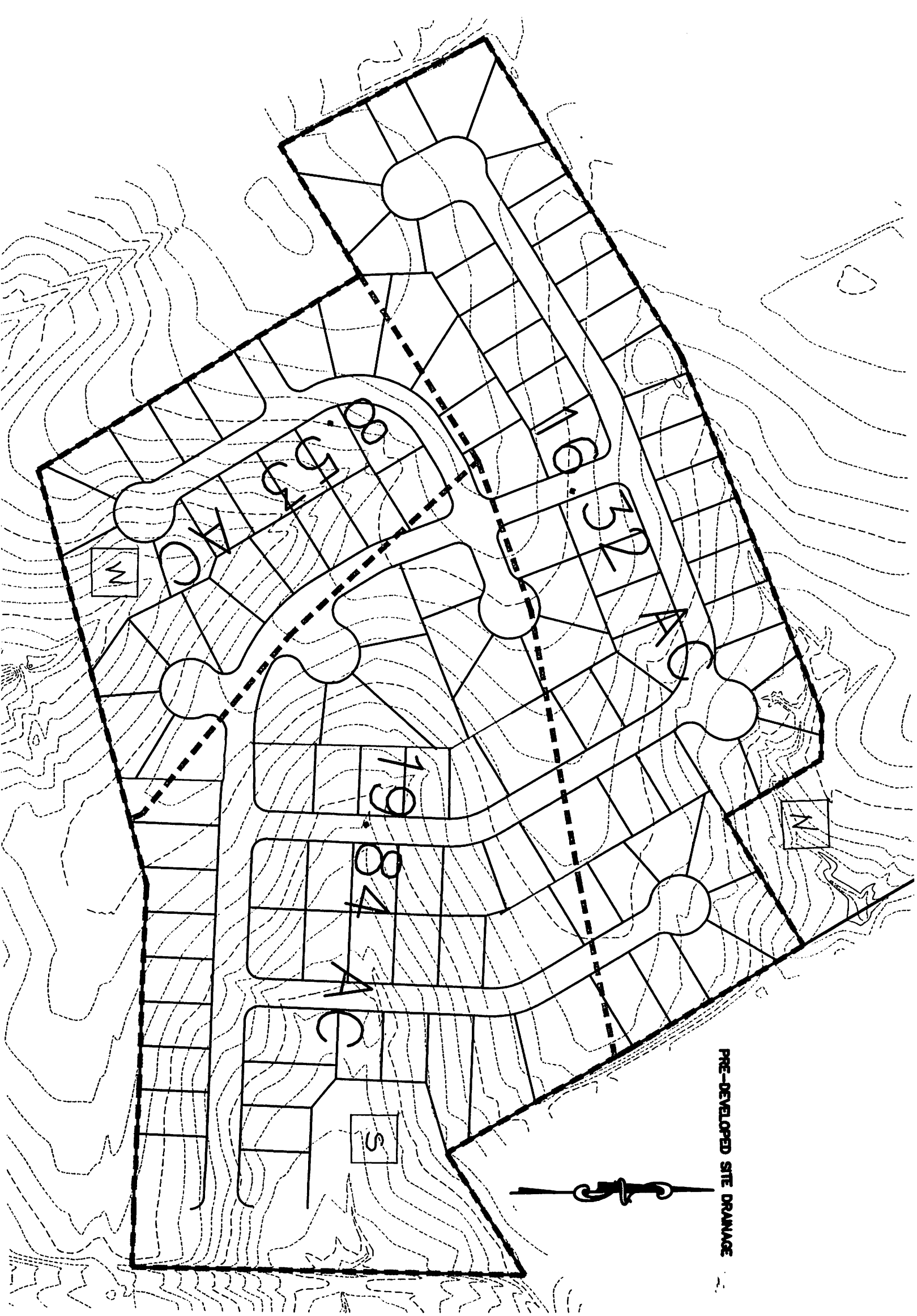
cc: O'Fallon Engineering Dept.



POST-DEVELOPED SITE DRAINAGE







PRE-DEVELOPED SITE DRAINAGE

```
*****  
*  
* INDIAN SPRINGS NORTH WATERSHE *  
* DETENTION ANALYSIS *  
* PREPARED BY: BAX ENGINEERING CO., INC. *  
* MARCH 5, 1997 *  
*  
*****
```

\*\*\*\*\* SUMMARY OF ROUTING COMPUTATIONS \*\*\*\*\*

Pond File: 8861N .PND  
Inflow Hydrograph: 8861N002.HYD  
Outflow Hydrograph:

Starting Pond W.S. Elevation = 600.00 ft

\*\*\*\*\* Summary of Peak Outflow and Peak Elevation \*\*\*\*\*

Peak Inflow = 47.25 cfs  
Peak Outflow = 37.03 cfs  
Peak Elevation = 602.79 ft

\*\*\*\*\* Summary of Approximate Peak Storage \*\*\*\*\*

Initial Storage = 0.00 ac-ft  
Peak Storage From Storm = 0.39 ac-ft  
-----  
Total Storage in Pond = 0.39 ac-ft

```
*****  
*                                                                 *  
* INDIAN SPRINGS                                           NORTH WATERSHE *  
*                               DETENTION ANALYSIS          *  
*           PREPARED BY: BAX ENGINEERING CO., INC.         *  
*                               MARCH 5, 1997                *  
*                                                                 *  
*****
```

\*\*\*\*\* SUMMARY OF ROUTING COMPUTATIONS \*\*\*\*\*

Pond File: 8861N .PND  
Inflow Hydrograph: 8861N005.HYD  
Outflow Hydrograph:

Starting Pond W.S. Elevation = 600.00 ft

\*\*\*\*\* Summary of Peak Outflow and Peak Elevation \*\*\*\*\*

Peak Inflow = 58.11 cfs  
Peak Outflow = 44.56 cfs  
Peak Elevation = 603.09 ft

\*\*\*\*\* Summary of Approximate Peak Storage \*\*\*\*\*

Initial Storage = 0.00 ac-ft  
Peak Storage From Storm = 0.51 ac-ft  
-----  
Total Storage in Pond = 0.51 ac-ft



```
*****  
*  
* INDIAN SPRINGS NORTH WATERSHE *  
* DETENTION ANALYSIS *  
* PREPARED BY: BAX ENGINEERING CO., INC. *  
* MARCH 5, 1997 *  
*  
*****
```

\*\*\*\*\* SUMMARY OF ROUTING COMPUTATIONS \*\*\*\*\*

Pond File: 8861N .PND  
Inflow Hydrograph: 8861N015.HYD  
Outflow Hydrograph:

Starting Pond W.S. Elevation = 600.00 ft

\*\*\*\*\* Summary of Peak Outflow and Peak Elevation \*\*\*\*\*

Peak Inflow = 77.48 cfs  
Peak Outflow = 57.54 cfs  
Peak Elevation = 603.57 ft

\*\*\*\*\* Summary of Approximate Peak Storage \*\*\*\*\*

Initial Storage = 0.00 ac-ft  
Peak Storage From Storm = 0.74 ac-ft  
-----  
Total Storage in Pond = 0.74 ac-ft

```
*****  
*  
* INDIAN SPRINGS NORTH WATERSHE *  
* DETENTION ANALYSIS *  
* PREPARED BY: BAX ENGINEERING CO., INC. *  
* MARCH 5, 1997 *  
*  
*****
```

\*\*\*\*\* SUMMARY OF ROUTING COMPUTATIONS \*\*\*\*\*

Pond File: 8861N .PND  
Inflow Hydrograph: 8861N025.HYD  
Outflow Hydrograph:

Starting Pond W.S. Elevation = 600.00 ft

\*\*\*\*\* Summary of Peak Outflow and Peak Elevation \*\*\*\*\*

Peak Inflow = 95.70 cfs  
Peak Outflow = 67.20 cfs  
Peak Elevation = 603.96 ft

\*\*\*\*\* Summary of Approximate Peak Storage \*\*\*\*\*

Initial Storage = 0.00 ac-ft  
Peak Storage From Storm = 0.98 ac-ft  
-----  
Total Storage in Pond = 0.98 ac-ft

\*\*\*\*\*  
INDIAN SPRINGS NORTH BASIN  
DETENTION ANALYSIS  
PREPARED BY: BAX ENGINEERING CO., INC.  
MARCH 5, 1997  
\*\*\*\*\*

