



ENGINEERING

PLANNING

SURVEYING

STORMWATER DETENTION ANALYSIS  
PREPARED BY: BAX ENGINEERING CO., INC.  
**THE KNOLLS - O'FALLON**  
BAX PROJECT NO. 97-9197  
JANUARY 29, 1997

#### INTRODUCTION:

The tract of land is presently an undeveloped site located in the City of O'Fallon, Missouri. It is proposed that 31.67 acres of the 60.6 acre tract be developed into residential lots. A stormwater detention basin shall be constructed near the southwest corner of the site. This basin will provide detention for the development when considering the increased runoff for the entire site. The storage volume and outflow rates shall be proportioned to insure that the peak rate of runoff leaving the site under post-developed conditions is less than or equal to the peak rate of runoff leaving the site under pre-developed conditions for the 25 year-20 minute design storm. The basin was also analyzed for the 2, 15 and 100 year frequency - 20 minute duration design storms.

#### GENERAL SITE DATA AND RUNOFF CALCULATIONS:

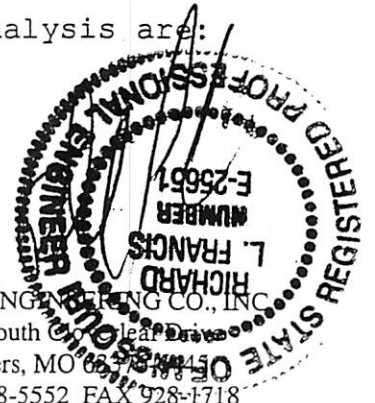
The pre-developed P.I. factors to be used for the analysis are:

2 year - 5% impervious	1.15 cfs/ac.
15 year - 5% impervious	1.87 cfs/ac.
25 year - 5% impervious	2.31 cfs/ac.
100 year - 5% impervious	2.95 cfs/ac.

The post-developed P.I. factors to be used for the analysis are:

2 year - 100% impervious	1.61 cfs/ac.
15 year - 100% impervious	2.64 cfs/ac.
25 year - 100% impervious	3.26 cfs/ac.
100 year - 100% impervious	4.17 cfs/ac.

BAX ENGINEERING CO., INC.  
1052 South Co. Clear Drive  
St. Peters, MO 65759  
314-928-5552 FAX 928-1718





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**TIME OF CONCENTRATION:**

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Of the inflows to the basin, the most remote point lies to the northeast near the intersection of McGwire Ct. and Cinnamon Teal Dr. Flows will travel approximately 400 feet overland to an inlet then 1200 feet via stormpipe to the detention basin. Time of concentration is estimated as follows:

A) T(overland) : L = 400 feet  
Elevation difference = 500 - 496 = 4 feet  
T(overland) = 9 minutes : See figure 1

B) T(stormpipe) : L = 1200 feet  
Elevation difference = 496 - 484 = 12 feet  
T(stormpipe) = 1.9 minutes : See figure 1

Total 10.9 min >> Use 10 min.

**BASIN PEAK INFLOWS:**

Inflows to the basin have been estimated from the drainage area map.

25 year-20 minute storm

$$13.06 \text{ Ac.} \times 3.26 \text{ cfs/Ac.} = 42.58 \text{ cfs}$$

2 year-20 minute storm:	21.03 cfs
15 year-20 minute storm:	34.48 cfs
100 year-20 minute storm:	54.46 cfs

**REQUIRED ATTENUATION:**

$$= \text{TRACT AREA} \times [\text{PI}(\text{post}) - \text{PI}(\text{pre})]$$

$$\begin{aligned} & 15 \text{ year-20 minute storm} \\ & 31.67 \times [ 3.26 - 2.31 ] = 30.09 \text{ cfs} \end{aligned}$$



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**PERMITTED RELEASE RATE:**

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The permitted release rate of the basin is found by subtracting the required attenuation from the peak basin inflow.

25 year-20 minute storm  
Permitted release rate:

$$42.58 \text{ cfs} - 30.09 \text{ cfs} = 12.49 \text{ cfs}$$

**STORM ROUTING CALCULATIONS AND RESULTS:**

A computer program was used in routing the design 25 year-20 minute storm through the basin. As found in the routing calculations, the results are as follows:

<u>20 MIN STORM</u>	<u>PERMITTED RELEASE RATE</u>	<u>CALCULATED RELEASE RATE</u>	<u>PEAK ELEVATION</u>
2 YR	-	1.57 cfs	482.98
15 YR	-	1.84 cfs	484.33
25 YR	12.49 cfs	1.99 cfs	485.05

As shown above, the calculated release rate of the design storm is less than the respective permitted release rate as required for the detention basin.

**CHECK 100 YEAR OUTFLOW: (low-flow blocked)**

$$\text{WEIR FLOW : } Q = C \times L \times H^{3/2}$$

where 100-YEAR FLOW Q = 54.46 cfs  
C = 3.32  
48" standpipe L = 12.57 ft  
H = 1.19 ft

sill = 485.25  
100 yr h/w = 486.44



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**SUMMARY :**

*SURVEYING*

25 year-20min H.W.	485.05
100 year-20min H.W. (low flow blocked)	486.44
Low Flow Slot	4" wide x 6" high
Low Flow Slot Elevation	479.12
Overflow Standpipe Elevation	485.25
Top Of Berm	494.00



