

**CITY OF O'FALLON**  
Charley Drive ( Phoenix Drive ) ✓  
Saint Charles County

Bridge No. 3210015

Design Calculations

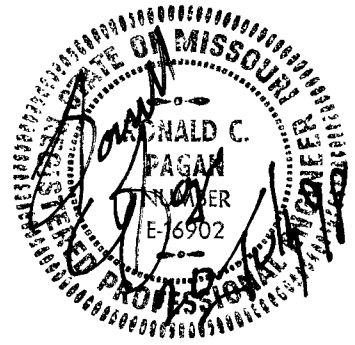
KDG Project No. 980100-0001

**CITY OF O'FALLON**  
Bridge No. 3210015  
Design Calculations  
Winghaven  
KdG Project No. 980100-0001

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10. Quantities
11. Specifications

CITY OF O'FALLON  
Bridge No. 3210015  
Design Calculations  
Winghaven  
KdG Project No. 980100-0001



### ENGINEERING CALCULATION COVER SHEET

PROJECT: <u>Bridge No. 3210015</u>	DISCIPLINE: <u>Bridge</u>
<u>Charley Drive</u>	CALCULATION NO.: <u>Final</u>
_____	NO. OF SHEETS: <u>See Index</u>
JOB NO.: <u>980100-0001</u>	CALCULATED BY: <u>JVS RCB</u>
CONTRACT NO.: _____	CHECKED BY: <u>[Signature]</u>
DESIGN CODE: <u>AASHTO 1996</u>	APPROVED BY: <u>[Signature]</u>
_____	APPROVED BY: _____

CALCULATION DESCRIPTION: \_\_\_\_\_  
Substructure Design  
\_\_\_\_\_  
Quantities  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

DESIGN BASIS OR REFERENCES: \_\_\_\_\_  
AASHTO 16th Edition, 1996  
\_\_\_\_\_  
Missouri Highway & Transportation Department Bridge Manual of Design  
\_\_\_\_\_  
\_\_\_\_\_

**CITY OF O'FALLON**  
Bridge No. 3210015  
Design Calculations  
Winghaven  
KdG Project No. 980100-0001

## **DESIGN SCOPE**

Structure Type Rigid  
Box Design  
Five Cell  
(12.0 Ft. Wide X 12.0 Ft. High)

Loading:  
HS20-44  
Load Factor Design  
Earth 120#/Cu. Ft.  
Equivalent Fluid Pressure 60#/Cu.Ft.

## DESIGN CRITERIA

### DESIGN SPECIFICATIONS

AASHTO - 1996 Sixteenth Edition

### DESIGN LOADING

HS20  
Earth 120#/cu.ft.  
Equivalent Fluid Pressure 60#/Cu.Ft.

### DESIGN UNIT STRESSES

Class B Concrete (Culverts)	$f_c$	=	3,000 psi
Reinforcing Steel (Grade 60)	$f_y$	=	60,000 psi

### REINFORCING STEEL

Minimum clearance to reinforcing steel shall be 1-1/2", unless otherwise shown.

### BAR COVER - AASHTO 8.22

Clear Dimensions to be shown on plans:

Top Slab	- Top Reinforcing	=	2" clear
	- Bottom Reinforcing	=	1-1/2" clear
Bottom Slab	- Top Reinforcing	=	1-1/2" clear
	- Bottom Reinforcing	=	3" clear
Sidewalls	- Reinforcement Stream Face	=	1-1/2" clear
	- Reinforcement Fill Face	=	2" clear

### MAXIMUM BAR LENGTHS

Longitudinal bars should be made full length without splicing up to about 40'-0"; splice if longer. Bars #5 and larger may be used to a length of 60'-0" without splicing.

### BAR SPLICES

See Section 2.4 for minimum bar lap and tension splices in reinforcement. Use a Class C splice for longitudinal bar (22" min.).

### JOINT FILLER

All joint filler shall meet requirements of Standard Specification 1057.2.5, except as noted.

DESIGN LAYOUT

Division of Bridges

No. 3210015

Job. \_\_\_\_\_

Route Charley Drive County Saint Charles Rte. Winghaven Drive

STRUCTURE

SUPERSTRUCTURE Five Cell (12.0W x 12.0H) (Rigid)

Skew ..... Square

Roadway ..... 3 - 12 foot lanes.

Loading ..... HS20

Beg. Sta. .... \_\_\_\_\_

Alignment ..... Tangent

Grade ..... H.P.I. Sta. 15+50.00 (Elev. 522.73) Bk. -1.00%, Ahd. +1.00%, Length = 120.00

..... V.P.I. Sta. 63+75.00 (Elev. 506.65) Bk. +1.00%, Ahd. -3.00%, Length = 200.00

SUBSTRUCTURE

Ftg Loads ..... 2,000 lbs per square foot

Pile Type ..... N/A

Length ..... N/A

Elev Ftg, Bott. .... 490.0 High 489.0 Low

GENERAL

Revetment/Slope ..... Sideslope 3:1 (Normal)

End Fills ..... Earth

Traffic Handling ..... \_\_\_\_\_

Present Bridge ..... None

SPECIAL REQUIREMENTS

Profile Grade ..... Centerline of Winghaven Drive

Rail Road Alignment ..... N/A

Tie Station ..... 62 + 53.89

Final Allowable Clearances ..... N.A.