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*

Elevation (ft)	Q (cfs)	Contributing Structures
600.00	0.0	2
600.20	0.9	2
600.40	2.5	2
600.60	4.6	2
600.80	7.2	2
601.00	10.0	2
601.20	13.1	2
601.40	15.2	1
601.60	16.8	1
601.80	18.4	4 +1
602.00	21.2	4 +1
602.20	24.5	4 +1
602.40	28.4	4 +1
602.60	32.7	4 +1
602.80	37.3	4 +1
603.00	42.1	4 +1
603.20	47.3	4 +1
603.40	52.8	4 +1
603.60	58.5	4 +1
603.80	64.4	4 +1
604.00	67.9	3 +1
604.20	71.1	3 +1
604.40	74.2	3 +1
604.60	77.1	3 +1
604.80	79.9	3 +1
605.00	82.7	5 +3 +1
605.20	88.4	5 +3 +1
605.40	96.7	5 +3 +1
605.60	106.6	5 +3 +1
605.80	117.7	5 +3 +1
606.00	130.0	5 +3 +1

Outlet Structure File: 8861N .STR

POND-2 Version: 5.17

S/N:

Date Executed:

Time Executed:

\*\*\*\*\*  
INDIAN SPRINGS NORTH BASIN

DETENTION ANALYSIS  
PREPARED BY: BAX ENGINEERING CO., INC.  
MARCH 5, 1997

\*\*\*\*\*

Outlet Structure File: 8861N .STR  
Planimeter Input File: 8861N .VOL  
Rating Table Output File: 8861N .PND

Min. Elev.(ft) = 600 Max. Elev.(ft) = 606 Incr.(ft) = .2

Additional elevations (ft) to be included in table:  
\*\*\*\*\*

\*\*\*\*\*  
SYSTEM CONNECTIVITY  
\*\*\*\*\*

Structure	No.	Q Table	Q Table
WEIR-VR	5		-> 5
WEIR-VR	4		-> 4
ORIFICE	3	? 4	-> A
WEIR-VR	2		-> 2
ORIFICE	1	? 2	-> B

Outflow rating table summary was stored in file:  
8861N .PND

Outlet Structure File: 8861N .STR

POND-2 Version: 5.17

S/N:

Date Executed:

Time Executed:

\*\*\*\*\*  
INDIAN SPRINGS NORTH BASIN

DETENTION ANALYSIS  
PREPARED BY: BAX ENGINEERING CO., INC.  
MARCH 5, 1997

\*\*\*\*\*

>>>>> Structure No. 5 <<<<<<  
( Input Data )

WEIR-VR  
Weir - Vertical Rectangular

E1 elev.(ft)?	605
E2 elev.(ft)?	606.001
Weir coefficient?	3
Weir elev.(ft)?	605.000
Length (ft)?	11.67
Contracted/Suppressed (C/S)?	S



Outlet Structure File: 8861N .STR

POND-2 Version: 5.17

S/N:

Date Executed:

Time Executed:

\*\*\*\*\*  
INDIAN SPRINGS NORTH BASIN

DETENTION ANALYSIS  
PREPARED BY: BAX ENGINEERING CO., INC.  
MARCH 5, 1997

\*\*\*\*\*

>>>>> Structure No. 4 <<<<<<  
(Input Data)

WEIR-VR  
Weir - Vertical Rectangular

E1 elev.(ft)?	601.75
E2 elev.(ft)?	606.001
Weir coefficient?	3
Weir elev.(ft)?	601.75
Length (ft)?	4.0
Contracted/Suppressed (C/S)?	S

Outlet Structure File: 8861N .STR

POND-2 Version: 5.17  
Date Executed:

S/N:  
Time Executed:

\*\*\*\*\*  
INDIAN SPRINGS NORTH BASIN  
DETENTION ANALYSIS  
PREPARED BY: BAX ENGINEERING CO., INC.  
MARCH 5, 1997  
\*\*\*\*\*

>>>>> Structure No. 3 <<<<<<  
(Input Data)

ORIFICE  
Orifice - Based on Area and Datum Elevation

E1 elev.(ft)?	603.25
E2 elev.(ft)?	606.001
Orifice coeff.?	0.6
Invert elev.(ft)?	601.6667
Datum elev.(ft) ?	602.4583
Orifice area (sq ft)?	6.333333

Outlet Structure File: 8861N .STR

POND-2 Version: 5.17

S/N:

Date Executed:

Time Executed:

\*\*\*\*\*  
INDIAN SPRINGS

NORTH BASIN

DETENTION ANALYSIS  
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MARCH 5, 1997

\*\*\*\*\*

>>>>> Structure No. 2 <<<<<<  
(Input Data)

WEIR-VR  
Weir - Vertical Rectangular

E1 elev.(ft)?	600
E2 elev.(ft)?	606.001
Weir coefficient?	3
Weir elev.(ft)?	600
Length (ft)?	3.333333
Contracted/Suppressed (C/S)?	S

Outlet Structure File: 8861N .STR

POND-2 Version: 5.17  
Date Executed:

S/N:  
Time Executed:

\*\*\*\*\*  
INDIAN SPRINGS NORTH BASIN

DETENTION ANALYSIS  
PREPARED BY: BAX ENGINEERING CO., INC.  
MARCH 5, 1997

\*\*\*\*\*

>>>>> Structure No. 1 <<<<<<  
(Input Data)

ORIFICE

Orifice - Based on Area and Datum Elevation

E1 elev.(ft)?	601
E2 elev.(ft)?	606.001
Orifice coeff.?	.6
Invert elev.(ft)?	600
Datum elev.(ft)?	600.5
Orifice area (sq ft)?	3.333333

\*\*\*\*\*  
 INDIAN SPRINGS NORTH BASIN  
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 \*\*\*\*\*

Outflow Rating Table for Structure #5  
 WEIR-VR Weir - Vertical Rectangular

\*\*\*\*\* INLET CONTROL ASSUMED \*\*\*\*\*

Elevation (ft)	Q (cfs)	Computation Messages
600.00	0.0	E < Inv.El. = 605
600.20	0.0	E < Inv.El. = 605
600.40	0.0	E < Inv.El. = 605
600.60	0.0	E < Inv.El. = 605
600.80	0.0	E < Inv.El. = 605
601.00	0.0	E < Inv.El. = 605
601.20	0.0	E < Inv.El. = 605
601.40	0.0	E < Inv.El. = 605
601.60	0.0	E < Inv.El. = 605
601.80	0.0	E < Inv.El. = 605
602.00	0.0	E < Inv.El. = 605
602.20	0.0	E < Inv.El. = 605
602.40	0.0	E < Inv.El. = 605
602.60	0.0	E < Inv.El. = 605
602.80	0.0	E < Inv.El. = 605
603.00	0.0	E < Inv.El. = 605
603.20	0.0	E < Inv.El. = 605
603.40	0.0	E < Inv.El. = 605
603.60	0.0	E < Inv.El. = 605
603.80	0.0	E < Inv.El. = 605
604.00	0.0	E < Inv.El. = 605
604.20	0.0	E < Inv.El. = 605
604.40	0.0	E < Inv.El. = 605
604.60	0.0	E < Inv.El. = 605
604.80	0.0	E < Inv.El. = 605
605.00	0.0	H = 0.0
605.20	3.1	H = .2
605.40	8.9	H = .4
605.60	16.3	H = .6
605.80	25.1	H = .8
606.00	35.0	H = 1.0

C = 3 L (ft) = 11.67  
 H (ft) = Table elev. - Invert elev. ( 605 ft )  
 Q (cfs) = C \* L \* (H\*\*1.5) -- Suppressed Weir



\*\*\*\*\*  
 INDIAN SPRINGS NORTH BASIN  
 DETENTION ANALYSIS  
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 \*\*\*\*\*