Project: THE KNOLLS

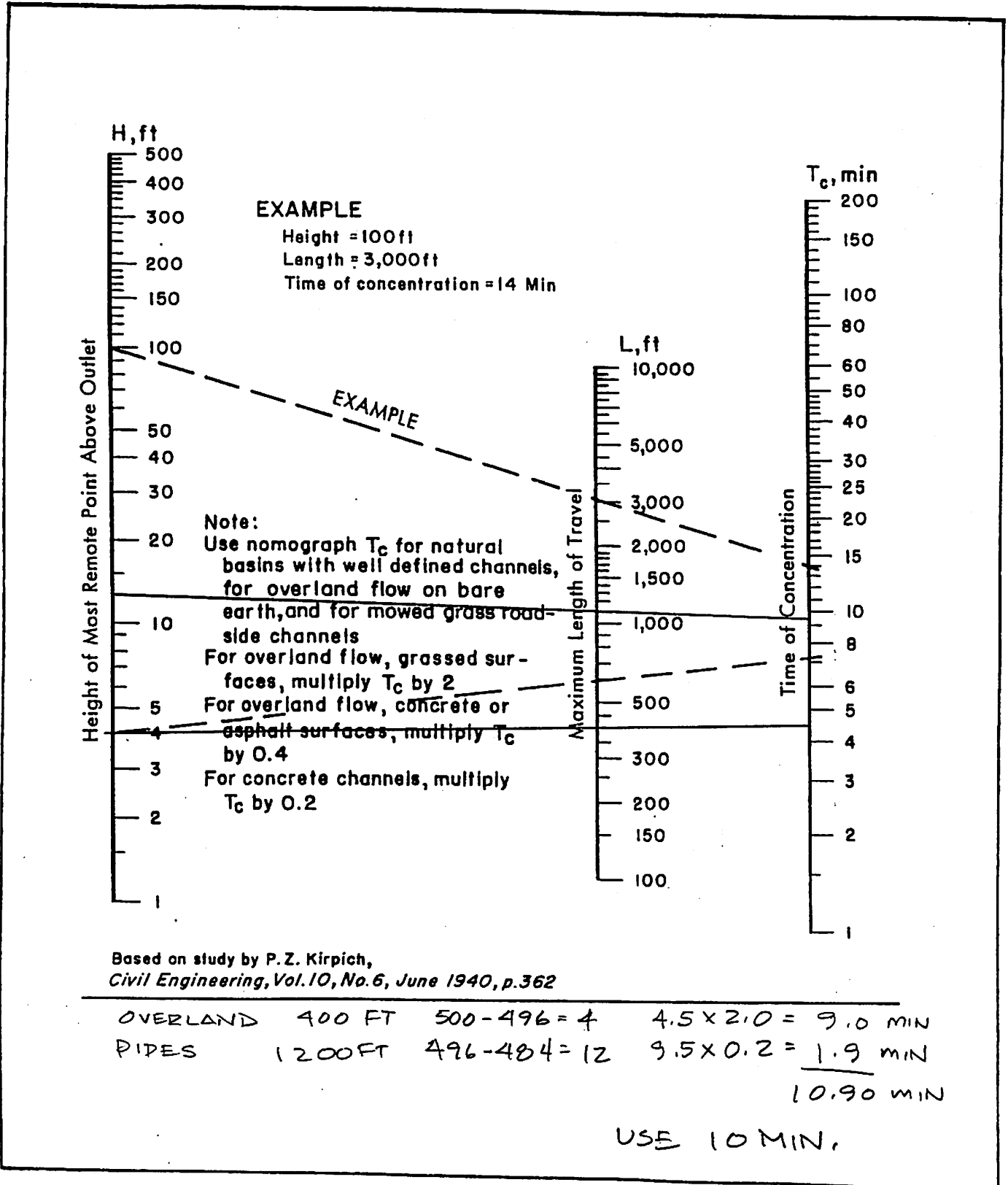
Date: 1-5-98

Project No: 97-9197

Designed: ADJ

Checked: \_\_\_\_\_

FIGURE 1





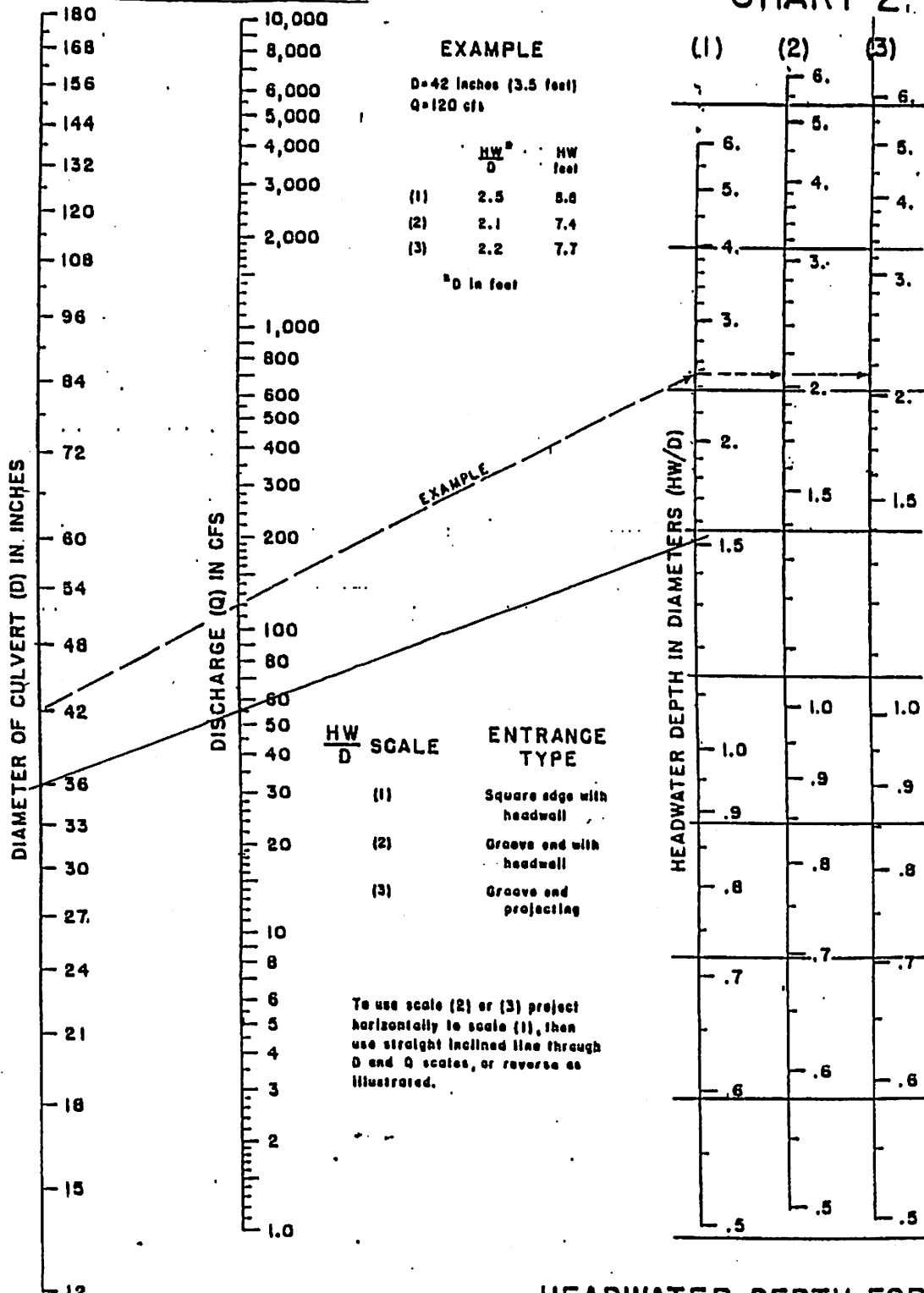
Project: THE KNOLLS

Date: 1-5-98 Project No: 97-9197

Designed: AD) Checked: \_\_\_\_\_

CHECK OUTFLOW PIPE

CHART 2



HEADWATER DEPTH FOR CONCRETE PIPE CULVERTS WITH INLET CONTROL

HEADWATER SCALES 2&3  
REVISED MAY 1964

BUREAU OF PUBLIC ROADS JAN. 1963

1052 South Cloverleaf Drive  
St. Peters, MO 63376-6445  
314-928-5552 FAX 928-1718

36" x 1.5 = 4.5'

< 485.25

AK

The Knolls  
DETENTION ANALYSIS  
BAX ENGINEERING CO. INC.  
JANUARY 5, 1998

CALCULATED 01-30-1998 13:44:41  
DISK FILE: C:\WINDOWS\DESKTOP\PONDPA~1\9197 .VOL

Planimeter scale: 1 inch = 1 ft.

Elevation (ft)	Planimeter (sq.in.)	Area (acres)	$A1+A2+\text{sqr}(A1*A2)$ (acres)	* Volume (acre-ft)	Volume Sum (acre-ft)
479.12	0.00	0.00	0.00	0.00	0.00
480.00	3,396.00	0.08	0.08	0.02	0.02
482.00	9,419.00	0.22	0.42	0.28	0.31
484.00	12,188.00	0.28	0.74	0.49	0.80
486.00	15,194.00	0.35	0.94	0.63	1.43
488.00	18,476.00	0.42	1.16	0.77	2.20
490.00	22,022.00	0.51	1.39	0.93	3.13
492.00	25,987.00	0.60	1.65	1.10	4.23
494.00	30,188.00	0.69	1.93	1.29	5.52

\* Incremental volume computed by the Conic Method for Reservoir Volumes.

$$\text{Volume} = (1/3) * (\text{EL2}-\text{EL1}) * (\text{Area1} + \text{Area2} + \text{sq.rt.}(\text{Area1}*\text{Area2}))$$

where: EL1, EL2 = Lower and upper elevations of the increment  
 Area1, Area2 = Areas computed for EL1, EL2, respectively  
 Volume = Incremental volume between EL1 and EL2

Outlet Structure File: 9197 .STR

POND-2 Version: 5.20  
Date Executed:

S/N:  
Time Executed:

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DETENTION ANALYSIS  
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JANUARY 5, 1998  
\*\*\*\*\*

\*\*\*\*\* COMPOSITE OUTFLOW SUMMARY \*\*\*\*\*

<u>Elevation (ft)</u>	<u>Q (cfs)</u>	<u>Contributing Structures</u>
479.12	0.0	1
479.62	0.4	1
480.12	0.7	2
480.62	0.9	2
481.12	1.1	2
481.62	1.2	2
482.12	1.4	2
482.62	1.5	2
483.12	1.6	2
483.62	1.7	2
484.12	1.8	2
484.62	1.9	2
485.12	2.0	2
485.62	2.0	2
486.12	2.1	2
486.62	2.2	2
487.12	2.3	2
487.62	2.4	2
488.12	2.4	2
488.62	2.5	2
489.12	2.6	2
489.62	2.6	2
490.12	2.7	2
490.62	2.7	2
491.12	2.8	2
491.62	2.9	2
492.12	2.9	2
492.62	3.0	2
493.12	3.0	2
493.62	3.1	2
494.00	3.1	2



Outlet Structure File: 9197 .STR

POND-2 Version: 5.20  
Date Executed:

S/N:  
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JANUARY 5, 1998  
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Outlet Structure File: C:\WINDOWS\DESKTOP\PONDPA~1\9197 .STR  
Planimeter Input File: C:\WINDOWS\DESKTOP\PONDPA~1\9197 .VOL  
Rating Table Output File: C:\WINDOWS\DESKTOP\PONDPA~1\9197 .PND

Min. Elev.(ft) = 479.12 Max. Elev.(ft) = 494 Incr.(ft) = .5

Additional elevations (ft) to be included in table:  
\*\*\*\*\*

\*\*\*\*\*  
SYSTEM CONNECTIVITY  
\*\*\*\*\*

Structure	No.	Q Table	Q Table
-----	---	-----	-----
WEIR-VR	1		-> 1
ORIFICE	2	? 1	-> A

Outflow rating table summary was stored in file:  
C:\WINDOWS\DESKTOP\PONDPA~1\9197 .PND

Outlet Structure File: 9197 .STR

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

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DETENTION ANALYSIS  
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JANUARY 5, 1998  
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>>>>> Structure No. 1 <<<<<<  
(Input Data)

WEIR-VR

Weir - Vertical Rectangular

E1 elev.(ft)?	479.12
E2 elev.(ft)?	494.001
Weir coefficient?	3
Weir elev.(ft)?	479.12
Length (ft)?	.3333333
Contracted/Suppressed (C/S)?	S

Outlet Structure File: 9197 .STR

POND-2 Version: 5.20

S/N:

Date Executed:

Time Executed:

\*\*\*\*\*  
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DETENTION ANALYSIS  
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JANUARY 5, 1998  
\*\*\*\*\*

>>>>> Structure No. 2 <<<<<<  
(Input Data)

ORIFICE

Orifice - Based on Area and Datum Elevation

E1 elev.(ft)?	479.62
E2 elev.(ft)?	494.001
Orifice coeff.?	0.6
Invert elev.(ft)?	479.120
Datum elev.(ft) ?	479.3700
Orifice area (sq ft)?	0.17000

Outlet Structure File: 9197 .STR

POND-2 Version: 5.20  
Date Executed:

S/N:  
Time Executed:

\*\*\*\*\*  
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\*\*\*\*\*

Outflow Rating Table for Structure #1  
WEIR-VR Weir - Vertical Rectangular

\*\*\*\*\* INLET CONTROL ASSUMED \*\*\*\*\*

Elevation (ft)	Q (cfs)	Computation Messages
479.12	0.0	H =0.0
479.62	0.4	H =.5
480.12	1.0	H =1.0
480.62	1.8	H =1.5
481.12	2.8	H =2.0
481.62	4.0	H =2.5
482.12	5.2	H =3.0
482.62	6.5	H =3.5
483.12	8.0	H =4.0
483.62	9.5	H =4.5
484.12	11.2	H =5.0
484.62	12.9	H =5.5
485.12	14.7	H =6.0
485.62	16.6	H =6.5
486.12	18.5	H =7.0
486.62	20.5	H =7.5
487.12	22.6	H =8.0
487.62	24.8	H =8.5
488.12	27.0	H =9.0
488.62	29.3	H =9.5
489.12	31.6	H =10.0
489.62	34.0	H =10.5
490.12	36.5	H =11.0
490.62	39.0	H =11.5
491.12	41.6	H =12.0
491.62	44.2	H =12.5
492.12	46.9	H =13.0
492.62	49.6	H =13.5
493.12	52.4	H =14.0
493.62	55.2	H =14.5
494.00	57.4	H =14.88

C = 3 L (ft) = .3333333  
H (ft) = Table elev. - Invert elev. ( 479.12 ft )  
Q (cfs) = C \* L \* (H\*\*1.5) -- Suppressed Weir

Outlet Structure File: 9197 .STR

POND-2 Version: 5.20  
Date Executed:

S/N:  
Time Executed:

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JANUARY 5, 1998  
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Outflow Rating Table for Structure #2  
ORIFICE Orifice - Based on Area and Datum Elevation

Elevation (ft)	Q (cfs)	Computation Messages
479.12	0.0	E < E1=479.62
479.62	0.4	H =.25
480.12	0.7	H =.750
480.62	0.9	H =1.25
481.12	1.1	H =1.75
481.62	1.2	H =2.25
482.12	1.4	H =2.75
482.62	1.5	H =3.25
483.12	1.6	H =3.75
483.62	1.7	H =4.25
484.12	1.8	H =4.75
484.62	1.9	H =5.25
485.12	2.0	H =5.75
485.62	2.0	H =6.25
486.12	2.1	H =6.75
486.62	2.2	H =7.25
487.12	2.3	H =7.75
487.62	2.4	H =8.25
488.12	2.4	H =8.75
488.62	2.5	H =9.25
489.12	2.6	H =9.75
489.62	2.6	H =10.25
490.12	2.7	H =10.75
490.62	2.7	H =11.25
491.12	2.8	H =11.75
491.62	2.9	H =12.25
492.12	2.9	H =12.75
492.62	3.0	H =13.25
493.12	3.0	H =13.75
493.62	3.1	H =14.25
494.00	3.1	H =14.63

C = .6      A = .17 sq.ft.  
H (ft) = Table elev. - Datum elev. ( 479.37 ft )  
Q (cfs) = C \* A \* sqrt(2g \* H)

Outlet Structure File: 9197 .STR

POND-2 Version: 5.20  
Date Executed:

S/N:  
Time Executed:

\*\*\*\*\*  
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PREPARED BY: BAX ENGINEERING CO., INC.  
JANUARY 5, 1998  
\*\*\*\*\*