Estimate includes 10% for Engineering and Contingencies and 5% for Preliminary Engineering

Dated:

By:

Estm. \$

<p>Date:</p> <hr/> <p>Initials:</p>	<p>Notes or Revisions in Conference</p>
-------------------------------------	---

CITY OF O'FALLON  
Bridge No. 3210015  
Design Calculations  
Winghaven  
KdG Project No. 980100-0001

## DRAWING LIST

Sheet No.	Title
1	Plan, Elevation, General Notes, and Quantities
2	Reinforcement
3	Cross Section and Wing Wall Details

**CORRESPONDENCE**



# PICKETT RAY & SILVER

CIVIL ENGINEERS

PLANNERS

LAND SURVEYORS

July 14, 1998

Revised July 15, 1998

Mr. Ron Pagan  
Kuhlmann Design Group, Inc  
66 Progress Parkway  
St. Louis, Missouri 63043

RE WINGHAVEN - BOX CULVERT  
PR&S PROJECT NO 97-034

Dear Ron

Per our meeting today, I am sending you "sealed" confirmation of box culvert information

	"S"	"H"	Elev 1	Elev 2	A Rt	A Lt	B	Des-Fill	Des-Fill
Winghaven Station 17-15	10	7	575.42	574.58	60	60	<u>24</u>	1	4
Winghaven Station 30+49	10	7	<u>580.68</u>	<u>579.92</u>	<u>60</u>	<u>60</u>	<u>24</u>	<u>1</u>	<u>7</u>
Winghaven Station 59+00	12	10	516.39	517.11	70	70	<u>30</u>	1	5
Charlie (Phoenix) Station 62+53.89	12	12	488.91	490.09	43	43	37	1	4
David (Red Hawk) Station 5+29.73	8	7	511.20	510.45	60	60	30	1	7

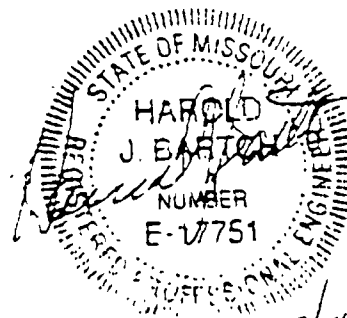
We will send Winghaven Station 30-49 as soon as the street is revised back to the previous grade. If you need anything else, please contact me or Mr. Jim Cannady

Very truly yours,  
PICKETT, RAY & SILVER, INC

*Tanya J. Dietz*  
Tanya J. Dietz  
Project Design Supervisor

bjs

cc: Mr. Joe McKee, Paric Corporation  
Mr. Dave Rogers, Fred Weber



# PICKETT RAY & SILVER

CIVIL ENGINEERS

PLANNERS

LAND SURVEYORS

ADG. MH FILE 980100



JUL 16 1998

CONFIDENTIALITY NOTE

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PLEASE DELIVER THE FOLLOWING PAGES:

TO: *Ron* 434 8280

FROM: *Janey*

PROJECT: *Wingfield*

PR&S PROJECT NO.: *97034*

DATE AND TIME: *7/15/98*

TOTAL NO. OF PAGES, INCLUDING COVER SHEET: *15*

TELECOPY OPERATOR: *15*

*3:40 pm*

PLEASE NOTIFY US IMMEDIATELY IF THE MESSAGE IS INCOMPLETE OR UNCLEAR. THANK YOU.

333 MID RIVERS MALL DRIVE • ST. PETERS, MISSOURI 63376 • 314-397-1211/314-397-1104 FAX

# PICKETT RAY & SILVER

CIVIL ENGINEERS

PLANNERS

LAND SURVEYORS

KDG, MH FILE 980100

July 14, 1998

Revised July 15, 1998

JUL 15 1998

Mr. Ron Pagan  
Kuhlmann Design Group, Inc.  
66 Progress Parkway  
St. Louis, Missouri 63043


RE WINGHAVEN - BOX CULVERT  
PR&S PROJECT NO 97-034

Dear Ron:

Per our meeting today, I am sending you "sealed" confirmation of box culvert information.

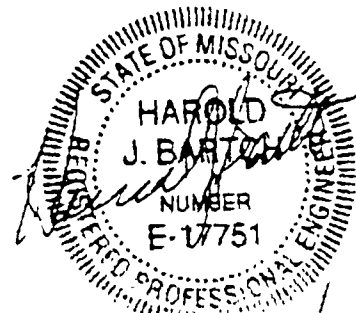
	"S"	"H"	Elev 1	Elev 2	A Rt	A Lt	B	Des-Fill	Des-Fill
Winghaven Station 17+00	10	7	575.42	574.58	60	60	<u>24</u>	1	4
Winghaven Station 30+49	10	7							
Winghaven Station 59+00	12	10	516.39	517.11	70	70	<u>30</u>	1	5
Charlie (Phoenix) Station 62+53.89	12	12	488.91	490.09	43	43	37	1	4
David (Red Hawk) Station 5+00+73	8	7	511.20	510.45	60	60	30	1	7

We will send Winghaven Station 30+49 as soon as the street is revised back to the previous grade. If you need anything else, please contact me or Mr. Jim Cannady.

Very truly yours,  
PICKETT, RAY & SILVER, INC

*Tanya J. Dietz*  
Tanya J. Dietz  
Project Design Supervisor

bjs  
cc Mr. Joe McKee, Parc Corporation  
Mr. Dave Rogers, Fred Weber



# PICKETT RAY & SILVER

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LAND SURVEYORS



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PLEASE DELIVER THE FOLLOWING PAGES:

TO: *Kon*

FROM: *Jany*

PROJECT: *Winghart*

F&S PROJECT NO.: *9703A*

DATE AND TIME: *7/14/98*

TOTAL NO. OF PAGES, INCLUDING COVER SHEET: *22*

TELECOPY OPERATOR: *15*

PLEASE NOTIFY US IMMEDIATELY IF THE MESSAGE IS INCOMPLETE OR UNCLEAR. THANK YOU.

# PICKETT RAY & SILVER

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PLEASE DELIVER THE FOLLOWING PAGES:

TO: RON PAGAN (434 8280)

FROM: TANYA

PROJECT: WINGHAVEN

PR&S PROJECT NO.: 97034

DATE AND TIME: 7.10.94

TOTAL NO. OF PAGES, INCLUDING COVER SHEET: 5

TELECOPY OPERATOR:

COPY TO MIKE HARMAN - WEBER 3440970

PLEASE NOTIFY US IMMEDIATELY IF THE MESSAGE IS INCOMPLETE OR UNCLEAR. THANK YOU.

333 MID RIVERS MALL DRIVE • ST. PETERS, MISSOURI 63376 • 314-397-1211/314-397-1104 FAX

**PICKETT RAY & SILVER**

323 Mid River Mall Dr  
St. PETERS, MD 21157

Civil Engineers  
Planners  
Land Surveyors

397-1211

PROJECT NAME \_\_\_\_\_  
PROJECT #/JOB ORDER # \_\_\_\_\_  
DATE \_\_\_\_\_  
DESIGNER \_\_\_\_\_  
PAGE \_\_\_\_\_

RON -

7.10.98

• BM @ Box(s) : HAS NOT BEEN SET.