Outflow Rating Table for Structure #4  
 WEIR-VR Weir - Vertical Rectangular

\*\*\*\*\* INLET CONTROL ASSUMED \*\*\*\*\*

Elevation (ft)	Q (cfs)	Computation Messages
600.00	0.0	E < Inv.El. = 601.75
600.20	0.0	E < Inv.El. = 601.75
600.40	0.0	E < Inv.El. = 601.75
600.60	0.0	E < Inv.El. = 601.75
600.80	0.0	E < Inv.El. = 601.75
601.00	0.0	E < Inv.El. = 601.75
601.20	0.0	E < Inv.El. = 601.75
601.40	0.0	E < Inv.El. = 601.75
601.60	0.0	E < Inv.El. = 601.75
601.80	0.1	H = .05
602.00	1.5	H = .25
602.20	3.6	H = .45
602.40	6.3	H = .65
602.60	9.4	H = .85
602.80	12.9	H = 1.05
603.00	16.8	H = 1.25
603.20	21.0	H = 1.45
603.40	25.4	H = 1.65
603.60	30.2	H = 1.85
603.80	35.2	H = 2.05
604.00	40.5	H = 2.25
604.20	46.0	H = 2.45
604.40	51.8	H = 2.65
604.60	57.7	H = 2.85
604.80	63.9	H = 3.05
605.00	70.3	H = 3.25
605.20	76.9	H = 3.45
605.40	83.7	H = 3.65
605.60	90.7	H = 3.85
605.80	97.8	H = 4.05
606.00	105.1	H = 4.25

C = 3 L (ft) = 4  
 H (ft) = Table elev. - Invert elev. ( 601.75 ft )  
 Q (cfs) = C \* L \* (H\*\*1.5) -- Suppressed Weir

\*\*\*\*\*  
INDIAN SPRINGS NORTH BASIN

DETENTION ANALYSIS  
PREPARED BY: BAX ENGINEERING CO., INC.  
MARCH 5, 1997

\*\*\*\*\*

Outflow Rating Table for Structure #3  
ORIFICE Orifice - Based on Area and Datum Elevation

Elevation (ft)	Q (cfs)	Computation Messages
600.00	0.0	E < E1=603.25
600.20	0.0	E < E1=603.25
600.40	0.0	E < E1=603.25
600.60	0.0	E < E1=603.25
600.80	0.0	E < E1=603.25
601.00	0.0	E < E1=603.25
601.20	0.0	E < E1=603.25
601.40	0.0	E < E1=603.25
601.60	0.0	E < E1=603.25
601.80	0.0	E < E1=603.25
602.00	0.0	E < E1=603.25
602.20	0.0	E < E1=603.25
602.40	0.0	E < E1=603.25
602.60	0.0	E < E1=603.25
602.80	0.0	E < E1=603.25
603.00	0.0	E < E1=603.25
603.20	0.0	E < E1=603.25
603.40	29.6	H =.942
603.60	32.6	H =1.142
603.80	35.3	H =1.342
604.00	37.9	H =1.542
604.20	40.2	H =1.742
604.40	42.5	H =1.942
604.60	44.6	H =2.142
604.80	46.7	H =2.342
605.00	48.6	H =2.542
605.20	50.5	H =2.742
605.40	52.3	H =2.942
605.60	54.1	H =3.142
605.80	55.7	H =3.342
606.00	57.4	H =3.542

C = .6      A = 6.333333 sq.ft.  
H (ft) = Table elev. - Datum elev. ( 602.4583 ft )  
Q (cfs) = C \* A \* sqr(2g \* H)

\*\*\*\*\*  
 INDIAN SPRINGS NORTH BASIN  
 DETENTION ANALYSIS  
 PREPARED BY: BAX ENGINEERING CO., INC.  
 MARCH 5, 1997  
 \*\*\*\*\*

Outflow Rating Table for Structure #2  
 WEIR-VR Weir - Vertical Rectangular

\*\*\*\*\* INLET CONTROL ASSUMED \*\*\*\*\*

Elevation (ft)	Q (cfs)	Computation Messages
600.00	0.0	H =0.0
600.20	0.9	H =.2
600.40	2.5	H =.4
600.60	4.6	H =.6
600.80	7.2	H =.8
601.00	10.0	H =1.0
601.20	13.1	H =1.2
601.40	16.6	H =1.4
601.60	20.2	H =1.6
601.80	24.1	H =1.8
602.00	28.3	H =2.0
602.20	32.6	H =2.2
602.40	37.2	H =2.4
602.60	41.9	H =2.6
602.80	46.9	H =2.8
603.00	52.0	H =3.0
603.20	57.2	H =3.2
603.40	62.7	H =3.4
603.60	68.3	H =3.6
603.80	74.1	H =3.8
604.00	80.0	H =4.0
604.20	86.1	H =4.2
604.40	92.3	H =4.4
604.60	98.7	H =4.6
604.80	105.2	H =4.8
605.00	111.8	H =5.0
605.20	118.6	H =5.2
605.40	125.5	H =5.4
605.60	132.5	H =5.6
605.80	139.7	H =5.8
606.00	147.0	H =6.0

C = 3 L (ft) = 3.333333  
 H (ft) = Table elev. - Invert elev. ( 600 ft )  
 Q (cfs) = C \* L \* (H\*\*1.5) -- Suppressed Weir

\*\*\*\*\*  
 INDIAN SPRINGS NORTH BASIN

DETENTION ANALYSIS  
 PREPARED BY: BAX ENGINEERING CO., INC.  
 MARCH 5, 1997

\*\*\*\*\*

Outflow Rating Table for Structure #1  
 ORIFICE Orifice - Based on Area and Datum Elevation

Elevation (ft)	Q (cfs)	Computation Messages
600.00	0.0	E < E1=601
600.20	0.0	E < E1=601
600.40	0.0	E < E1=601
600.60	0.0	E < E1=601
600.80	0.0	E < E1=601
601.00	11.3	H =.5
601.20	13.4	H =.7
601.40	15.2	H =.9
601.60	16.8	H =1.1
601.80	18.3	H =1.3
602.00	19.7	H =1.5
602.20	20.9	H =1.7
602.40	22.1	H =1.9
602.60	23.3	H =2.1
602.80	24.3	H =2.3
603.00	25.4	H =2.5
603.20	26.4	H =2.7
603.40	27.3	H =2.9
603.60	28.3	H =3.1
603.80	29.2	H =3.3
604.00	30.0	H =3.5
604.20	30.9	H =3.7
604.40	31.7	H =3.9
604.60	32.5	H =4.1
604.80	33.3	H =4.3
605.00	34.0	H =4.5
605.20	34.8	H =4.7
605.40	35.5	H =4.9
605.60	36.2	H =5.1
605.80	36.9	H =5.3
606.00	37.6	H =5.5

C = .6      A = 3.333333 sq.ft.  
 H (ft) = Table elev. - Datum elev. ( 600.5 ft )  
 Q (cfs) = C \* A \* sqr(2g \* H)

\*\*\*\*\*  
 INDIAN SPRINGS NORTH BASIN  
 DETENTION ANALYSIS  
 PREPARED BY: BAX ENGINEERING CO., INC.  
 MARCH 5, 1997  
 \*\*\*\*\*

Outflow Rating Table A  
 Table A = 4 ? 3

Elevation (ft)	Q (cfs)	Contributing Structures
600.00	0.0	-
600.20	0.0	-
600.40	0.0	-
600.60	0.0	-
600.80	0.0	-
601.00	0.0	-
601.20	0.0	-
601.40	0.0	-
601.60	0.0	-
601.80	0.1	4
602.00	1.5	4
602.20	3.6	4
602.40	6.3	4
602.60	9.4	4
602.80	12.9	4
603.00	16.8	4
603.20	21.0	4
603.40	25.4	4
603.60	30.2	4
603.80	35.2	4
604.00	37.9	3
604.20	40.2	3
604.40	42.5	3
604.60	44.6	3
604.80	46.7	3
605.00	48.6	3
605.20	50.5	3
605.40	52.3	3
605.60	54.1	3
605.80	55.7	3
606.00	57.4	3



\*\*\*\*\*  
INDIAN SPRINGS NORTH BASIN

DETENTION ANALYSIS  
PREPARED BY: BAX ENGINEERING CO., INC.  
MARCH 5, 1997

\*\*\*\*\*

Outflow Rating Table B  
Table B = 2 ? 1

<u>Elevation (ft)</u>	<u>Q (cfs)</u>	<u>Contributing Structures</u>
600.00	0.0	2
600.20	0.9	2
600.40	2.5	2
600.60	4.6	2
600.80	7.2	2
601.00	10.0	2
601.20	13.1	2
601.40	15.2	1
601.60	16.8	1
601.80	18.3	1
602.00	19.7	1
602.20	20.9	1
602.40	22.1	1
602.60	23.3	1
602.80	24.3	1
603.00	25.4	1
603.20	26.4	1
603.40	27.3	1
603.60	28.3	1
603.80	29.2	1
604.00	30.0	1
604.20	30.9	1
604.40	31.7	1
604.60	32.5	1
604.80	33.3	1
605.00	34.0	1
605.20	34.8	1
605.40	35.5	1
605.60	36.2	1
605.80	36.9	1
606.00	37.6	1