Outflow Rating Table A  
Table A = 1 ? 2

Elevation (ft)	Q (cfs)	Contributing Structures
479.12	0.0	1
479.62	0.4	1
480.12	0.7	2
480.62	0.9	2
481.12	1.1	2
481.62	1.2	2
482.12	1.4	2
482.62	1.5	2
483.12	1.6	2
483.62	1.7	2
484.12	1.8	2
484.62	1.9	2
485.12	2.0	2
485.62	2.0	2
486.12	2.1	2
486.62	2.2	2
487.12	2.3	2
487.62	2.4	2
488.12	2.4	2
488.62	2.5	2
489.12	2.6	2
489.62	2.6	2
490.12	2.7	2
490.62	2.7	2
491.12	2.8	2
491.62	2.9	2
492.12	2.9	2
492.62	3.0	2
493.12	3.0	2
493.62	3.1	2
494.00	3.1	2

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*
*           THE KNOLLS
*         DETENTION ANALYSIS
*   PREPARED BY: BAX ENGINEERING CO., INC.
*           JANUARY 5, 1998
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Inflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\9197-025.HYD  
 Rating Table file: C:\WINDOWS\DESKTOP\PONDPA~1\9197 .PND

----INITIAL CONDITIONS----  
 Elevation = 479.12 ft  
 Outflow = 0.00 cfs  
 Storage = 0.00 ac-ft

GIVEN POND DATA

ELEVATION (ft)	OUTFLOW (cfs)	STORAGE (ac-ft)
479.12	0.0	0.000
479.62	0.4	0.004
480.12	0.7	0.033
480.62	0.9	0.082
481.12	1.1	0.147
481.62	1.2	0.229
482.12	1.4	0.332
482.62	1.5	0.445
483.12	1.6	0.567
483.62	1.7	0.696
484.12	1.8	0.834
484.62	1.9	0.980
485.12	2.0	1.134
485.62	2.0	1.298
486.12	2.1	1.470
486.62	2.2	1.651
487.12	2.3	1.841
487.62	2.4	2.041
488.12	2.4	2.250
488.62	2.5	2.470
489.12	2.6	2.699
489.62	2.6	2.939
490.12	2.7	3.189
490.62	2.7	3.450
491.12	2.8	3.722
491.62	2.9	4.005
492.12	2.9	4.301
492.62	3.0	4.608
493.12	3.0	4.926
493.62	3.1	5.257
494.00	3.1	5.517

INTERMEDIATE ROUTING  
 COMPUTATIONS

2S/t (cfs)	2S/t + 0 (cfs)
0.0	0.0
6.1	6.5
47.3	48.0
118.9	119.8
213.1	214.2
333.2	334.4
481.7	483.1
646.7	648.2
823.1	824.7
1011.1	1012.8
1211.0	1212.8
1423.0	1424.9
1647.3	1649.3
1884.1	1886.1
2134.0	2136.1
2396.9	2399.1
2673.3	2675.6
2963.4	2965.8
3267.7	3270.1
3586.2	3588.7
3919.2	3921.8
4267.0	4269.6
4630.1	4632.8
5009.0	5011.7
5404.1	5406.9
5815.8	5818.7
6244.5	6247.4
6690.1	6693.1
7153.1	7156.1
7633.6	7636.7
8010.8	8013.9

Time increment (t) = 1.0 min.

Pond File: C:\WINDOWS\DESKTOP\PONDPA~1\9197 .PND  
 Inflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\9197-025.HYD  
 Outflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\91970025.HYD

INFLOW HYDROGRAPH

ROUTING COMPUTATIONS

TIME (min)	INFLOW (cfs)	I1+I2 (cfs)	2S/t - 0 (cfs)	2S/t + 0 (cfs)	OUTFLOW (cfs)	ELEVATION (ft)
0.0	0.00	---	0.0	0.0	0.00	479.12
1.0	4.30	4.3	3.8	4.3	0.27	479.45
2.0	8.50	12.8	15.6	16.6	0.47	479.74
3.0	12.80	21.3	35.7	36.9	0.62	479.99
4.0	17.00	29.8	64.0	65.5	0.75	480.24
5.0	21.30	38.3	100.6	102.3	0.85	480.50
6.0	25.49	46.8	145.5	147.4	0.96	480.77
7.0	29.79	55.3	198.6	200.7	1.07	481.05
8.0	34.09	63.9	260.2	262.5	1.14	481.32
9.0	38.29	72.4	330.2	332.6	1.20	481.61
10.0	42.59	80.9	408.5	411.1	1.30	481.88
11.0	42.60	85.2	490.8	493.6	1.41	482.15
12.0	42.60	85.2	573.1	576.0	1.46	482.40
13.0	42.60	85.2	655.3	658.3	1.51	482.65
14.0	42.60	85.2	737.4	740.5	1.55	482.88
15.0	42.60	85.2	819.4	822.6	1.60	483.11
16.0	42.60	85.2	901.3	904.6	1.64	483.33
17.0	42.60	85.2	983.1	986.5	1.69	483.55
18.0	42.60	85.2	1064.9	1068.3	1.73	483.76
19.0	42.60	85.2	1146.6	1150.1	1.77	483.96
20.0	42.60	85.2	1228.1	1231.8	1.81	484.16
21.0	38.32	80.9	1305.4	1309.1	1.85	484.35
22.0	34.12	72.4	1374.0	1377.8	1.88	484.51
23.0	29.82	63.9	1434.2	1438.0	1.91	484.65
24.0	25.52	55.3	1485.7	1489.5	1.93	484.76
25.0	21.32	46.8	1528.6	1532.5	1.95	484.86
26.0	17.02	38.3	1563.0	1566.9	1.96	484.94
27.0	12.82	29.8	1588.9	1592.9	1.97	484.99
28.0	8.52	21.3	1606.3	1610.2	1.98	485.03
29.0	4.32	12.8	1615.1	1619.1	1.99	485.05
30.0	0.03	4.4	1615.5	1619.5	1.99	485.05
31.0	0.00	0.0	1611.6	1615.6	1.98	485.04
32.0	0.00	0.0	1607.6	1611.6	1.98	485.04
33.0	0.00	0.0	1603.7	1607.6	1.98	485.03
34.0	0.00	0.0	1599.7	1603.7	1.98	485.02
35.0	0.00	0.0	1595.7	1599.7	1.98	485.01
36.0	0.00	0.0	1591.8	1595.7	1.98	485.00
37.0	0.00	0.0	1587.8	1591.8	1.97	484.99
38.0	0.00	0.0	1583.9	1587.8	1.97	484.98
39.0	0.00	0.0	1580.0	1583.9	1.97	484.97
40.0	0.00	0.0	1576.0	1580.0	1.97	484.97
41.0	0.00	0.0	1572.1	1576.0	1.97	484.96
42.0	0.00	0.0	1568.1	1572.1	1.97	484.95
43.0	0.00	0.0	1564.2	1568.1	1.96	484.94
44.0	0.00	0.0	1560.3	1564.2	1.96	484.93



Pond File: C:\WINDOWS\DESKTOP\PONDPA~1\9197 .PND  
 Inflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\9197-025.HYD  
 Outflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\91970025.HYD

INFLOW HYDROGRAPH

ROUTING COMPUTATIONS

TIME (min)	INFLOW (cfs)	I1+I2 (cfs)	2S/t - 0 (cfs)	2S/t + 0 (cfs)	OUTFLOW (cfs)	ELEVATION (ft)
45.0	0.00	0.0	1556.4	1560.3	1.96	484.92
46.0	0.00	0.0	1552.5	1556.4	1.96	484.91
47.0	0.00	0.0	1548.5	1552.5	1.96	484.90
48.0	0.00	0.0	1544.6	1548.5	1.96	484.90
49.0	0.00	0.0	1540.7	1544.6	1.95	484.89
50.0	0.00	0.0	1536.8	1540.7	1.95	484.88
51.0	0.00	0.0	1532.9	1536.8	1.95	484.87
52.0	0.00	0.0	1529.0	1532.9	1.95	484.86
53.0	0.00	0.0	1525.1	1529.0	1.95	484.85
54.0	0.00	0.0	1521.2	1525.1	1.94	484.84
55.0	0.00	0.0	1517.4	1521.2	1.94	484.83
56.0	0.00	0.0	1513.5	1517.4	1.94	484.83
57.0	0.00	0.0	1509.6	1513.5	1.94	484.82
58.0	0.00	0.0	1505.7	1509.6	1.94	484.81
59.0	0.00	0.0	1501.9	1505.7	1.94	484.80
60.0	0.00	0.0	1498.0	1501.9	1.93	484.79
61.0	0.00	0.0	1494.1	1498.0	1.93	484.78
62.0	0.00	0.0	1490.3	1494.1	1.93	484.77
63.0	0.00	0.0	1486.4	1490.3	1.93	484.77
64.0	0.00	0.0	1482.5	1486.4	1.93	484.76
65.0	0.00	0.0	1478.7	1482.5	1.93	484.75
66.0	0.00	0.0	1474.8	1478.7	1.92	484.74
67.0	0.00	0.0	1471.0	1474.8	1.92	484.73
68.0	0.00	0.0	1467.2	1471.0	1.92	484.72
69.0	0.00	0.0	1463.3	1467.2	1.92	484.71
70.0	0.00	0.0	1459.5	1463.3	1.92	484.71
71.0	0.00	0.0	1455.7	1459.5	1.92	484.70
72.0	0.00	0.0	1451.8	1455.7	1.91	484.69
73.0	0.00	0.0	1448.0	1451.8	1.91	484.68
74.0	0.00	0.0	1444.2	1448.0	1.91	484.67
75.0	0.00	0.0	1440.4	1444.2	1.91	484.66
76.0	0.00	0.0	1436.6	1440.4	1.91	484.65
77.0	0.00	0.0	1432.7	1436.6	1.91	484.65
78.0	0.00	0.0	1428.9	1432.7	1.90	484.64
79.0	0.00	0.0	1425.1	1428.9	1.90	484.63
80.0	0.00	0.0	1421.3	1425.1	1.90	484.62
81.0	0.00	0.0	1417.5	1421.3	1.90	484.61
82.0	0.00	0.0	1413.7	1417.5	1.90	484.60
83.0	0.00	0.0	1410.0	1413.7	1.89	484.59
84.0	0.00	0.0	1406.2	1410.0	1.89	484.58
85.0	0.00	0.0	1402.4	1406.2	1.89	484.58
86.0	0.00	0.0	1398.6	1402.4	1.89	484.57
87.0	0.00	0.0	1394.8	1398.6	1.89	484.56
88.0	0.00	0.0	1391.1	1394.8	1.89	484.55
89.0	0.00	0.0	1387.3	1391.1	1.88	484.54

\*\*\*\*\* SUMMARY OF ROUTING COMPUTATIONS \*\*\*\*\*

Pond File: C:\WINDOWS\DESKTOP\PONDPA~1\9197 .PND  
Inflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\9197-025.HYD  
Outflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\91970025.HYD