• HW ELEV - PER MY CALC :

WINGHAVEN 524.3

PHOENIX 496.3

RED HAWK 520.6

F.P.

WINGHAVEN 522.0

PHOENIX 496.3

RED HAWK N/A

UTILITY SURVEY - DELIVERED (THIS WK)

COMPLETE SET PLANS - READY FRI. (7.10.98)

HW CALCS - ENCLOSED

" ELEV + ABOVE

PROJECT: Wingham - Charlie Dr

STATION: 62+50

SHEET \_\_\_\_\_ OF \_\_\_\_\_

CULVERT DESIGN FORM

DESIGNER/DATE: Edy, 12/22/07

REVIEWER/DATE: \_\_\_\_\_

ROADWAY ELEVATION: 505.40 (11)

EL<sub>1</sub>: 489.75 (11)

EL<sub>2</sub>: 487.25 (11)

EL<sub>3</sub>: 496.5 (11)

3 = 3 - FALL / L<sub>0</sub>  
 S = 0.67%  
 L<sub>0</sub> = 75

HYDROLOGICAL DATA

METHOD:  SEE ADJ. ENTS

DRAINAGE AREA: \_\_\_\_\_

CHANNEL SHAPE: \_\_\_\_\_

ROUTING: \_\_\_\_\_

OTHER: \_\_\_\_\_

DESIGN FLOWS/TAILWATER

R1 (YEARS) / LOW FLOW: 15 / 3671.5

R2 (YEARS) / HIGH FLOW: 100 / 5102.7

CULVERT DESCRIPTION: \_\_\_\_\_

MATERIAL - SHAPE - SIZE - ENTRANCE

5 - 12' x 12' Box

5 - 12' x 12' Box

USE FEMA Q

5 - 12' x 12' Box

TECHNICAL FOOTNOTES:

(1) USE Q/HB FOR BOX CULVERTS

(2) HW<sub>1</sub>/D - HW<sub>1</sub>/D OR HW<sub>1</sub>/D FROM DESIGN CHARTS

(3) FALL = HW<sub>1</sub> - (EL<sub>M</sub> - EL<sub>1</sub>); FALL IS ZERO FOR CONVERSION GRADE

SUBSCRIPT DEFINITIONS:

0 APPROXIMATE

1 CULVERT FACE

2 DESIGN HEADWATER

3 HEADWATER IN INLET CONTROL

4 HEADWATER IN OUTLET CONTROL

5 INLET CONTROL SECTION

6 OUTLET

7 STREAMBED AT CULVERT FACE

8 TAILWATER

HEADWATER CALCULATIONS

TOTAL FLOW PER BARREL (cfs)	Q/HB (1)	INLET CONTROL			OUTLET CONTROL			COMMENTS					
		HW <sub>1</sub> /D (2)	FALL (3)	EL <sub>1</sub> (4)	EL <sub>2</sub> (5)	H (6)	EL <sub>3</sub> (7)						
3672	734	9.4	-	498.2	-	4.8	9.4	8.4	0.5	7	493.4	496.4	Outlet
5103	1021	0.86	10.3	-	5000	-	6.1	9.0	0.5	14	499.6	500.0	Outlet (FEMA)
2495	498	5.4	6.5	-	496.3	-	3.7	7.9	0.5	3	494.3	496.3	Inlet control

(4) EL<sub>1</sub> = HW<sub>1</sub> + EL<sub>1</sub> (INVERT OF INLET CONTROL SECTION)

(5) TW BASED ON DOWNSTREAM CONTROL OR FLOW DEPTH CHANNEL

(6) H<sub>0</sub> = TW OR (L<sub>0</sub> + D/2) (WHICHEVER IS GREATER)

(7) H<sub>0</sub> = [1 + K<sub>0</sub> (29.4 L<sub>0</sub> / A<sub>135</sub>)<sup>2</sup>] V<sup>2</sup> / 2g

(8) EL<sub>3</sub> = EL<sub>0</sub> + H<sub>0</sub>

COMMENTS / DISCUSSION:

CULVERT BARREL SELECTED: \_\_\_\_\_

SIZE: 5 - 12' x 12' Box

SHAPE: SQUARE

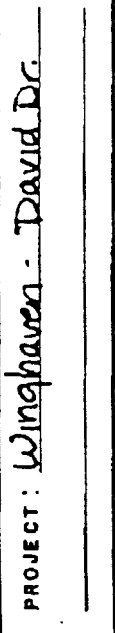
MATERIAL: Concrete

ENTRANCE: 0.013

5/14/08  
 5/15/08  
 5/16/08  
 5/17/08  
 5/18/08

PROJECT: Winghaven - David Dr.  
 STATION: 5+30  
 SHEET \_\_\_\_\_ OF \_\_\_\_\_  
 DESIGNER/DATE: 186 / 12/22/97  
 REVIEWER/DATE: \_\_\_\_\_ / \_\_\_\_\_

ROADWAY ELEVATION: 525.6 (11)  
 EL<sub>1</sub>: 511.10 (11)  
 EL<sub>2</sub>: 510.26 (11)  
 S = S<sub>0</sub> - FALL / L<sub>0</sub>  
 S = \_\_\_\_\_  
 L = 108



HYDROLOGICAL DATA  
 METHOD: \_\_\_\_\_  
 DRAINAGE AREA: \_\_\_\_\_  
 CHANNEL SHAPE: \_\_\_\_\_  
 ROUTING: \_\_\_\_\_  
 OTHER: \_\_\_\_\_  
 DESIGN FLOWS/TAIWATER:  
 R 1 (YEARS) FLOW (cfs) TW (ft)  
15 780.8 \_\_\_\_\_  
100 1085 \_\_\_\_\_

HYDROLOGICAL DATA  
 METHOD: \_\_\_\_\_  
 DRAINAGE AREA: \_\_\_\_\_  
 CHANNEL SHAPE: \_\_\_\_\_  
 ROUTING: \_\_\_\_\_  
 OTHER: \_\_\_\_\_  
 DESIGN FLOWS/TAIWATER:  
 R 1 (YEARS) FLOW (cfs) TW (ft)  
15 780.8 \_\_\_\_\_  
100 1085 \_\_\_\_\_