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*****  
*  
* INDIAN SPRINGS SOUTH WATERSHE *  
* DETENTION ANALYSIS *  
* PREPARED BY: BAX ENGINEERING CO., INC. *  
* MARCH 5, 1997 *  
*  
*****
```

\*\*\*\*\* SUMMARY OF ROUTING COMPUTATIONS \*\*\*\*\*

Pond File: 8861S .PND  
Inflow Hydrograph: 8861S002.HYD  
Outflow Hydrograph:

Starting Pond W.S. Elevation = 592.00 ft

\*\*\*\*\* Summary of Peak Outflow and Peak Elevation \*\*\*\*\*

Peak Inflow = 30.09 cfs  
Peak Outflow = 16.26 cfs  
Peak Elevation = 593.43 ft

\*\*\*\*\* Summary of Approximate Peak Storage \*\*\*\*\*

Initial Storage = 1.84 ac-ft  
Peak Storage From Storm = 0.63 ac-ft  
-----  
Total Storage in Pond = 2.46 ac-ft

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*  
* INDIAN SPRINGS SOUTH WATERSHE *  
* DETENTION ANALYSIS *  
* PREPARED BY: BAX ENGINEERING CO., INC. *  
* MARCH 5, 1997 *  
*  
*****
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\*\*\*\*\* SUMMARY OF ROUTING COMPUTATIONS \*\*\*\*\*

Pond File: 8861S .PND  
Inflow Hydrograph: 8861S005.HYD  
Outflow Hydrograph:

Starting Pond W.S. Elevation = 592.00 ft

\*\*\*\*\* Summary of Peak Outflow and Peak Elevation \*\*\*\*\*

Peak Inflow = 37.01 cfs  
Peak Outflow = 22.20 cfs  
Peak Elevation = 593.65 ft

\*\*\*\*\* Summary of Approximate Peak Storage \*\*\*\*\*

Initial Storage = 1.84 ac-ft  
Peak Storage From Storm = 0.73 ac-ft  
-----  
Total Storage in Pond = 2.56 ac-ft

\*\*\*\*\*  
\*  
\* INDIAN SPRINGS SOUTH WATERSHE \*  
\* DETENTION ANALYSIS \*  
\* PREPARED BY: BAX ENGINEERING CO., INC. \*  
\* MARCH 5, 1997 \*  
\*  
\*\*\*\*\*

\*\*\*\*\* SUMMARY OF ROUTING COMPUTATIONS \*\*\*\*\*

Pond File: 8861S .PND  
Inflow Hydrograph: 8861S015.HYD  
Outflow Hydrograph:

Starting Pond W.S. Elevation = 592.00 ft

\*\*\*\*\* Summary of Peak Outflow and Peak Elevation \*\*\*\*\*

Peak Inflow = 49.34 cfs  
Peak Outflow = 32.84 cfs  
Peak Elevation = 593.99 ft

\*\*\*\*\* Summary of Approximate Peak Storage \*\*\*\*\*

Initial Storage = 1.84 ac-ft  
Peak Storage From Storm = 0.89 ac-ft  
-----  
Total Storage in Pond = 2.73 ac-ft

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\*  
\* INDIAN SPRINGS SOUTH WATERSHE \*  
\* DETENTION ANALYSIS \*  
\* PREPARED BY: BAX ENGINEERING CO., INC. \*  
\* MARCH 5, 1997 \*  
\*  
\*\*\*\*\*

\*\*\*\*\* SUMMARY OF ROUTING COMPUTATIONS \*\*\*\*\*

Pond File: 8861S .PND  
Inflow Hydrograph: 8861S025.HYD  
Outflow Hydrograph:

Starting Pond W.S. Elevation = 592.00 ft

\*\*\*\*\* Summary of Peak Outflow and Peak Elevation \*\*\*\*\*

Peak Inflow = 60.93 cfs  
Peak Outflow = 43.04 cfs  
Peak Elevation = 594.29 ft

\*\*\*\*\* Summary of Approximate Peak Storage \*\*\*\*\*

Initial Storage = 1.84 ac-ft  
Peak Storage From Storm = 1.04 ac-ft  
-----  
Total Storage in Pond = 2.87 ac-ft





Outlet Structure File: 8861S .STR

POND-2 Version: 5.17

S/N:

Date Executed:

Time Executed:

\*\*\*\*\*

INDIAN SPRINGS

SOUTH BASIN

DETENTION ANALYSIS

PREPARED BY: BAX ENGINEERING CO., INC.

MARCH 5, 1997

\*\*\*\*\*

Outlet Structure File: 8861S .STR  
Planimeter Input File: 8861S .VOL  
Rating Table Output File: 8861S .PND

Min. Elev.(ft) = 592 Max. Elev.(ft) = 596 Incr.(ft) = .25

Additional elevations (ft) to be included in table:

\*\*\*\*\*

\*\*\*\*\*

SYSTEM CONNECTIVITY

\*\*\*\*\*

Structure	No.	Q Table	Q Table
-----	---	-----	-----
WEIR-VR	3		-> 3

Outflow rating table summary was stored in file:  
8861S .PND

Outlet Structure File: 8861S .STR

POND-2 Version: 5.17  
Date Executed:

S/N:  
Time Executed:

\*\*\*\*\*  
INDIAN SPRINGS SOUTH BASIN  
DETENTION ANALYSIS  
PREPARED BY: BAX ENGINEERING CO., INC.  
MARCH 5, 1997  
\*\*\*\*\*

>>>>> Structure No. 3 <<<<<<  
(Input Data)

WEIR-VR  
Weir - Vertical Rectangular

E1 elev.(ft)?	592.5
E2 elev.(ft)?	596.001
Weir coefficient?	3
Weir elev.(ft)?	592.500
Length (ft)?	6.0
Contracted/Suppressed (C/S)?	S

\*\*\*\*\*  
 INDIAN SPRINGS SOUTH BASIN

DETENTION ANALYSIS  
 PREPARED BY: BAX ENGINEERING CO., INC.  
 MARCH 5, 1997

\*\*\*\*\*

Outflow Rating Table for Structure #3  
 WEIR-VR Weir - Vertical Rectangular

\*\*\*\*\* INLET CONTROL ASSUMED \*\*\*\*\*

Elevation (ft)	Q (cfs)	Computation Messages
592.00	0.0	E < Inv.El. = 592.5
592.25	0.0	E < Inv.El. = 592.5
592.50	0.0	H = 0.0
592.75	2.3	H = .25
593.00	6.4	H = .5
593.25	11.7	H = .750
593.50	18.0	H = 1.0
593.75	25.2	H = 1.25
594.00	33.1	H = 1.5
594.25	41.7	H = 1.75
594.50	50.9	H = 2.0
594.75	60.8	H = 2.25
595.00	71.2	H = 2.5
595.25	82.1	H = 2.75
595.50	93.5	H = 3.0
595.75	105.5	H = 3.25
596.00	117.9	H = 3.5

C = 3 L (ft) = 6

H (ft) = Table elev. - Invert elev. ( 592.5 ft )

Q (cfs) = C \* L \* (H\*\*1.5) -- Suppressed Weir

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*****  
*  
* INDIAN SPRINGS WEST WATERSHE *  
* DETENTION ANALYSIS *  
* PREPARED BY: BAX ENGINEERING CO., INC. *  
* MARCH 5, 1997 *  
*  
*****
```

\*\*\*\*\* SUMMARY OF ROUTING COMPUTATIONS \*\*\*\*\*

Pond File: 8861W .PND  
Inflow Hydrograph: 8861W002.HYD  
Outflow Hydrograph:

Starting Pond W.S. Elevation = 610.00 ft

\*\*\*\*\* Summary of Peak Outflow and Peak Elevation \*\*\*\*\*

Peak Inflow = 10.29 cfs  
Peak Outflow = 4.12 cfs  
Peak Elevation = 613.44 ft

\*\*\*\*\* Summary of Approximate Peak Storage \*\*\*\*\*

Initial Storage = 0.00 ac-ft  
Peak Storage From Storm = 0.18 ac-ft  
-----  
Total Storage in Pond = 0.18 ac-ft