Starting Pond W.S. Elevation = 479.12 ft

\*\*\*\*\* Summary of Peak Outflow and Peak Elevation \*\*\*\*\*

Peak Inflow = 42.60 cfs  
Peak Outflow = 1.99 cfs  
Peak Elevation = 485.05 ft

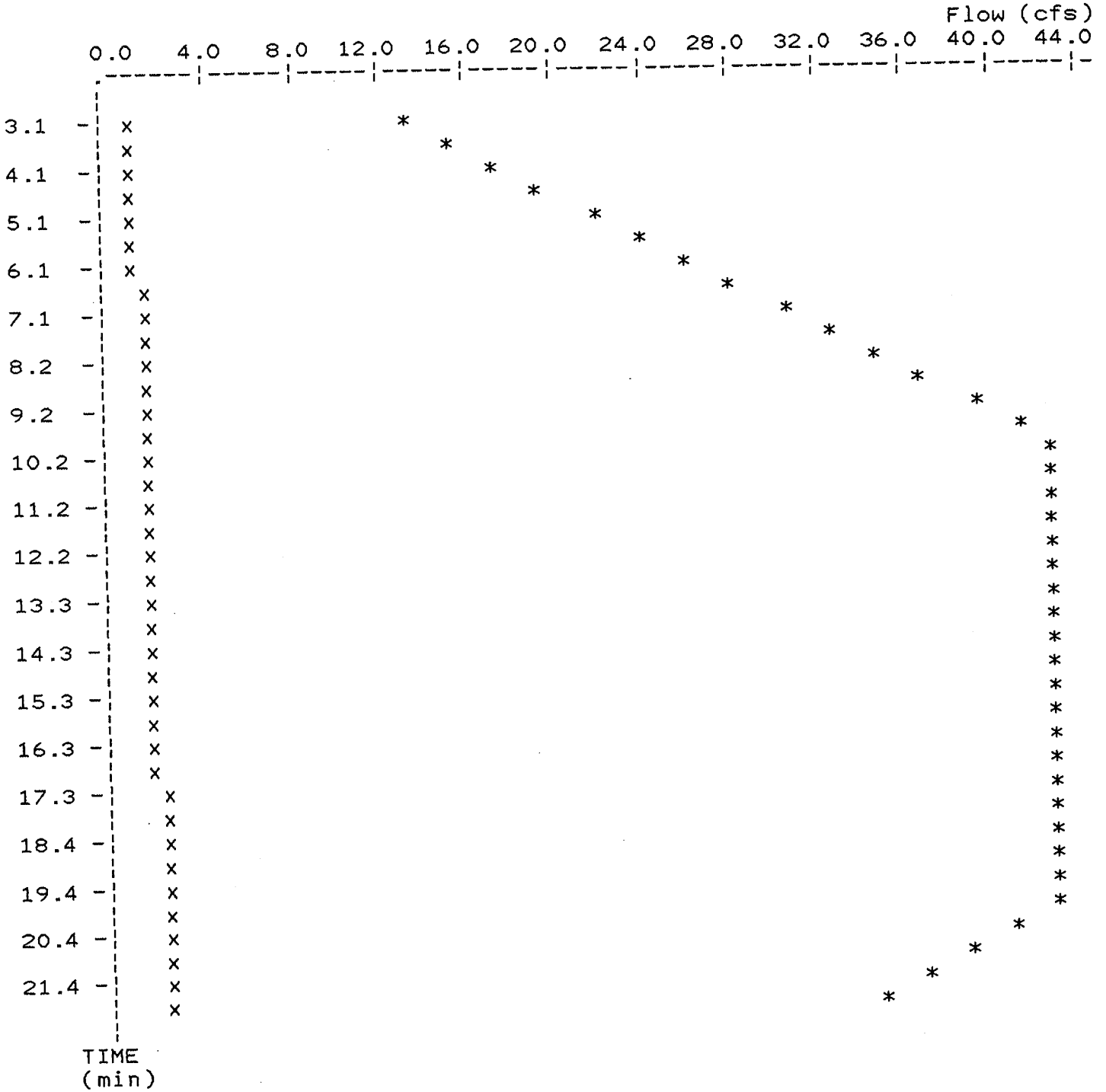
\*\*\*\*\* Summary of Approximate Peak Storage \*\*\*\*\*

Initial Storage = 0.00 ac-ft  
Peak Storage From Storm = 1.11 ac-ft  
-----  
Total Storage in Pond = 1.11 ac-ft

Pond File: C:\WINDOWS\DESKTOP\PONDPA~1\9197 .PND  
 Inflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\9197-025.HYD  
 Outflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\91970025.HYD

EXECUTED: 01-30-1998  
 14:14:21

Peak Inflow = 42.60 cfs  
 Peak Outflow = 1.99 cfs  
 Peak Elevation = 485.05 ft



x File: C:\WINDOWS\DESKTOP\PONDPA~1\91970025.HYD Qmax = 2.0 cfs  
 \* File: C:\WINDOWS\DESKTOP\PONDPA~1\9197-025.HYD Qmax = 42.6 cfs

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*****
*
*           THE KNOLLS
*         DETENTION ANALYSIS
*   PREPARED BY: BAX ENGINEERING CO., INC.
*           JANUARY 5, 1998
*
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Inflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\9197-015.HYD  
 Rating Table file: C:\WINDOWS\DESKTOP\PONDPA~1\9197 .PND

----INITIAL CONDITIONS----  
 Elevation = 479.12 ft  
 Outflow = 0.00 cfs  
 Storage = 0.00 ac-ft

GIVEN POND DATA			INTERMEDIATE ROUTING COMPUTATIONS	
ELEVATION (ft)	OUTFLOW (cfs)	STORAGE (ac-ft)	2S/t (cfs)	2S/t + 0 (cfs)
479.12	0.0	0.000	0.0	0.0
479.62	0.4	0.004	6.1	6.5
480.12	0.7	0.033	47.3	48.0
480.62	0.9	0.082	118.9	119.8
481.12	1.1	0.147	213.1	214.2
481.62	1.2	0.229	333.2	334.4
482.12	1.4	0.332	481.7	483.1
482.62	1.5	0.445	646.7	648.2
483.12	1.6	0.567	823.1	824.7
483.62	1.7	0.696	1011.1	1012.8
484.12	1.8	0.834	1211.0	1212.8
484.62	1.9	0.980	1423.0	1424.9
485.12	2.0	1.134	1647.3	1649.3
485.62	2.0	1.298	1884.1	1886.1
486.12	2.1	1.470	2134.0	2136.1
486.62	2.2	1.651	2396.9	2399.1
487.12	2.3	1.841	2673.3	2675.6
487.62	2.4	2.041	2963.4	2965.8
488.12	2.4	2.250	3267.7	3270.1
488.62	2.5	2.470	3586.2	3588.7
489.12	2.6	2.699	3919.2	3921.8
489.62	2.6	2.939	4267.0	4269.6
490.12	2.7	3.189	4630.1	4632.8
490.62	2.7	3.450	5009.0	5011.7
491.12	2.8	3.722	5404.1	5406.9
491.62	2.9	4.005	5815.8	5818.7
492.12	2.9	4.301	6244.5	6247.4
492.62	3.0	4.608	6690.1	6693.1
493.12	3.0	4.926	7153.1	7156.1
493.62	3.1	5.257	7633.6	7636.7
494.00	3.1	5.517	8010.8	8013.9

Time increment (t) = 1.0 min.

Pond File: C:\WINDOWS\DESKTOP\PONDPA~1\9197 .PND  
 Inflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\9197-015.HYD  
 Outflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\91970015.HYD

ROUTING COMPUTATIONS

INFLOW HYDROGRAPH

TIME (min)	INFLOW (cfs)	I1+I2 (cfs)	2S/t - 0 (cfs)	2S/t + 0 (cfs)	OUTFLOW (cfs)	ELEVATION (ft)
0.0	0.00		0.0	0.0	0.00	479.12
1.0	3.48	3.5	3.1	3.5	0.21	479.39
2.0	6.88	10.4	12.5	13.4	0.45	479.70
3.0	10.36	17.2	28.6	29.8	0.57	479.90
4.0	13.76	24.1	51.3	52.7	0.71	480.15
5.0	17.24	31.0	80.7	82.3	0.80	480.36
6.0	20.63	37.9	116.8	118.6	0.90	480.61
7.0	24.12	44.8	159.6	161.5	0.99	480.84
8.0	27.60	51.7	209.1	211.3	1.09	481.10
9.0	31.00	58.6	265.4	267.7	1.14	481.34
10.0	34.48	65.5	328.5	330.9	1.20	481.61
11.0	34.48	69.0	394.9	397.5	1.28	481.83
12.0	34.48	69.0	461.1	463.8	1.37	482.06
13.0	34.48	69.0	527.2	530.1	1.43	482.26
14.0	34.48	69.0	593.2	596.2	1.47	482.46
15.0	34.48	69.0	659.2	662.2	1.51	482.66
16.0	34.48	69.0	725.0	728.1	1.55	482.85
17.0	34.48	69.0	790.8	794.0	1.58	483.03
18.0	34.48	69.0	856.6	859.8	1.62	483.21
19.0	34.48	69.0	922.2	925.5	1.65	483.39
20.0	34.48	69.0	987.8	991.2	1.69	483.56
21.0	31.02	65.5	1049.9	1053.3	1.72	483.72
22.0	27.62	58.6	1105.0	1108.5	1.75	483.86
23.0	24.14	51.8	1153.2	1156.8	1.77	483.98
24.0	20.66	44.8	1194.4	1198.0	1.79	484.08
25.0	17.25	37.9	1228.7	1232.3	1.81	484.17
26.0	13.78	31.0	1256.1	1259.7	1.82	484.23
27.0	10.37	24.2	1276.6	1280.3	1.83	484.28
28.0	6.90	17.3	1290.2	1293.9	1.84	484.31
29.0	3.49	10.4	1296.9	1300.6	1.84	484.33
30.0	0.02	3.5	1296.7	1300.4	1.84	484.33
31.0	0.00	0.0	1293.1	1296.7	1.84	484.32
32.0	0.00	0.0	1289.4	1293.1	1.84	484.31
33.0	0.00	0.0	1285.7	1289.4	1.84	484.30
34.0	0.00	0.0	1282.0	1285.7	1.83	484.29
35.0	0.00	0.0	1278.4	1282.0	1.83	484.28
36.0	0.00	0.0	1274.7	1278.4	1.83	484.27
37.0	0.00	0.0	1271.1	1274.7	1.83	484.27
38.0	0.00	0.0	1267.4	1271.1	1.83	484.26
39.0	0.00	0.0	1263.7	1267.4	1.83	484.25
40.0	0.00	0.0	1260.1	1263.7	1.82	484.24
41.0	0.00	0.0	1256.5	1260.1	1.82	484.23
42.0	0.00	0.0	1252.8	1256.5	1.82	484.22
43.0	0.00	0.0	1249.2	1252.8	1.82	484.21
44.0	0.00	0.0	1245.5	1249.2	1.82	484.21

Pond File: C:\WINDOWS\DESKTOP\PONDPA~1\9197 .PND  
 Inflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\9197-015.HYD  
 Outflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\91970015.HYD