HYDROLOGICAL DATA  
 METHOD: \_\_\_\_\_  
 DRAINAGE AREA: \_\_\_\_\_  
 CHANNEL SHAPE: \_\_\_\_\_  
 ROUTING: \_\_\_\_\_  
 OTHER: \_\_\_\_\_  
 DESIGN FLOWS/TAIWATER:  
 R 1 (YEARS) FLOW (cfs) TW (ft)  
15 780.8 \_\_\_\_\_  
100 1085 \_\_\_\_\_

CULVERT DESCRIPTION:  
 MATERIAL - SHAPE - SIZE - ENTRANCE  
2-7' x 8' W (15yr)  
2-7' x 8' (100yr)

CULVERT DESCRIPTION	TOTAL FLOW PER BARREL (cfs)	Q/N (1)	INLET CONTROL			OUTLET CONTROL				HEADWATER ELEVATION	OUTLET VELOCITY	COMMENTS	
			HW/D (2)	HW1 (3)	FALL (4)	EL1 (5)	TW (6)	h <sub>0</sub> (7)	h <sub>0</sub> (8)				H (9)
2-7' x 8' W (15yr)	780.8	340.8	1.2	8.4	-	519.5	4.2	5.6	5.6	.5	1.32	517.4	inlet control
2-7' x 8' (100yr)	1085	342	1.36	9.52	-	520.6	5.2	6.1	6.1	.5	2.58	519.24	inlet control

TECHNICAL FOOTNOTES:  
 (1) USE Q/N FOR BOX CULVERTS  
 (2) HW<sub>1</sub>/D = HW / D OR HW<sub>1</sub>/D FROM DESIGN CHARTS  
 (3) FALL = HW<sub>1</sub> - (EL<sub>1</sub> - EL<sub>2</sub>); FALL IS ZERO FOR CULVERTS ON GRADE  
 (4) EL<sub>1</sub> = HW<sub>1</sub>; EL<sub>1</sub> (INVERT OF INLET CONTROL SECTION)  
 (5) TW BASED ON DOWNSTREAM CONTROL OR FLOW DEPTH IN CHANNEL  
 (6) h<sub>0</sub> = TW OR (4.0/D) (WHICHEVER IS GREATER)  
 (7) H = [1 + h<sub>0</sub><sup>5</sup> (29n<sup>2</sup>L) / A133] V<sup>2</sup> / 2g  
 (8) EL<sub>h0</sub> = EL<sub>1</sub> + H + h<sub>0</sub>

SUBSCRIPT DEFINITIONS:  
 1. APPROXIMATE  
 2. CULVERT FACE  
 3. DESIGN HEADWATER  
 4. HEADWATER IN INLET CONTROL  
 5. HEADWATER IN OUTLET CONTROL  
 6. INLET CONTROL SECTION  
 7. OUTLET  
 8. STREAMBED AT CULVERT FACE  
 9. TAILWATER

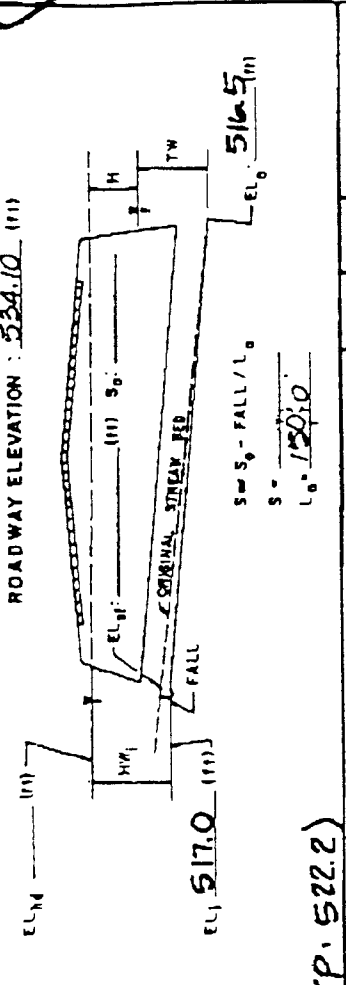
COMMENTS / DISCUSSION:  
 CULVERT BARREL SELECTED:  
 SIZE: 7' H x 8' W - 2  
 SHAPE: \_\_\_\_\_  
 MATERIAL: CONC.  
 ENTRANCE: R-013

COMMENTS / DISCUSSION:  
 CULVERT BARREL SELECTED:  
 SIZE: 7' H x 8' W - 2  
 SHAPE: \_\_\_\_\_  
 MATERIAL: CONC.  
 ENTRANCE: R-013



PROJECT: Winghaven - Winghaven Dr.  
 STATION: 59+00  
 SHEET      OF       
 DESIGNER / DATE: TDB / 11/22/17  
 REVIEWER / DATE:     /    

CULVERT DESIGN FORM



HYDROLOGICAL DATA  
 METHOD:       
 ORAIRAGE AREA:       STREAM SLOPE  
 CHANNEL SHAPE:       
 ROUTING:       OTHER:       
 DESIGN FLOWS/TAIWATER  
 R.L. (YEARS) FLOW (cfs) TW (ft)  
15 3019  
100 4196

(FP: 522.2)

CULVERT DESCRIPTION: MATERIAL - SHAPE - SIZE - ENTRANCE	TOTAL FLOW PER CHANNEL Q (11+2)	INLET CONTROL		HEADWATER CALCULATIONS				OUTLET CONTROL	VELOCITY	COMMENTS	
		HW <sub>1</sub> /D (12)	HW <sub>1</sub> (11)	FALL (13)	EL <sub>I</sub> (14)	TW (15)	4c				h <sub>0</sub> (16)
4-10'h x 12'w (15)	3019	0.85	9.5	525.5	4.9	7.45	0.5	1.1	524.1	526.5	Inlet Control
4-10'h x 12'w (100)	4196	1.08	10.8	527.8	6.2	8.1	0.5	2.01	526.6	527.8	"
USE # FROM FEMO											
4-10'h x 12'w	244	0.73	7.3	524.3							