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*****  
*  
* INDIAN SPRINGS WEST WATERSHE *  
* DETENTION ANALYSIS *  
* PREPARED BY: BAX ENGINEERING CO., INC. *  
* MARCH 5, 1997 *  
*  
*****
```

\*\*\*\*\* SUMMARY OF ROUTING COMPUTATIONS \*\*\*\*\*

Pond File: 8861W .PND  
Inflow Hydrograph: 8861W005.HYD  
Outflow Hydrograph:

Starting Pond W.S. Elevation = 610.00 ft

\*\*\*\*\* Summary of Peak Outflow and Peak Elevation \*\*\*\*\*

Peak Inflow	=	12.65 cfs
Peak Outflow	=	4.48 cfs
Peak Elevation	=	613.97 ft

\*\*\*\*\* Summary of Approximate Peak Storage \*\*\*\*\*

Initial Storage	=	0.00 ac-ft
Peak Storage From Storm	=	0.23 ac-ft
		-----
Total Storage in Pond	=	0.23 ac-ft

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*****  
*  
* INDIAN SPRINGS WEST WATERSHE *  
* DETENTION ANALYSIS *  
* PREPARED BY: BAX ENGINEERING CO., INC. *  
* MARCH 5, 1997 *  
*  
*****
```

\*\*\*\*\* SUMMARY OF ROUTING COMPUTATIONS \*\*\*\*\*

Pond File: 8861W .PND  
Inflow Hydrograph: 8861W015.HYD  
Outflow Hydrograph:

Starting Pond W.S. Elevation = 610.00 ft

\*\*\*\*\* Summary of Peak Outflow and Peak Elevation \*\*\*\*\*

Peak Inflow = 16.87 cfs  
Peak Outflow = 5.01 cfs  
Peak Elevation = 614.83 ft

\*\*\*\*\* Summary of Approximate Peak Storage \*\*\*\*\*

Initial Storage = 0.00 ac-ft  
Peak Storage From Storm = 0.34 ac-ft  
-----  
Total Storage in Pond = 0.34 ac-ft