INFLOW HYDROGRAPH

TIME (min)	INFLOW (cfs)
45.0	0.00
46.0	0.00
47.0	0.00
48.0	0.00
49.0	0.00
50.0	0.00
51.0	0.00
52.0	0.00
53.0	0.00
54.0	0.00
55.0	0.00
56.0	0.00
57.0	0.00
58.0	0.00
59.0	0.00
60.0	0.00
61.0	0.00
62.0	0.00
63.0	0.00
64.0	0.00
65.0	0.00
66.0	0.00
67.0	0.00
68.0	0.00
69.0	0.00
70.0	0.00
71.0	0.00
72.0	0.00
73.0	0.00
74.0	0.00
75.0	0.00
76.0	0.00
77.0	0.00
78.0	0.00
79.0	0.00
80.0	0.00
81.0	0.00
82.0	0.00
83.0	0.00
84.0	0.00
85.0	0.00
86.0	0.00
87.0	0.00
88.0	0.00
89.0	0.00

ROUTING COMPUTATIONS

I1+I2 (cfs)	2S/t - 0 (cfs)	2S/t + 0 (cfs)	OUTFLOW (cfs)	ELEVATION (ft)
0.0	1241.9	1245.5	1.82	484.20
0.0	1238.3	1241.9	1.81	484.19
0.0	1234.7	1238.3	1.81	484.18
0.0	1231.0	1234.7	1.81	484.17
0.0	1227.4	1231.0	1.81	484.16
0.0	1223.8	1227.4	1.81	484.15
0.0	1220.2	1223.8	1.81	484.15
0.0	1216.6	1220.2	1.80	484.14
0.0	1213.0	1216.6	1.80	484.13
0.0	1209.4	1213.0	1.80	484.12
0.0	1205.8	1209.4	1.80	484.11
0.0	1202.2	1205.8	1.80	484.10
0.0	1198.6	1202.2	1.79	484.09
0.0	1195.0	1198.6	1.79	484.08
0.0	1191.4	1195.0	1.79	484.08
0.0	1187.9	1191.4	1.79	484.07
0.0	1184.3	1187.9	1.79	484.06
0.0	1180.7	1184.3	1.79	484.05
0.0	1177.1	1180.7	1.78	484.04
0.0	1173.6	1177.1	1.78	484.03
0.0	1170.0	1173.6	1.78	484.02
0.0	1166.5	1170.0	1.78	484.01
0.0	1162.9	1166.5	1.78	484.00
0.0	1159.4	1162.9	1.78	484.00
0.0	1155.8	1159.4	1.77	483.99
0.0	1152.3	1155.8	1.77	483.98
0.0	1148.7	1152.3	1.77	483.97
0.0	1145.2	1148.7	1.77	483.96
0.0	1141.7	1145.2	1.77	483.95
0.0	1138.1	1141.7	1.76	483.94
0.0	1134.6	1138.1	1.76	483.93
0.0	1131.1	1134.6	1.76	483.92
0.0	1127.6	1131.1	1.76	483.92
0.0	1124.1	1127.6	1.76	483.91
0.0	1120.5	1124.1	1.76	483.90
0.0	1117.0	1120.5	1.76	483.90
0.0	1113.5	1117.0	1.75	483.89
0.0	1110.0	1113.5	1.75	483.88
0.0	1106.5	1110.0	1.75	483.87
0.0	1103.0	1106.5	1.75	483.86
0.0	1099.6	1103.0	1.75	483.85
0.0	1096.1	1099.6	1.75	483.85
0.0	1092.6	1096.1	1.74	483.84
0.0	1089.1	1092.6	1.74	483.83
0.0	1085.6	1089.1	1.74	483.82
0.0	1082.1	1085.6	1.74	483.81

\*\*\*\*\* SUMMARY OF ROUTING COMPUTATIONS \*\*\*\*\*

Pond File: C:\WINDOWS\DESKTOP\PONDPA~1\9197 .PND  
Inflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\9197-015.HYD  
Outflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\91970015.HYD

Starting Pond W.S. Elevation = 479.12 ft

\*\*\*\*\* Summary of Peak Outflow and Peak Elevation \*\*\*\*\*

Peak Inflow = 34.48 cfs  
Peak Outflow = 1.84 cfs  
Peak Elevation = 484.33 ft

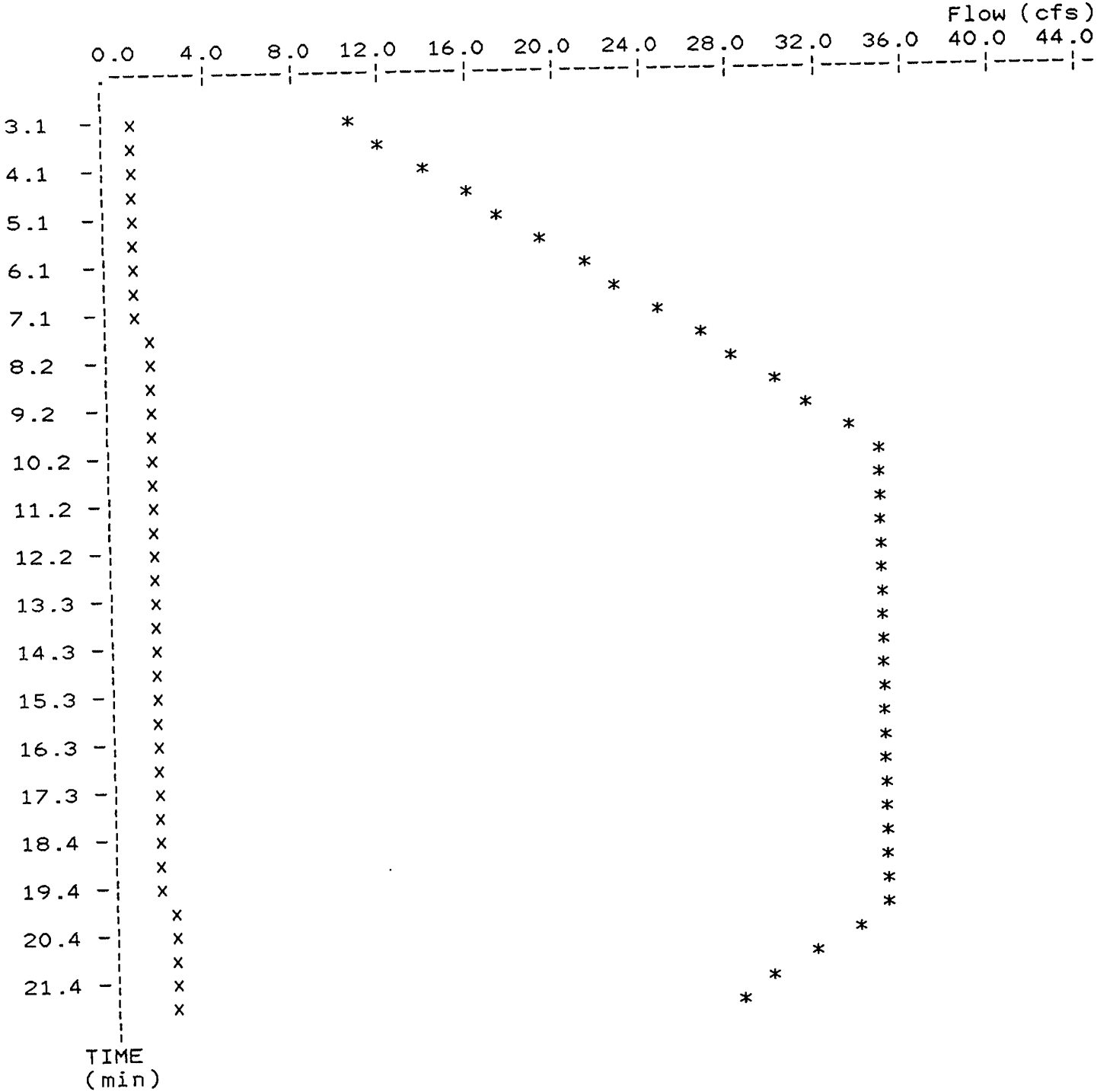
\*\*\*\*\* Summary of Approximate Peak Storage \*\*\*\*\*

Initial Storage = 0.00 ac-ft  
Peak Storage From Storm = 0.89 ac-ft  
-----  
Total Storage in Pond = 0.89 ac-ft

Pond File: C:\WINDOWS\DESKTOP\PONDPA~1\9197 .PND  
 Inflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\9197-015.HYD  
 Outflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\91970015.HYD

EXECUTED: 01-30-1998  
14:14:21

Peak Inflow = 34.48 cfs  
 Peak Outflow = 1.84 cfs  
 Peak Elevation = 484.33 ft



x File: C:\WINDOWS\DESKTOP\PONDPA~1\91970015.HYD Qmax = 1.8 cfs  
 \* File: C:\WINDOWS\DESKTOP\PONDPA~1\9197-015.HYD Qmax = 34.5 cfs



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*
*           THE KNOLLS
*         DETENTION ANALYSIS
*   PREPARED BY: BAX ENGINEERING CO., INC.
*           JANUARY 5, 1998
*
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Inflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\9197-002.HYD  
 Rating Table file: C:\WINDOWS\DESKTOP\PONDPA~1\9197 .PND

----INITIAL CONDITIONS----  
 Elevation = 479.12 ft  
 Outflow = 0.00 cfs  
 Storage = 0.00 ac-ft

GIVEN POND DATA

ELEVATION (ft)	OUTFLOW (cfs)	STORAGE (ac-ft)
479.12	0.0	0.000
479.62	0.4	0.004
480.12	0.7	0.033
480.62	0.9	0.082
481.12	1.1	0.147
481.62	1.2	0.229
482.12	1.4	0.332
482.62	1.5	0.445
483.12	1.6	0.567
483.62	1.7	0.696
484.12	1.8	0.834
484.62	1.9	0.980
485.12	2.0	1.134
485.62	2.0	1.298
486.12	2.1	1.470
486.62	2.2	1.651
487.12	2.3	1.841
487.62	2.4	2.041
488.12	2.4	2.250
488.62	2.5	2.470
489.12	2.6	2.699
489.62	2.6	2.939
490.12	2.7	3.189
490.62	2.7	3.450
491.12	2.8	3.722
491.62	2.9	4.005
492.12	2.9	4.301
492.62	3.0	4.608
493.12	3.0	4.926
493.62	3.1	5.257
494.00	3.1	5.517

INTERMEDIATE ROUTING  
 COMPUTATIONS

2S/t (cfs)	2S/t + 0 (cfs)
0.0	0.0
6.1	6.5
47.3	48.0
118.9	119.8
213.1	214.2
333.2	334.4
481.7	483.1
646.7	648.2
823.1	824.7
1011.1	1012.8
1211.0	1212.8
1423.0	1424.9
1647.3	1649.3
1884.1	1886.1
2134.0	2136.1
2396.9	2399.1
2673.3	2675.6
2963.4	2965.8
3267.7	3270.1
3586.2	3588.7
3919.2	3921.8
4267.0	4269.6
4630.1	4632.8
5009.0	5011.7
5404.1	5406.9
5815.8	5818.7
6244.5	6247.4
6690.1	6693.1
7153.1	7156.1
7633.6	7636.7
8010.8	8013.9

Time increment (t) = 1.0 min.