TECHNICAL FOOTNOTES:  
 (1) USE Q/NB FOR BOX CULVERTS  
 (2) HW<sub>1</sub>/D = HW<sub>1</sub>/D OR HW<sub>1</sub>/D FROM DESIGN CHARTS  
 (3) FALL = HW<sub>1</sub> - (EL<sub>M</sub> - EL<sub>O</sub>); FALL IS ZERO FOR CULVERTS ON GRADE  
 (4) EL<sub>M</sub> = HW<sub>1</sub> + EL<sub>I</sub> (INVERT OF INLET CONTROL SECTION)  
 (5) TW BASED ON DOWN STREAM CONTROL OR FLOW DEPTH IN CHANNEL  
 (6) h<sub>0</sub> = TW or (d<sub>c</sub><sup>3</sup>/D<sup>2</sup>) WHICHEVER IS GREATER  
 (7) H = [(h<sub>0</sub> + h<sub>0</sub>) (29.8 L) / R<sup>1.33</sup>]<sup>2/3</sup> V<sup>2</sup> / 2g  
 (8) EL<sub>O</sub> = EL<sub>O</sub> + H + h<sub>0</sub>

SUBSCRIPT DEFINITIONS:  
 1. APPROXIMATE  
 2. CULVERT FACE  
 3. DESIGN HEADWATER  
 4. HEADWATER IN INLET CONTROL  
 5. HEADWATER IN OUTLET CONTROL  
 6. INLET CONTROL SECTION  
 7. OUTLET CONTROL SECTION  
 8. STREAMBED AT CULVERT FACE  
 9. STREAMBED AT TAILWATER

COMMENTS / DISCUSSION:  
 CULVERT BARREL SELECTED:  
 SIZE: 4-10'h x 12'w  
 SHAPE:       
 MATERIAL: Concrete  
 ENTRANCE: R.O.D.

6/17/18

KDG. MH FILE

980100

JUL 02 1998

Kuhlmann design Group, Inc.

6 Westbury Drive, St. Charles, MO 63301-2571  
Phone 314.946.5566 • Fax 314.946.6713

FACSIMILE TRANSMISSION

PLEASE DELIVER IMMEDIATELY

*CONNECTION JULY 2, 98*

DATE: 7/2/98

TO: Mr. Ron Pagan

COMPANY:

FROM: Sam Elcott *SEL*

TIME

FAX #

PROJECT = 970231

SENT BY

Date	7-2-98	# of pages	1
From	SAL ELKOTT		
Co	KALC		
Phone #		Phone #	
Fax #		Fax #	
Post-It* Fax Note	7671	To	JIM CANNADY
		Co/Dept	PRS
		Phone #	
		Fax #	

These are the floor elevations for the Winghaven Drive tunnel as designed by Pickett Ray and Silver (PRS). These are based on PRS plans dated December 1997 and last revised on March 27, 1998. Mr. Jim Cannady verified these for me this morning. In addition, He said that even though the tunnel floor elevations are not called out on the drawings (as you have correctly stated), PRS' intent is for the tunnels to slope at one half of one percent (0.005 foot per foot). Based on this slope and the centerline tunnel floor elevation that is shown on the roadway profile one can verify these elevations.

- with length = 128' centerline floor elevation = 575.00  
 West Side floor elevation = 574.68 (measured at end of tunnel <sup>64'</sup> away from roadway centerline)  
 East Side floor elevation = 575.32 (measured at end of tunnel <sup>64'</sup> away from roadway centerline)
- with length = 100' centerline floor elevation = 580.30  
 West Side floor elevation = 580.05 (measured at end of tunnel 50' away from roadway centerline)  
 East Side floor elevation = 580.55 (measured at end of tunnel 50' away from roadway centerline)

It is understood that you may need to change these lengths by few feet and the elevations by few tenths. It would be necessary to let Jim and us know of these changes. We at the St. Charles office have to design for the drainage of these tunnels.

Copy: Jim Cannady, Frank Bauer, Jim Poole

PLEASE COVER PAGE ONE

IF YOU ENCOUNTER DIFFICULTIES IN RECEIVING THIS TRANSMISSION  
PLEASE CALL 314.946.5566

WARNING

This communication is confidential, may constitute non-public information, and is intended only for the use of the addressee. Unauthorized use, disclosure, or distribution is strictly prohibited and may be unlawful. If you have received this communication in error, please immediately notify us at 314.946.5566 and return the message to the address above via the U.S. Postal Service. We will reimburse nominal costs you incur in notifying and returning the message to us. Thank you.

Kuhlmann *design* Group, Inc.

Transportation Department

66 Progress Parkway

St. Louis, Missouri 63043

Telephone: (314) 434-8898

Fax: (314) 434-8280

E-Mail: [kdgmh@kdginc.com](mailto:kdgmh@kdginc.com)

## FAX TRANSMITTAL COVER SHEET

TO: MR. FRANK GODWIN P.E.

FAX NO. 314 240 5511

CITY OF OFALLON

DATE: 25 JUNE 1998

138 SOUTH MAIN STREET

PHONE 314 240 2000

OFALLON MISSOURI 63366

FROM: RONALD C. PAGAN, P.E.

PROJECT NO. 980100

MESSAGE: ATTACHED IS CULVERT DESIGN CRITERIA WE DISCUSSED.

THANK YOU

TOTAL NUMBER OF PAGED TRANSMITTED INCLUDING COVER PAGE: 2

If you encounter difficulties in receiving this transmission, please call (314) 434-8898.

### WARNING

The information contained in this communication is confidential, may constitute non-public information, and is intended only for the use of the addressee. Unauthorized use, disclosure or copying is strictly prohibited and may be unlawful. If you have received this communication in error, please immediately notify us at (314) 434-8898 and return the original message to us at the address above via the US postal service. We will reimburse nominal costs you incur in notifying and returning the message to us.

Thank you

## REINFORCEMENT

### BAR COVER - AASHTO 8.22

CLEAR DIMENSIONS TO BE SHOWN ON PLANS:

- TOP SLAB - TOP REINFORCING = 2" CL.  
BOTTOM REINFORCING = 1" CL.
- BOTTOM - TOP REINFORCING = 1-1/2" CL.  
BOTTOM REINFORCING = 3" CL.
- SIDEWALLS - REINFORCEMENT STREAM FACE = 1-1/2" CL.  
REINFORCEMENT FILL FACE = 2" CL.