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*****  
*  
* INDIAN SPRINGS WEST WATERSHE *  
* DETENTION ANALYSIS *  
* PREPARED BY: BAX ENGINEERING CO., INC. *  
* MARCH 5, 1997 *  
*  
*****
```

\*\*\*\*\* SUMMARY OF ROUTING COMPUTATIONS \*\*\*\*\*

Pond File: 8861W .PND  
Inflow Hydrograph: 8861W025.HYD  
Outflow Hydrograph:

Starting Pond W.S. Elevation = 610.00 ft

\*\*\*\*\* Summary of Peak Outflow and Peak Elevation \*\*\*\*\*

Peak Inflow = 20.80 cfs  
Peak Outflow = 5.37 cfs  
Peak Elevation = 615.55 ft

\*\*\*\*\* Summary of Approximate Peak Storage \*\*\*\*\*

Initial Storage = 0.00 ac-ft  
Peak Storage From Storm = 0.43 ac-ft  
-----  
Total Storage in Pond = 0.43 ac-ft



\*\*\*\*\*  
 INDIAN SPRINGS WEST BASIN  
 DETENTION ANALYSIS  
 PREPARED BY: BAX ENGINEERING CO., INC.  
 MARCH 5, 1997  
 \*\*\*\*\*

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

Elevation (ft)	Q (cfs)	Contributing Structures
610.00	0.0	1
610.20	0.1	1
610.40	0.4	1
610.60	0.7	1
610.80	1.1	1
611.00	1.5	1
611.20	2.0	1
611.40	2.3	2
611.60	2.5	2
611.80	2.7	2
612.00	2.9	2
612.20	3.1	2
612.40	3.3	2
612.60	3.5	2
612.80	3.7	2
613.00	3.8	2
613.20	4.0	2
613.40	4.1	2
613.60	4.2	2
613.80	4.4	2
614.00	4.5	2
614.20	4.6	2
614.40	4.8	2
614.60	4.9	2
614.80	5.0	2
615.00	5.1	2
615.20	5.2	2
615.40	5.3	2
615.60	5.4	2
615.80	5.5	2
616.00	5.6	2
616.20	5.7	2
616.40	5.8	2
616.60	5.9	2
616.80	6.0	2
617.00	6.1	3 +2
617.20	9.4	3 +2
617.40	15.2	3 +2
617.60	22.7	3 +2
617.80	31.6	3 +2
618.00	41.6	3 +2

Outlet Structure File: 8861W .STR

POND-2 Version: 5.17

S/N:

Date Executed:

Time Executed:

\*\*\*\*\*  
INDIAN SPRINGS WEST BASIN

DETENTION ANALYSIS

PREPARED BY: BAX ENGINEERING CO., INC.

MARCH 5, 1997

\*\*\*\*\*

Outlet Structure File: 8861W .STR  
Planimeter Input File: 8861W .VOL  
Rating Table Output File: 8861W .PND

Min. Elev.(ft) = 610 Max. Elev.(ft) = 618 Incr.(ft) = .2

Additional elevations (ft) to be included in table:  
\*\*\*\*\*

\*\*\*\*\*  
SYSTEM CONNECTIVITY  
\*\*\*\*\*

Structure	No.	Q Table	Q Table
WEIR-VR	3		-> 3
WEIR-VR	1		-> 1
ORIFICE	2	? 1	-> A

Outflow rating table summary was stored in file:  
8861W .PND

Outlet Structure File: 8861W .STR

POND-2 Version: 5.17

S/N:

Date Executed:

Time Executed:

\*\*\*\*\*  
INDIAN SPRINGS WEST BASIN

DETENTION ANALYSIS  
PREPARED BY: BAX ENGINEERING CO., INC.  
MARCH 5, 1997

\*\*\*\*\*

>>>>> Structure No. 3 <<<<<<  
(Input Data)

WEIR-VR  
Weir - Vertical Rectangular

E1 elev.(ft)?	617
E2 elev.(ft)?	618.001
Weir coefficient?	3
Weir elev.(ft)?	617.000
Length (ft)?	11.67
Contracted/Suppressed (C/S)?	S

Outlet Structure File: 8861W .STR

POND-2 Version: 5.17

S/N:

Date Executed:

Time Executed:

\*\*\*\*\*  
INDIAN SPRINGS WEST BASIN

DETENTION ANALYSIS  
PREPARED BY: BAX ENGINEERING CO., INC.  
MARCH 5, 1997

\*\*\*\*\*

>>>>> Structure No. 1 <<<<<<  
(Input Data)

WEIR-VR  
Weir - Vertical Rectangular

E1 elev.(ft)?	610
E2 elev.(ft)?	618.001
Weir coefficient?	3
Weir elev.(ft)?	610.00
Length (ft)?	.500000
Contracted/Suppressed (C/S)?	S

Outlet Structure File: 8861W .STR

POND-2 Version: 5.17  
Date Executed:

S/N:  
Time Executed:

\*\*\*\*\*  
INDIAN SPRINGS WEST BASIN

DETENTION ANALYSIS  
PREPARED BY: BAX ENGINEERING CO., INC.  
MARCH 5, 1997

\*\*\*\*\*

>>>>> Structure No. 2 <<<<<<  
(Input Data)

ORIFICE  
Orifice - Based on Area and Datum Elevation

E1 elev.(ft)?	611.00
E2 elev.(ft)?	618.001
Orifice coeff.?	0.6
Invert elev.(ft)?	610.000
Datum elev.(ft) ?	610.5000
Orifice area (sq ft)?	0.50000

\*\*\*\*\*  
 INDIAN SPRINGS WEST BASIN

DETENTION ANALYSIS  
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 MARCH 5, 1997

\*\*\*\*\*

Outflow Rating Table for Structure #3  
 WEIR-VR Weir - Vertical Rectangular

\*\*\*\*\* INLET CONTROL ASSUMED \*\*\*\*\*

Elevation (ft)	Q (cfs)	Computation Messages
610.00	0.0	E < Inv.El.= 617
610.20	0.0	E < Inv.El.= 617
610.40	0.0	E < Inv.El.= 617
610.60	0.0	E < Inv.El.= 617
610.80	0.0	E < Inv.El.= 617
611.00	0.0	E < Inv.El.= 617
611.20	0.0	E < Inv.El.= 617
611.40	0.0	E < Inv.El.= 617
611.60	0.0	E < Inv.El.= 617
611.80	0.0	E < Inv.El.= 617
612.00	0.0	E < Inv.El.= 617
612.20	0.0	E < Inv.El.= 617
612.40	0.0	E < Inv.El.= 617
612.60	0.0	E < Inv.El.= 617
612.80	0.0	E < Inv.El.= 617
613.00	0.0	E < Inv.El.= 617
613.20	0.0	E < Inv.El.= 617
613.40	0.0	E < Inv.El.= 617
613.60	0.0	E < Inv.El.= 617
613.80	0.0	E < Inv.El.= 617