Pond File: C:\WINDOWS\DESKTOP\PONDPA~1\9197 .PND  
 Inflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\9197-002.HYD  
 Outflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\91970002.HYD

INFLOW HYDROGRAPH

ROUTING COMPUTATIONS

TIME (min)	INFLOW (cfs)	I1+I2 (cfs)	2S/t - 0 (cfs)	2S/t + 0 (cfs)	OUTFLOW (cfs)	ELEVATION (ft)
0.0	0.00	-----	0.0	0.0	0.00	479.12
1.0	2.12	2.1	1.9	2.1	0.13	479.28
2.0	4.20	6.3	7.4	8.2	0.41	479.64
3.0	6.32	10.5	16.9	17.9	0.48	479.76
4.0	8.40	14.7	30.5	31.6	0.58	479.92
5.0	10.52	18.9	48.0	49.4	0.70	480.13
6.0	12.58	23.1	69.6	71.1	0.76	480.28
7.0	14.70	27.3	95.2	96.8	0.84	480.46
8.0	16.83	31.5	124.9	126.7	0.91	480.66
9.0	18.90	35.7	158.6	160.6	0.99	480.84
10.0	21.02	39.9	196.4	198.5	1.07	481.04
11.0	21.03	42.1	236.2	238.5	1.12	481.22
12.0	21.03	42.1	276.0	278.3	1.15	481.39
13.0	21.03	42.1	315.7	318.0	1.19	481.55
14.0	21.03	42.1	355.2	357.7	1.23	481.70
15.0	21.03	42.1	394.7	397.3	1.28	481.83
16.0	21.03	42.1	434.1	436.8	1.34	481.96
17.0	21.03	42.1	473.4	476.2	1.39	482.10
18.0	21.03	42.1	512.6	515.5	1.42	482.22
19.0	21.03	42.1	551.8	554.7	1.44	482.34
20.0	21.03	42.1	590.9	593.9	1.47	482.46
21.0	18.92	40.0	627.9	630.9	1.49	482.57
22.0	16.84	35.8	660.6	663.7	1.51	482.66
23.0	14.72	31.6	689.1	692.2	1.52	482.74
24.0	12.59	27.3	713.4	716.5	1.54	482.81
25.0	10.52	23.1	733.4	736.5	1.55	482.87
26.0	8.41	18.9	749.2	752.3	1.56	482.91
27.0	6.33	14.7	760.8	763.9	1.57	482.95
28.0	4.21	10.5	768.2	771.4	1.57	482.97
29.0	2.13	6.3	771.4	774.6	1.57	482.98
30.0	0.01	2.1	770.4	773.5	1.57	482.98
31.0	0.00	0.0	767.3	770.4	1.57	482.97
32.0	0.00	0.0	764.1	767.3	1.57	482.96
33.0	0.00	0.0	761.0	764.1	1.57	482.95
34.0	0.00	0.0	757.9	761.0	1.56	482.94
35.0	0.00	0.0	754.8	757.9	1.56	482.93
36.0	0.00	0.0	751.6	754.8	1.56	482.92
37.0	0.00	0.0	748.5	751.6	1.56	482.91
38.0	0.00	0.0	745.4	748.5	1.56	482.90
39.0	0.00	0.0	742.3	745.4	1.56	482.90
40.0	0.00	0.0	739.2	742.3	1.55	482.89
41.0	0.00	0.0	736.1	739.2	1.55	482.88
42.0	0.00	0.0	733.0	736.1	1.55	482.87
43.0	0.00	0.0	729.9	733.0	1.55	482.86
44.0	0.00	0.0	726.8	729.9	1.55	482.85

Pond File: C:\WINDOWS\DESKTOP\PONDPA~1\9197 .PND  
 Inflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\9197-002.HYD  
 Outflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\91970002.HYD

INFLOW HYDROGRAPH

ROUTING COMPUTATIONS

TIME (min)	INFLOW (cfs)	I1+I2 (cfs)	2S/t - 0 (cfs)	2S/t + 0 (cfs)	OUTFLOW (cfs)	ELEVATION (ft)
45.0	0.00	0.0	723.7	726.8	1.54	482.84
46.0	0.00	0.0	720.6	723.7	1.54	482.83
47.0	0.00	0.0	717.5	720.6	1.54	482.83
48.0	0.00	0.0	714.5	717.5	1.54	482.82
49.0	0.00	0.0	711.4	714.5	1.54	482.81
50.0	0.00	0.0	708.3	711.4	1.54	482.80
51.0	0.00	0.0	705.2	708.3	1.53	482.79
52.0	0.00	0.0	702.2	705.2	1.53	482.78
53.0	0.00	0.0	699.1	702.2	1.53	482.77
54.0	0.00	0.0	696.1	699.1	1.53	482.76
55.0	0.00	0.0	693.0	696.1	1.53	482.76
56.0	0.00	0.0	690.0	693.0	1.53	482.75
57.0	0.00	0.0	686.9	690.0	1.52	482.74
58.0	0.00	0.0	683.9	686.9	1.52	482.73
59.0	0.00	0.0	680.8	683.9	1.52	482.72
60.0	0.00	0.0	677.8	680.8	1.52	482.71
61.0	0.00	0.0	674.8	677.8	1.52	482.70
62.0	0.00	0.0	671.7	674.8	1.52	482.70
63.0	0.00	0.0	668.7	671.7	1.51	482.69
64.0	0.00	0.0	665.7	668.7	1.51	482.68
65.0	0.00	0.0	662.7	665.7	1.51	482.67
66.0	0.00	0.0	659.6	662.7	1.51	482.66
67.0	0.00	0.0	656.6	659.6	1.51	482.65
68.0	0.00	0.0	653.6	656.6	1.50	482.64
69.0	0.00	0.0	650.6	653.6	1.50	482.64
70.0	0.00	0.0	647.6	650.6	1.50	482.63
71.0	0.00	0.0	644.6	647.6	1.50	482.62
72.0	0.00	0.0	641.6	644.6	1.50	482.61
73.0	0.00	0.0	638.6	641.6	1.50	482.60
74.0	0.00	0.0	635.6	638.6	1.49	482.59
75.0	0.00	0.0	632.7	635.6	1.49	482.58
76.0	0.00	0.0	629.7	632.7	1.49	482.57
77.0	0.00	0.0	626.7	629.7	1.49	482.56
78.0	0.00	0.0	623.7	626.7	1.49	482.55
79.0	0.00	0.0	620.7	623.7	1.49	482.55
80.0	0.00	0.0	617.8	620.7	1.48	482.54
81.0	0.00	0.0	614.8	617.8	1.48	482.53
82.0	0.00	0.0	611.9	614.8	1.48	482.52
83.0	0.00	0.0	608.9	611.9	1.48	482.51
84.0	0.00	0.0	606.0	608.9	1.48	482.50
85.0	0.00	0.0	603.0	606.0	1.47	482.49
86.0	0.00	0.0	600.1	603.0	1.47	482.48
87.0	0.00	0.0	597.1	600.1	1.47	482.47
88.0	0.00	0.0	594.2	597.1	1.47	482.47
89.0	0.00	0.0	591.2	594.2	1.47	482.46

\*\*\*\*\* SUMMARY OF ROUTING COMPUTATIONS \*\*\*\*\*

Pond File: C:\WINDOWS\DESKTOP\PONDPA~1\9197 .PND  
Inflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\9197-002.HYD  
Outflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\91970002.HYD

Starting Pond W.S. Elevation = 479.12 ft

\*\*\*\*\* Summary of Peak Outflow and Peak Elevation \*\*\*\*\*

Peak Inflow = 21.03 cfs  
Peak Outflow = 1.57 cfs  
Peak Elevation = 482.98 ft

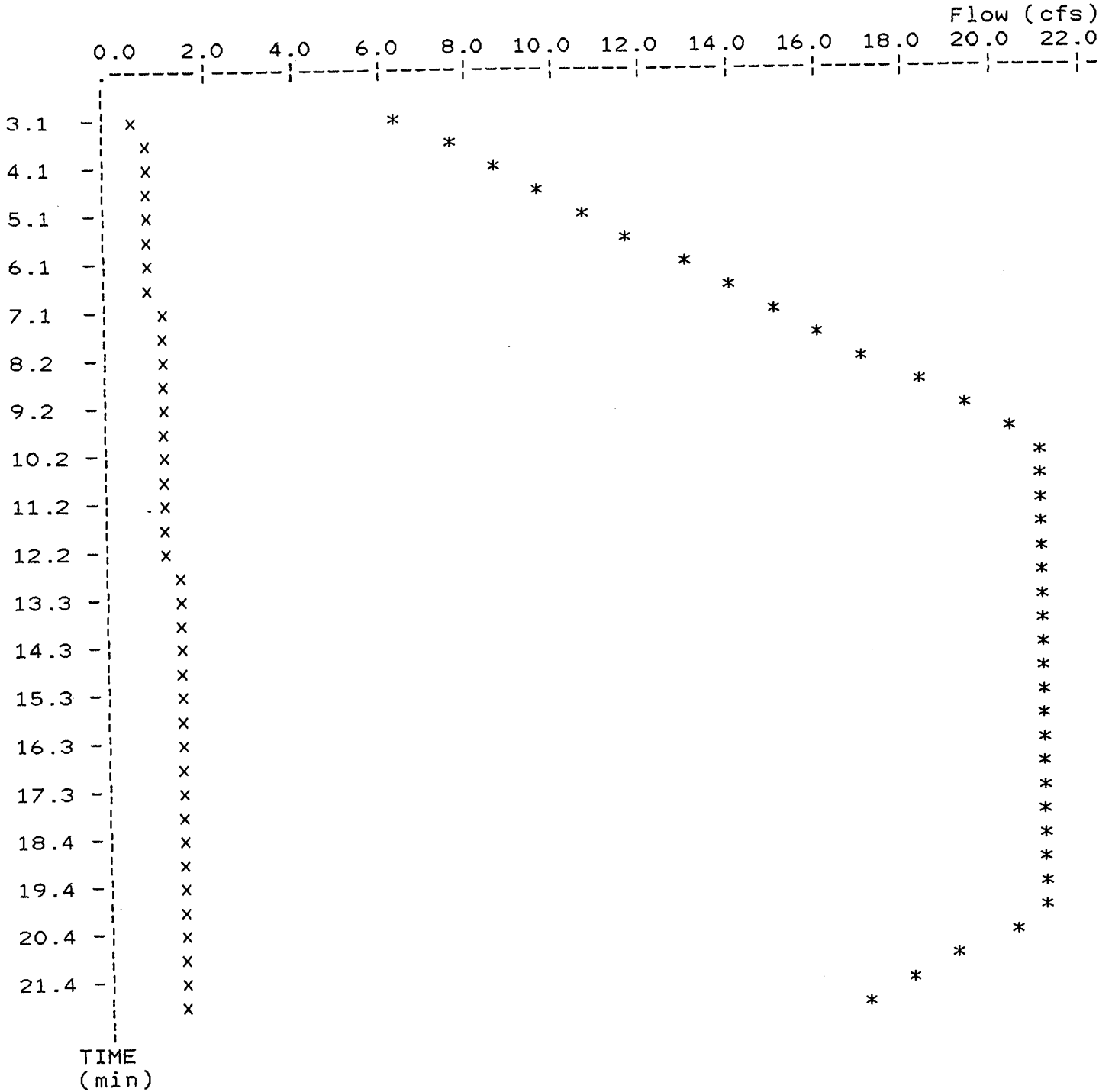
\*\*\*\*\* Summary of Approximate Peak Storage \*\*\*\*\*