1 1/2"

### MAXIMUM BAR LENGTHS

LONGITUDINAL BARS SHOULD BE MADE FULL LENGTH WITHOUT SPLICING UP TO ABOUT 40'-0"; SPLICE IF LONGER. BARS #5 AND LARGER MAY BE USED TO A LENGTH OF 60'-0" WITHOUT SPLICING.

### BAR SPLICES

SEE SECTION 2.4 FOR MINIMUM BAR LAP AND TENSION SPLICES IN REINFORCEMENT. USE A CLASS C SPLICE FOR LONGITUDINAL BAR (22" MIN.).

### BOX CULVERTS ON ROCK

VERTICAL BARS IN THE WALLS SHALL SET ON ROCK. E1 & E2 BARS IN THE WING SHALL BE SET 12" INTO ROCK AND GROUTED (SEE SEC. 4 F1 FOR NOTE FOR PLANS).

### GENERAL NOTES:

#### CONSTRUCTION SPECIFICATIONS:

All materials and methods of construction shall meet the requirements of MoDot Standard Specifications for Highway Construction 1996.

#### DESIGN SPECIFICATIONS:

A.A.S.H.T.O. - 1996  
Service Load Design

#### DESIGN LOADING:

HS20  
Earth 120#/Cu. Ft.,  
Equivalent Fluid Pressure 30#/Cu Ft.

#### DESIGN UNIT STRESSES:

Class B Concrete (Substructure)  $f'c = 3,000$  psi  
Reinforcing Steel (Grade 60)  $f_y = 60,000$  psi

#### JOINT FILLER:

All Joint Filler shall meet the requirements of Std. Spec. 1057.2.4, except as noted.

Joint filler shall be securely stitched to one face of the concrete with No. 10 gage copper wire or No. 12 gage soft drawn galvanized steel wire.

#### REINFORCING STEEL:

Minimum clearance to reinforcing steel shall be 1-1/2", unless otherwise shown.

Lap all reinforcing 24 bar diameters unless otherwise noted.

ST. LOUIS

COUNTY

A100

# Hydraulic Structures

## REINFORCEMENT

### BAR COVER - AASHTO 8.22

CLEAR DIMENSIONS TO BE SHOWN ON PLANS:

- |           |   |                           |                     |     |
|-----------|---|---------------------------|---------------------|-----|
| TOP SLAB  | - | TOP REINFORCING           | = 2" CL.            | 1/2 |
|           |   | BOTTOM REINFORCING        | = <del>1" CL.</del> |     |
| BOTTOM    | - | TOP REINFORCING           | = 1-1/2" CL.        |     |
|           |   | BOTTOM REINFORCING        | = 3" CL.            |     |
| SIDEWALLS | - | REINFORCEMENT STREAM FACE | = 1-1/2" CL.        |     |
|           |   | REINFORCEMENT FILL FACE   | = 2" CL.            |     |

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PROPOSED BOX CULVERT  
5'-12" w X 12" h