614.00	0.0	E < Inv.El.= 617
614.20	0.0	E < Inv.El.= 617
614.40	0.0	E < Inv.El.= 617
614.60	0.0	E < Inv.El.= 617
614.80	0.0	E < Inv.El.= 617
615.00	0.0	E < Inv.El.= 617
615.20	0.0	E < Inv.El.= 617
615.40	0.0	E < Inv.El.= 617
615.60	0.0	E < Inv.El.= 617
615.80	0.0	E < Inv.El.= 617
616.00	0.0	E < Inv.El.= 617
616.20	0.0	E < Inv.El.= 617
616.40	0.0	E < Inv.El.= 617
616.60	0.0	E < Inv.El.= 617

Outlet Structure File: 8861W .STR

POND-2 Version: 5.17

S/N:

Date Executed:

Time Executed:

>>>> CONTINUED from previous page <<<<<

Outflow Rating Table for Structure #3  
WEIR-VR Weir - Vertical Rectangular

\*\*\*\*\* INLET CONTROL ASSUMED \*\*\*\*\*

Elevation (ft)	Q (cfs)	Computation Messages
616.80	0.0	E < Inv.El.= 617
617.00	0.0	H =0.0
617.20	3.1	H =.2
617.40	8.9	H =.4
617.60	16.3	H =.6
617.80	25.1	H =.8
618.00	35.0	H =1.0

C = 3 L (ft) = 11.67

H (ft) = Table elev. - Invert elev. ( 617 ft )

Q (cfs) = C \* L \* (H\*\*1.5) -- Suppressed Weir

\*\*\*\*\*  
 INDIAN SPRINGS WEST BASIN

DETENTION ANALYSIS  
 PREPARED BY: BAX ENGINEERING CO., INC.  
 MARCH 5, 1997

\*\*\*\*\*

Outflow Rating Table for Structure #1  
 WEIR-VR Weir - Vertical Rectangular

\*\*\*\*\* INLET CONTROL ASSUMED \*\*\*\*\*

Elevation (ft)	Q (cfs)	Computation Messages
610.00	0.0	H =0.0
610.20	0.1	H =.2
610.40	0.4	H =.4
610.60	0.7	H =.6
610.80	1.1	H =.8
611.00	1.5	H =1.0
611.20	2.0	H =1.2
611.40	2.5	H =1.4
611.60	3.0	H =1.6
611.80	3.6	H =1.8
612.00	4.2	H =2.0
612.20	4.9	H =2.2
612.40	5.6	H =2.4
612.60	6.3	H =2.6
612.80	7.0	H =2.8
613.00	7.8	H =3.0
613.20	8.6	H =3.2
613.40	9.4	H =3.4
613.60	10.2	H =3.6
613.80	11.1	H =3.8
614.00	12.0	H =4.0
614.20	12.9	H =4.2
614.40	13.8	H =4.4
614.60	14.8	H =4.6
614.80	15.8	H =4.8
615.00	16.8	H =5.0
615.20	17.8	H =5.2
615.40	18.8	H =5.4
615.60	19.9	H =5.6
615.80	21.0	H =5.8
616.00	22.0	H =6.0
616.20	23.2	H =6.2
616.40	24.3	H =6.4
616.60	25.4	H =6.6



\*\*\*\*\*  
 INDIAN SPRINGS  
 DETENTION ANALYSIS  
 PREPARED BY: BAX ENGINEERING CO., INC.  
 MARCH 5, 1997  
 \*\*\*\*\*

WEIR-VR Weir - Vertical Rectangular  
 Outlet Rating Table for Structure #1

\*\*\*\*\* INLET CONTROL ASSUMED \*\*\*\*\*

Elevation (ft)	Q (cfs)	Computation Messages
810.00	0.0	H = 0.0
810.20	0.4	H = 2
810.40	0.4	H = 4
810.60	0.7	H = 6
810.80	1.1	H = 8
811.00	1.5	H = 10
811.20	2.0	H = 12
811.40	2.5	H = 14
811.60	3.0	H = 16
811.80	3.6	H = 18
812.00	4.2	H = 20
812.20	4.8	H = 22
812.40	5.4	H = 24
812.60	6.0	H = 26
812.80	7.0	H = 28
813.00	7.8	H = 30
813.20	8.6	H = 32
813.40	9.4	H = 34
813.60	10.2	H = 36
813.80	11.1	H = 38
814.00	12.0	H = 40
814.20	12.9	H = 42
814.40	13.8	H = 44
814.60	14.8	H = 46
814.80	15.8	H = 48
815.00	16.8	H = 50
815.20	17.8	H = 52
815.40	18.8	H = 54
815.60	19.8	H = 56
815.80	21.0	H = 58
816.00	22.0	H = 60
816.20	23.2	H = 62
816.40	24.4	H = 64
816.60	25.4	H = 66

>>>> CONTINUED from previous page <<<<<

Outflow Rating Table for Structure #1  
 WEIR-VR Weir - Vertical Rectangular

\*\*\*\*\* INLET CONTROL ASSUMED \*\*\*\*\*

Elevation (ft)	Q (cfs)	Computation Messages
616.80	26.6	H =6.8
617.00	27.8	H =7.0
617.20	29.0	H =7.2
617.40	30.2	H =7.400
617.60	31.4	H =7.6
617.80	32.7	H =7.8
618.00	33.9	H =8.0

$C = 3 \quad L \text{ (ft)} = .5$

$H \text{ (ft)} = \text{Table elev.} - \text{Invert elev. ( 610 ft )}$

$Q \text{ (cfs)} = C * L * (H^{**1.5})$  -- Suppressed Weir

\*\*\*\*\*  
INDIAN SPRINGS WEST BASIN

DETENTION ANALYSIS  
PREPARED BY: BAX ENGINEERING CO., INC.  
MARCH 5, 1997

\*\*\*\*\*

Outflow Rating Table for Structure #2  
ORIFICE Orifice - Based on Area and Datum Elevation

Elevation (ft)	Q (cfs)	Computation Messages
610.00	0.0	E < E1=611.00
610.20	0.0	E < E1=611.00
610.40	0.0	E < E1=611.00
610.60	0.0	E < E1=611.00
610.80	0.0	E < E1=611.00
611.00	1.7	H =.5
611.20	2.0	H =.7
611.40	2.3	H =.9
611.60	2.5	H =1.1
611.80	2.7	H =1.3
612.00	2.9	H =1.5
612.20	3.1	H =1.7
612.40	3.3	H =1.9
612.60	3.5	H =2.1
612.80	3.7	H =2.3
613.00	3.8	H =2.5
613.20	4.0	H =2.7
613.40	4.1	H =2.9
613.60	4.2	H =3.1
613.80	4.4	H =3.3
614.00	4.5	H =3.5
614.20	4.6	H =3.7
614.40	4.8	H =3.9
614.60	4.9	H =4.1
614.80	5.0	H =4.3
615.00	5.1	H =4.5
615.20	5.2	H =4.7
615.40	5.3	H =4.9
615.60	5.4	H =5.1
615.80	5.5	H =5.3
616.00	5.6	H =5.5
616.20	5.7	H =5.7
616.40	5.8	H =5.9
616.60	5.9	H =6.1

>>>> CONTINUED from previous page <<<<<

Outflow Rating Table for Structure #2  
 ORIFICE Orifice - Based on Area and Datum Elevation

Elevation (ft)	Q (cfs)	Computation Messages