Initial Storage = 0.00 ac-ft  
Peak Storage From Storm = 0.53 ac-ft  
-----  
Total Storage in Pond = 0.53 ac-ft

Pond File: C:\WINDOWS\DESKTOP\PONDPA~1\9197 .PND  
 Inflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\9197-002.HYD  
 Outflow Hydrograph: C:\WINDOWS\DESKTOP\PONDPA~1\91970002.HYD

EXECUTED: 01-30-1998  
 14:14:21

Peak Inflow = 21.03 cfs  
 Peak Outflow = 1.57 cfs  
 Peak Elevation = 482.98 ft



x File: C:\WINDOWS\DESKTOP\PONDPA~1\91970002.HYD Qmax = 1.6 cfs  
 \* File: C:\WINDOWS\DESKTOP\PONDPA~1\9197-002.HYD Qmax = 21.0 cfs

10:39 AM 3/9/98

Channel Calculator

Given Input Data:

Shape .....	Advanced
Solving for .....	Depth of Flow
Flowrate .....	4.0000 cfs
Slope .....	0.0100 ft/ft
Manning's n .....	0.0500
Height .....	12.0000 in
Bottom width .....	0.0000 in
Left radius .....	0.0000 in
Right radius .....	0.0000 in
Left slope .....	3.0000 ft/ft
Right slope .....	3.0000 ft/ft

Computed Results:

Depth .....	10.7058 in
Velocity .....	1.6752 fps
Flow area .....	2.3878 ft2
Flow perimeter .....	67.7091 in
Hydraulic radius .....	5.0782 in
Top width .....	64.2345 in
Area .....	3.0000 ft2
Perimeter .....	75.8947 in
Percent full .....	89.2146 %

Critical Information

Critical depth .....	7.7243 in
Critical slope .....	0.0570 ft/ft
Critical velocity .....	3.2179 fps
Critical area .....	1.2430 ft2
Critical perimeter .....	48.8531 in
Critical hydraulic radius .....	3.6640 in
Critical top width .....	46.3461 in
Specific energy .....	0.9358 ft
Minimum energy .....	0.9655 ft
Froude number .....	0.4422
Flow condition .....	Subcritical

18

## Weir Calculator

## Given Input Data:

Weir Type .....	Rectangular
Equation .....	Suppressed
Solving for .....	Depth of Flow
Flowrate .....	219.9000 cfs
Coefficient .....	2.6000
Height .....	24.0000 in

## Computed Results:

Depth of Flow .....	11.4358 in
Full Flow .....	668.5648 cfs
Velocity .....	13.5735 fps
Width .....	204.0000 in
Area .....	34.0000 ft2
Perimeter .....	252.0000 in
Wet Perimeter .....	226.8716 in
Wet Area .....	16.2007 ft2
Percent Full .....	47.6491 %

Weir Calculator

Given Input Data:

Weir Type .....	Rectangular
Equation .....	Suppressed
Solving for .....	Depth of Flow
Flowrate .....	151.0800 cfs
Coefficient .....	2.6000
Height .....	24.0000 in

Computed Results:

Depth of Flow .....	8.9040 in
Full Flow .....	668.5648 cfs
Velocity .....	11.9771 fps
Width .....	204.0000 in
Area .....	34.0000 ft2
Perimeter .....	252.0000 in
Wet Perimeter .....	221.8081 in
Wet Area .....	12.6140 ft2
Percent Full .....	37.1001 %



## Weir Calculator

## Given Input Data:

Weir Type .....	Rectangular
Equation .....	Suppressed
Solving for .....	Depth of Flow
Flowrate .....	108.5900 cfs
Coefficient .....	2.6000
Height .....	24.0000 in

## Computed Results:

Depth of Flow .....	7.1446 in
Full Flow .....	668.5648 cfs
Velocity .....	10.7287 fps
Width .....	204.0000 in
Area .....	34.0000 ft2
Perimeter .....	252.0000 in
Wet Perimeter .....	218.2891 in
Wet Area .....	10.1215 ft2
Percent Full .....	29.7690 %



### ANTI-SEEP COLLAR DESIGN

Use 100yr/20 minute H.W. Elev. = 486.44 ft.  
Flowline of pipe outflow = 479.12 ft.

Solution: Determine the length of pipe within the saturated zone of the embankment.

$$L_s = y(3+4) \left[ 1 + \frac{\text{Pipe slope}}{0.25 - \text{Pipe slope}} \right]$$

$$L_s = 7.32'(3+4) \left[ 1 + \frac{0.01}{0.25 - 0.01} \right]$$

$$L_s = 53.38 \text{ feet}$$

Use Table 1 - to use to find number and size of collars.

Pipe diameter = 2.50 feet

N = 2 collars

Size = 6.30' x 6.30'

Design 2 anti-seep collars (6.30' x 6.30')  
Place both of the anti-seep collars within the saturation zone as shown on the profiles.

## ANTI-SEEP COLLAR DESIGN

This procedure provides the anti-seep collar dimensions for only temporary sediment basins to increase the seepage length by 15% for various pipe slopes, embankment slopes and riser heights.

The first step in designing anti-seep collars is to determine the length of pipe within the saturated zone of the embankment. This can be done graphically or by the following equation, assuming that the upstream slope of the embankment intersects the invert of the pipe at its upstream end. (See embankment-invert intersection on the drawing below:

$$L_s = y (z + 4) \left[ 1 + \frac{\text{pipe slope}}{0.25\text{-pipe slope}} \right]$$

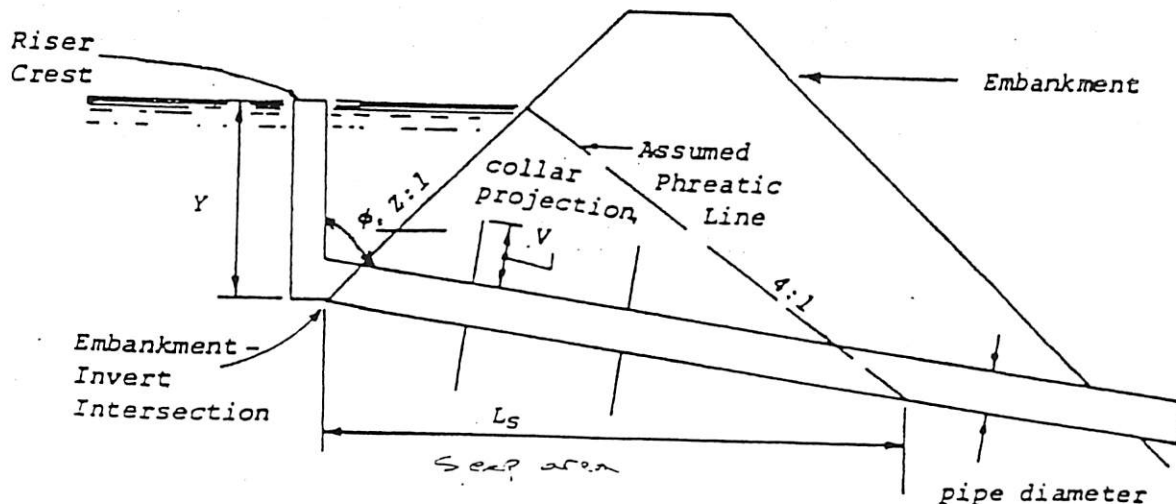
where:  $L_s$  = length of pipe in the saturated zone (ft.)

$y$  = distance in feet from upstream invert of pipe to highest normal water level expected to occur during the life of the structure, usually the top of the riser.

$z$  = slope of upstream embankment as a ratio of  $z$  ft. horizontal to one ft. vertical.

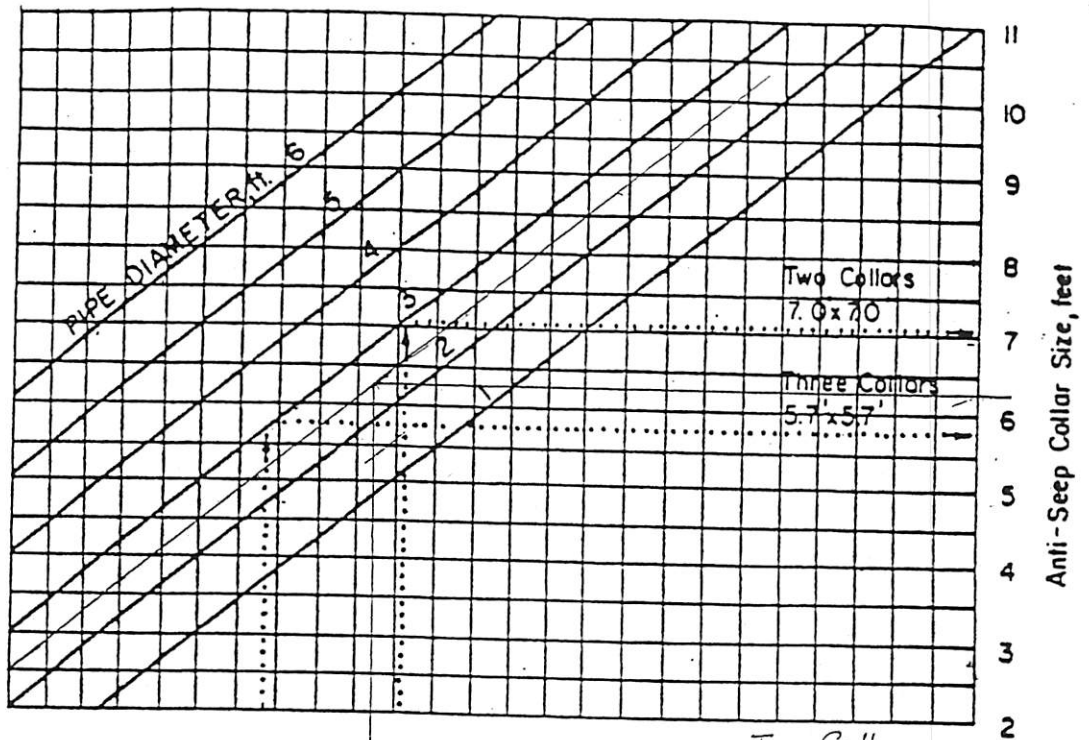
pipe slope = slope of pipe in feet per foot.