A 500

490

HL=489.0

484  
496

498

500

502

504

506

65+00

64+00

60+29

504

502

500

498

496

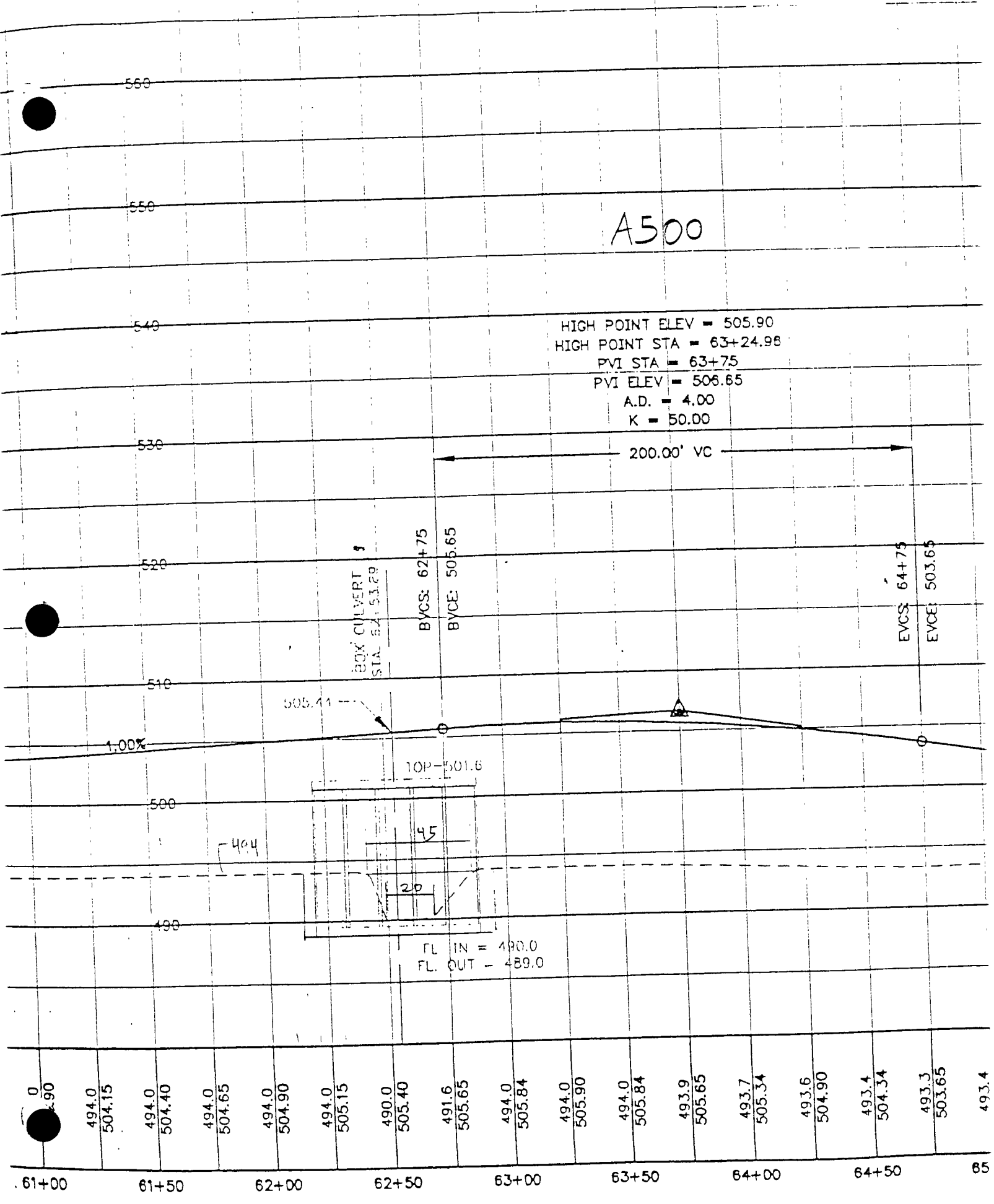
494

HL=490.0

500

SHEET 5 OF 25

U  
UN  
PL  
TH



A500

HIGH POINT ELEV = 505.90  
 HIGH POINT STA = 63+24.98  
 PVI STA = 63+75  
 PVI ELEV = 506.65  
 A.D. = 4.00  
 K = 50.00

200.00' VC

BOX CULVERT  
 STA. 62+53.29

BYCS: 62+75  
 BYCE: 506.65

EVCS: 64+75  
 EVCE: 503.65

505.11

1.00%

TOP = 501.6

40.4

45

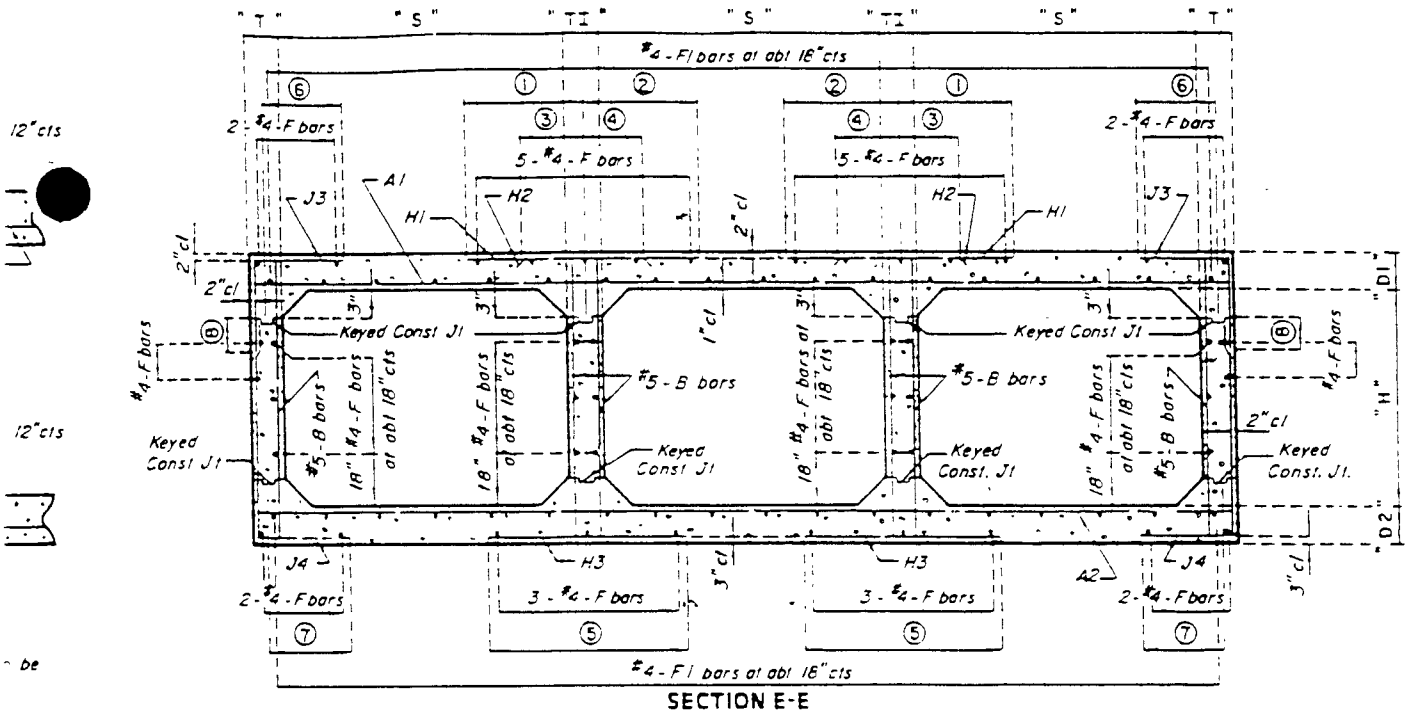
20

FL IN = 490.0  
 FL OUT = 489.0

0	494.0	494.0	494.0	494.0	494.0	490.0	491.6	494.0	494.0	493.9	493.7	493.6	493.4	493.3	493.4
2.90	504.15	504.40	504.65	504.90	505.15	505.40	505.65	505.84	505.90	505.84	505.65	505.34	504.90	503.65	503.65
61+00	61+50	62+00	62+50	63+00	63+50	64+00	64+50	65							

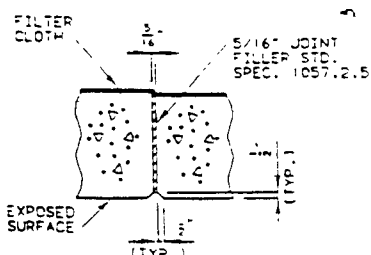
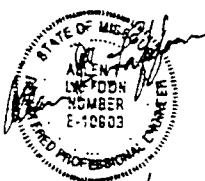