616.80	6.0	H =6.3
617.00	6.1	H =6.5
617.20	6.2	H =6.7
617.40	6.3	H =6.9
617.60	6.4	H =7.1
617.80	6.5	H =7.3
618.00	6.6	H =7.5

C = .6      A = .5 sq.ft.

H (ft) = Table elev. - Datum elev. ( 610.5 ft )

Q (cfs) = C \* A \* sqrt(2g \* H)

\*\*\*\*\*  
 INDIAN SPRINGS WEST BASIN

DETENTION ANALYSIS  
 PREPARED BY: BAX ENGINEERING CO., INC.  
 MARCH 5, 1997

\*\*\*\*\*

Outflow Rating Table A  
 Table A = 1 ? 2

Elevation (ft)	Q (cfs)	Contributing Structures
610.00	0.0	1
610.20	0.1	1
610.40	0.4	1
610.60	0.7	1
610.80	1.1	1
611.00	1.5	1
611.20	2.0	1
611.40	2.3	2
611.60	2.5	2
611.80	2.7	2
612.00	2.9	2
612.20	3.1	2
612.40	3.3	2
612.60	3.5	2
612.80	3.7	2
613.00	3.8	2
613.20	4.0	2
613.40	4.1	2
613.60	4.2	2
613.80	4.4	2
614.00	4.5	2
614.20	4.6	2
614.40	4.8	2
614.60	4.9	2
614.80	5.0	2
615.00	5.1	2
615.20	5.2	2
615.40	5.3	2
615.60	5.4	2
615.80	5.5	2
616.00	5.6	2
616.20	5.7	2
616.40	5.8	2
616.60	5.9	2
616.80	6.0	2
617.00	6.1	2
617.20	6.2	2
617.40	6.3	2
617.60	6.4	2
617.80	6.5	2
618.00	6.6	2



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Need 5 yrs.

SEDIMENT STORAGE CALCULATIONS  
INDIAN SPRINGS - NORTH BASIN  
BAX PROJECT NO. 96-8861  
APRIL 11, 1997

Sediment storage will be provided by over excavation of the lake bottom. The following calculations are based on an attached nomograph provided by the City of O'Fallon.

Total disturbed area tributary to lake: 17.37 AC.  
Rational Method "C" Factor: 0.40%

FROM FIGURE 1:

The required volume for 1 year construction period:

$$117 \text{ Cu.Ft./Ac.} \times 17.37 \text{ Ac.} = 2,032 \text{ Cu.Ft.}$$

Volume Calculation:

ELEVATION	AREA	VOLUME	TOTAL VOLUME
602.0	10,038 s.f.	0 c.f.	0 c.f.
601.0	8,810 s.f.	9,424 c.f.	9,424 c.f.

Based on the above calculations the lake will be required to be over excavated 0.22' (2,073 c.f.) to provide storage for the anticipated sediment run-off.

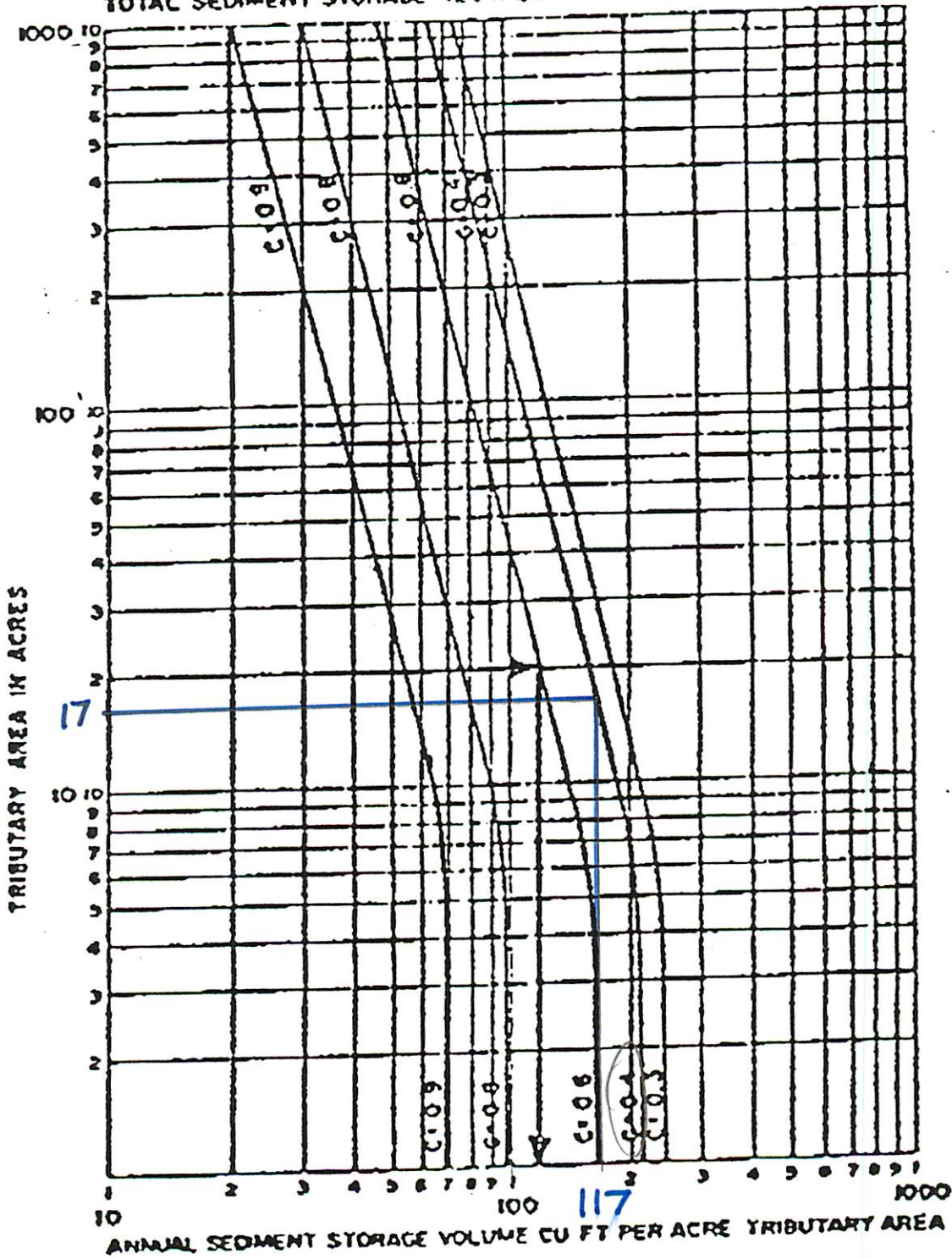
EXAMPLE:

TRIBUTARY AREA = 20 ACRES

RATIONAL METHOD RUNOFF COEFFICIENT "C" = 0.6

SEDIMENT STORAGE = 120 CU. FT. PER ACRE PER YEAR

TOTAL SEDIMENT STORAGE = 120 X 20 = 2400 CU. FT. PER YEAR.



ANNUAL SEDIMENT STORAGE

FIG. 1





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Need 5 yrs.

SEDIMENT STORAGE CALCULATIONS  
INDIAN SPRINGS - SOUTH BASIN  
BAX PROJECT NO. 96-8861  
APRIL 11, 1997

Sediment storage will be provided by over excavation of the lake bottom. The following calculations are based on an attached nomograph provided by the City of O'Fallon.

Total disturbed area tributary to lake: 14.29 AC.  
Rational Method "C" Factor: 0.40%

FROM FIGURE 1:

The required volume for 1 year construction period:

$$118 \text{ Cu.Ft./Ac.} \times 14.29 \text{ Ac.} = 1,686 \text{ Cu.Ft.}$$

Volume Calculation:

ELEVATION	AREA	VOLUME	TOTAL VOLUME
586.0	9,186 s.f.	0 c.f.	0 c.f.
585.0	8,000 s.f.	8,593 c.f.	8,593 c.f.

Based on the above calculations the lake will be required to be over excavated 0.20' (1,719 c.f.) to provide storage for the anticipated sediment run-off.



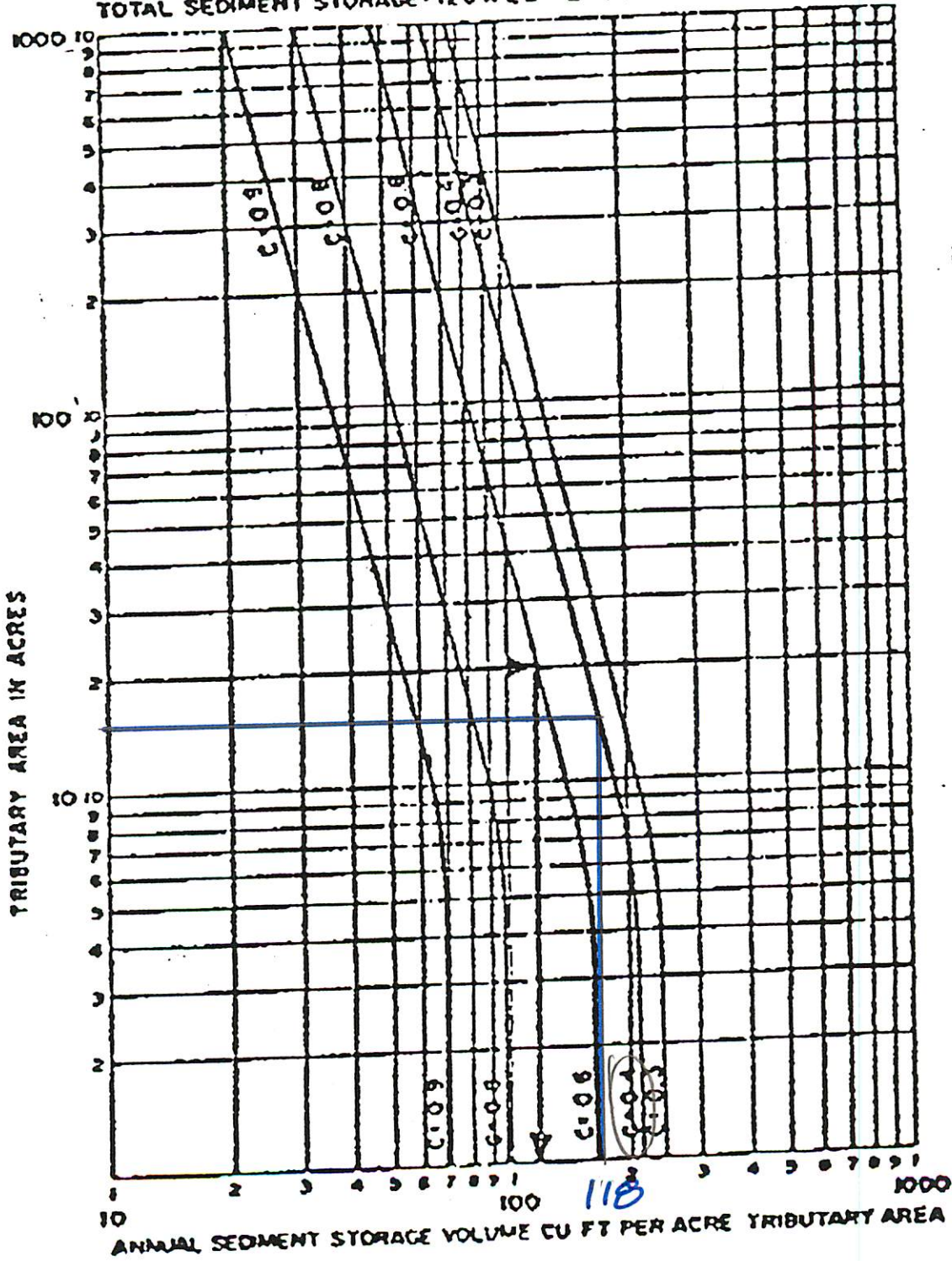
EXAMPLE:

TRIBUTARY AREA - 20 ACRES

RATIONAL METHOD RUNOFF COEFFICIENT "C" = 0.6

SEDIMENT STORAGE = 120 CU. FT. PER ACRE PER YEAR

TOTAL SEDIMENT STORAGE = 120 X 20 = 2400 CU. FT. PER YEAR.



ANNUAL SEDIMENT STORAGE

FIG. 1



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SURVEYING

Need 5 yrs.

SEDIMENT STORAGE CALCULATIONS  
INDIAN SPRINGS - WEST BASIN  
BAX PROJECT NO. 96-8861  
APRIL 11, 1997

Sediment storage will be provided by over excavation of the lake bottom. The following calculations are based on an attached nomograph provided by the City of O'Fallon.

Total disturbed area tributary to lake: 6.03 AC.  
Rational Method "C" Factor: 0.40%

FROM FIGURE 1:

The required volume for 1 year construction period:

$$120 \text{ Cu.Ft./Ac.} \times 6.03 \text{ Ac.} = 724 \text{ Cu.Ft.}$$

Volume Calculation:

ELEVATION	AREA	VOLUME	TOTAL VOLUME
612.0	3,319 s.f.	0 c.f.	0 c.f.
611.0	2,650 s.f.	2,985 c.f.	2,985 c.f.

Based on the above calculations the lake will be required to be over excavated 0.25' (746 c.f.) to provide storage for the anticipated sediment run-off.



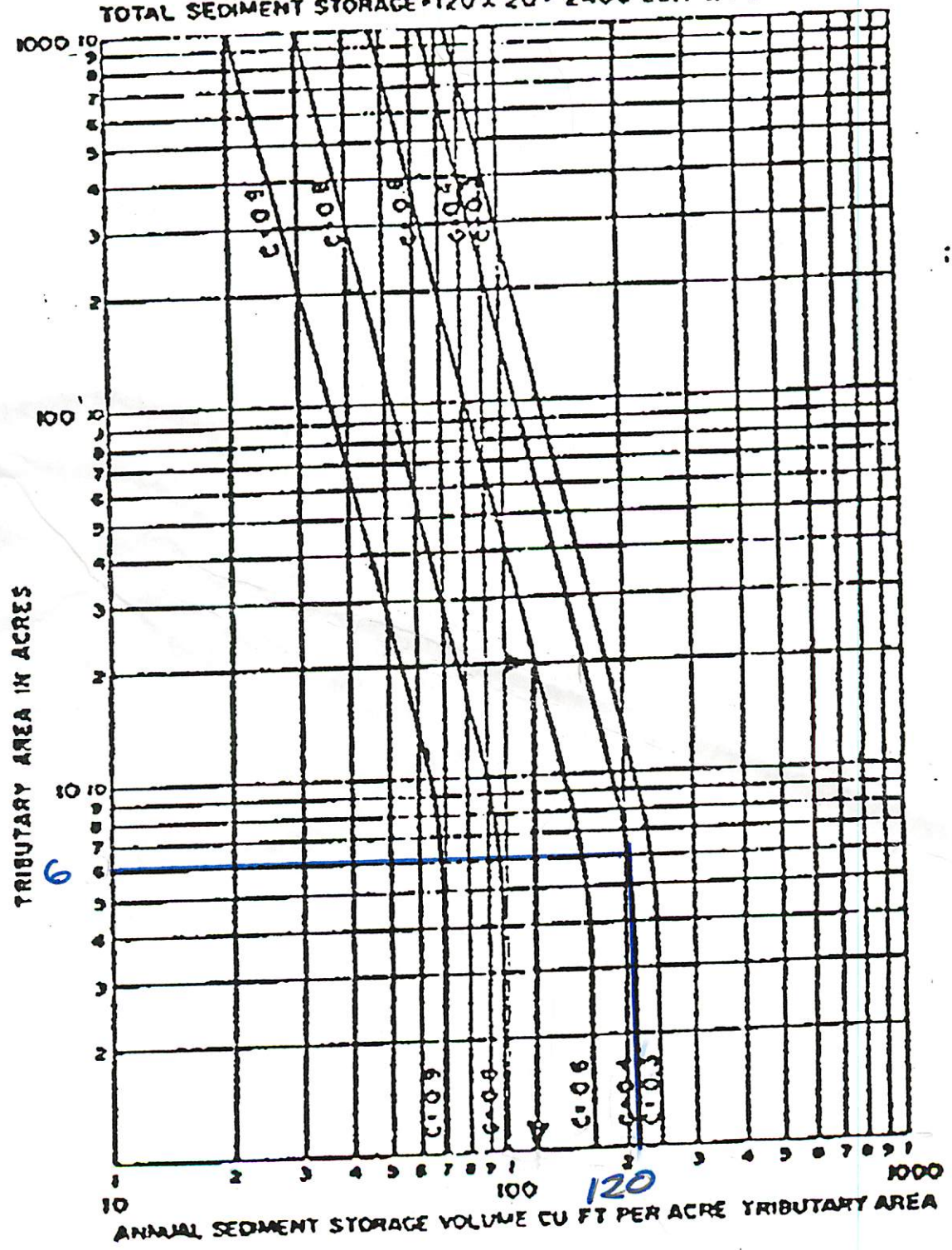
EXAMPLE:

TRIBUTARY AREA = 20 ACRES

RATIONAL METHOD RUNOFF COEFFICIENT "C" = 0.6

SEDIMENT STORAGE = 120 CU. FT. PER ACRE PER YEAR

TOTAL SEDIMENT STORAGE = 120 X 20 = 2400 CU. FT. PER YEAR.



ANNUAL SEDIMENT STORAGE

FIG. 1