This procedure is based on the approximation of the phreatic line as shown in the drawing below:



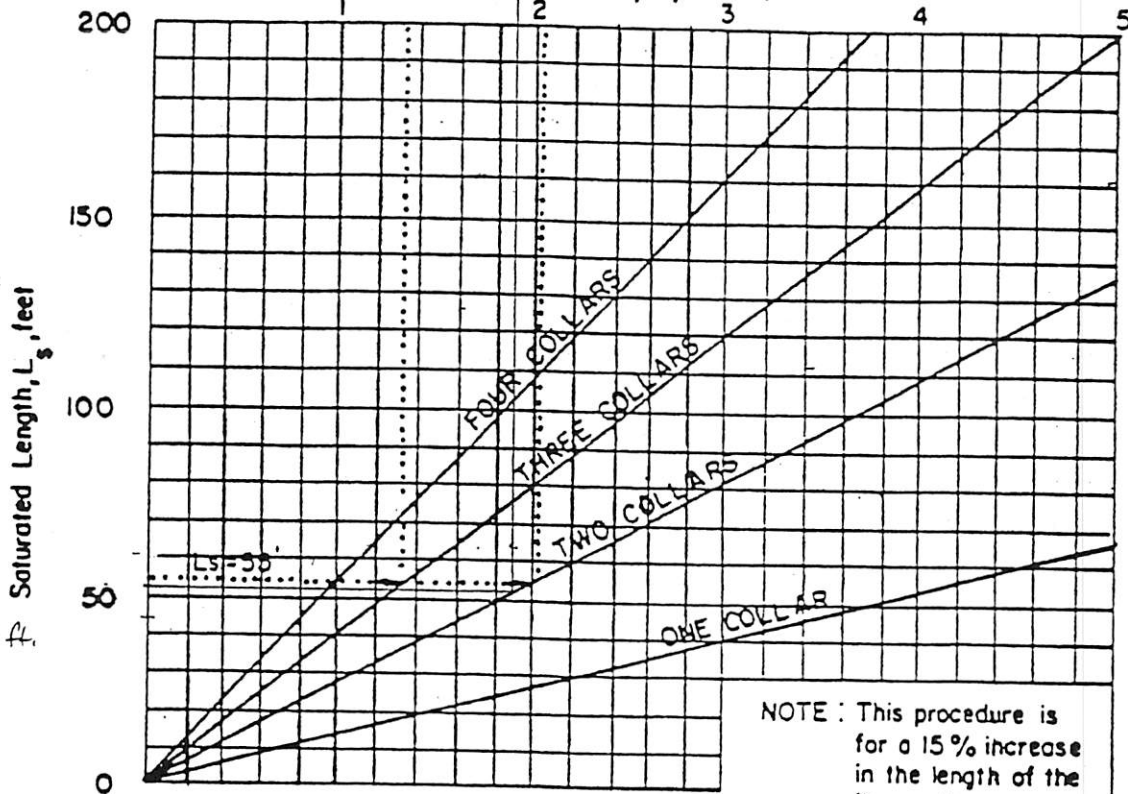
# ANTI-SEEP COLLAR DESIGN

$D = 2.50 \text{ ft.}$



COLLAR PROJECTION, V, FEET

Two Collars  
6.3' x 6.3'



$L_s = 53.33 \text{ ft.}$

NOTE: This procedure is for a 15% increase in the length of the flow path.



ENGINEERING

PLANNING

SURVEYING

**DATE:** March 9, 1998

**TO:** City of O'Fallon  
Attn: Joan Gallup  
138 South Main Street  
O'Fallon, MO-63366

**RE:** The Knolls  
BAX PROJECT NO. 97-9197

**ATTACHED ARE:**

**QUANTITY**

4 Sets  
4 Copies  
1 Copy  
1 Copy  
1 Copy  
1 Copy  
1 Original  
1 Copy

**DESCRIPTION**

Revised Construction Plans  
Revised Hydraulic Calculations  
Inlet control on FE49  
F.I.R.M. Map and Flood Profiles  
Spillway Calculations  
Swale Calculations  
Flood Plain Development Application  
C.O.E. Permit

**THESE ARE TRANSMITTED FOR:**

- |  |  |
|--|--|
| <input type="checkbox"/> As-You Requested                        | <input type="checkbox"/> For Your Information        |
| <input type="checkbox"/> Review and Approval                     | <input type="checkbox"/> Address Assignment          |
| <input type="checkbox"/> Grading Permit                          | <input type="checkbox"/> Fire Hydrant Recommendation |
| <input checked="" type="checkbox"/> Final Approval/Required Sets | <input type="checkbox"/> Easement Requests           |

**REMARKS:** Please review and approve the revised construction plans and send us one stamped and approved set of plans for our file. Any questions please call me. Thank You.

(X) PLEASE RETURN 1 PLAN(S) WITH INFORMATION REQUESTED

**SINCERELY,**

Michael R. Keebler, E.I.T.

cc: Jerry Schneidegger

BAX ENGINEERING CO., INC.  
1052 South Cloverleaf Drive  
St. Peters, MO 63376-6445  
314-928-5552 FAX 928-1718  
e-mail: baxeng@msn.com



ENGINEERING

PLANNING

SURVEYING

SILTATION/SEDIMENT STORAGE CALCULATIONS

The Knolls - O'Fallon  
BAX PROJECT NO. 97-9197  
DECEMBER 23, 1997

Siltation/Sediment storage will be provided by over excavation of the basin. The following calculations are based on a nomograph provided by the City of O'Fallon.

Total disturbed area tributary to lake 31.7 AC.  
Rational Method "C" Factor 0.40 %

FROM FIGURE 1:

The required siltation volume for 2 year construction period:

$$260 \text{ Cu.Ft./Ac.} \times 31.7 \text{ Ac.} = 8,242 \text{ Cu.Ft.}$$

Volume Calculations:

ELEVATION	OVER-EX*	FINAL	SUM	DEPTH	TOTAL VOLUME
	AREA (-)	AREA (=)	AREA		
	Sq.Ft.	Sq.Ft.	Sq.Ft.	Ft.	Cu.Ft.
481.0	8,134	0	8,134		0
482.0	9,419	3,069	6,350	1.0	7,242
483.0	10,772	7,565	3,207	1.0	4,779
484.0	12,188	12,188	0	1.0	6,382

\* over-excavated area above basin outflow.

ELEVATION	AREA	DEPTH	VOLUME
	Sq.Ft.	Ft.	Cu.Ft.
481.0	8,134	0.0	0
480.0	6,918	1.0	7,526
479.5	6,335	0.5	11,143 (> 8,242)

Based on the above calculations the basin will be required to be over-excavated 1.5' (see site plan) to provide storage for the anticipated siltation. 6,382 cubic feet of storage above the basin outflow is also provided for sediment storage.

BAX ENGINEERING CO., INC.  
1052 South Cloverleaf Drive  
St. Peters, MO 63376-6445  
314-928-5552 FAX 928-1718



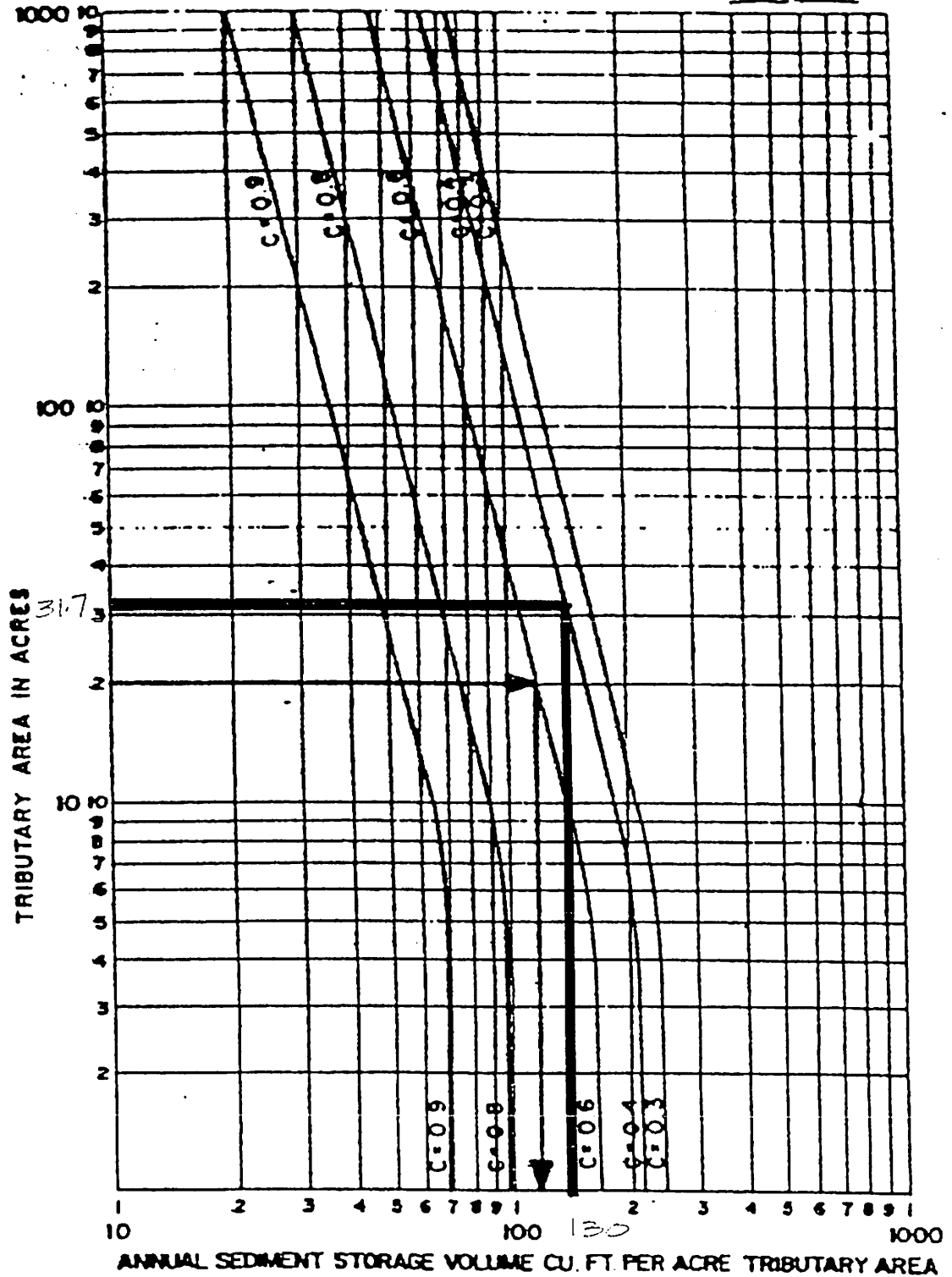
**EXAMPLE:**

TRIBUTARY AREA = 20 ACRES

RATIONAL METHOD RUNOFF COEFFICIENT "C" = 0.6

SEDIMENT STORAGE = 120 CU. FT. PER ACRE PER YEAR

TOTAL SEDIMENT STORAGE = 120 X 20 = 2400 CU. FT. PER YEAR.



ANNUAL SEDIMENT STORAGE

FIG. 6