SECTION E-E

REINFORCING BAR LENGTHS																
H1	①	and	②	KL	K	Coefficient shown below										
H2	③	and	④	KL	L	"S" + "T"										
H3	⑤	0.65L			H3	bars to be centered on interior walls										
J3	⑥	and	J4	⑦	0.3L	J3	⑧									2' 3"
* Continue H1 bars across center span with an additional F bar in middle of center span																
FOR DESIGN FILL SEE DATA SHEET	"S"															
	8' and 9'				10 and 11'				12 and 13'				14 and 15'			
	①	②	③	④	①	②	③	④	①	②	③	④	①	②	③	④
12"	.54	*	.31	.39	.48	*	.28	.33	.42	*	.25	.29	.36	*	.25	.26
13" thru 18"	.48	*	.30	.34	.41	*	.28	.28	.39	*	.25	.26	.34	.41	.25	.25
19" thru 2' 0"	.44	*	.30	.30	.38	*	.28	.28	.36	*	.25	.25	.32	.39	.25	.25
2' 1" thru 3' 0"	.40	*	.30	.30	.35	*	.28	.28	.34	.39	.25	.25	.31	.37	.25	.25
3' 1" thru 4' 0"	.35	*	.30	.30	.32	.37	.28	.28	.32	.37	.25	.25	.30	.36	.25	.25
4' 1" thru 5' 0"	.32	.37	.30	.30	.30	.35	.28	.28	.30	.35	.25	.25	.30	.35	.25	.25
5' 1" and over	.31	.35	.30	.30	.30	.34	.28	.28	.30	.34	.25	.25	.30	.34	.25	.25



DETAIL OF TRANSVERSE JOINT THRU BARREL OF CULVERT

NOTE: USE A TRANSVERSE JOINT WHEN BARREL IS OVER 75' LONG BETWEEN HEADWALLS AND NOT ON ROCK.

A FILTER CLOTH THREE FOOT IN WIDTH AND DOUBLE THICKNESS SHALL BE APPLIED TO ALL TRANSVERSE JOINTS IN THE TOP SLAB AND SIDEWALLS. THE MATERIAL SHALL BE CENTERED ON THE JOINT AND THE EDGES SEALED WITH A MASTIC OR WITH TWO SIDED TAPE. THE FILTER CLOTH SHALL BE A GEOTEXTILE MEETING THE APPROVAL OF THE ENGINEER AND HAVING A GRAB TENSILE STRENGTH OF 180 LBS. (ASTM D-4632) APPARENT OPENING SIZE OF 50 TO 100 (ASTM D-4751). NO DIRECT PAYMENT WILL BE MADE FOR FURNISHING AND INSTALLING THE FILTER CLOTH.

USE ADDITIONAL TRANSVERSE JOINTS TO PROVIDE 50' MAXIMUM SPACING BETWEEN JOINTS. IF MORE THAN ONE TRANSVERSE JOINT IS REQUIRED, SEE STANDARD 703.74 FOR DETAILS.

GENERAL NOTES:

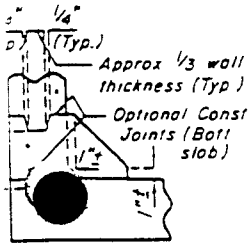
FOR DIMENSIONS AND SIZE AND SPACING OF REINFORCING STEEL SEE SPECIAL BRIDGE SHEET AND STANDARD 703.76

LAP ALL LONGITUDINAL BARS A MINIMUM OF 22" AT SPLICES

MINIMUM CLEARANCE TO REINFORCING STEEL SHALL BE 1/2" UNLESS OTHERWISE SHOWN

JOINT FILLER SHALL BE SECURELY STITCHED TO ONE FACE OF THE CONCRETE WITH NO. 10 GAGE COPPER WIRE OR NO. 12 GAGE SOFT DRAWN GALVANIZED STEEL WIRE

Use of least one Keyed Const Joint



TAIL OF ALTERNATE KEYED CONST. JOINTS BOTTOM SLAB ONLY

MISSOURI HIGHWAY AND TRANSPORTATION COMMISSION

**CONCRETE TRIPLE BOX STRUCTURE STRAIGHT WINGS**

(SQUARE)

DRAWING 703.70D

REV AUGUST 1991

SHEET 1 of 2

# GEOTECHNICAL REPORT



July 9, 1998

ADD. MH FILE

980100

JUL 7 1998


Mr. David Rogers  
 Fred Weber, Inc.  
 % Mr. Ronald C. Pagan, P.E.  
 Kuhlmann Design Group, Inc.  
 66 Progress Parkway  
 Maryland Heights, MO 63043-3706

RE: Addendum N<sup>o</sup> 1  
 Winghaven Box Culverts  
 O'Fallon, Missouri  
 SCI N<sup>o</sup> 980495.11

Dear Mr. Pagan:

This letter provides the additional geotechnical information for the Winghaven Box Culverts you requested to supplement our letter to you dated June 29, 1998. Three specific items presented herein pertain to the following:

- 1) Rock mats for structural slab base footings.
- 2) Anticipated settlements.
- 3) Backfill and fluid pressures for below-grade walls.

We understand that the bearing capacity required for the box culverts in the lowland areas will be 1,500 pounds per square foot (psf) and we provided an allowable bearing capacity of 1,200 psf for one box culvert that will pass under Charlie Drive near station 62+50. We recommend that 2 feet of soil be removed below the footing subgrade elevation and replaced with compacted granular material for this culvert. The replacement material should consist of a 3-inch minus gradation crushed stone. This rock mat will help to bridge the soft and wet foundation soils. A similar procedure of varying depths may be utilized for the other culverts in the lowland areas since we anticipate construction difficulties due to the high groundwater elevations.

The box culverts in the highland areas (culverts A and B) will likely be constructed on excavated rock. We anticipate negligible settlements of the foundation rock due to the weight of the structures and fills. In the lowland areas, however, we anticipate total settlement of the foundation soils due to the weight of the structure and fill to be placed to be about 3 to 6 inches. Some of this settlement will likely occur during construction. If construction of the culverts in the lowland areas is not delayed until after the settlement due to the fill has occurred, the structure will likely settle. However, we anticipate this settlement will likely be relatively uniform across the footprint due to the rigidity of the reinforced concrete base mat and structure. A differential settlement of less than 1½ inches can be anticipated across the whole footprint for these structures.

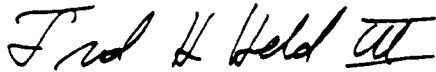
Our letter dated June 29, 1998 states that to use the "granular" values of equivalent fluid unit weight for earth pressures that the granular backfill material should extend horizontally from the

wall at least half of the wall height. This distance is not required to provide positive foundation drainage to prevent buildup of hydrostatic pressures. A minimum horizontal distance of about 18 inches with a perforated drain pipe should be sufficient to provide this drainage. Therefore, an equivalent fluid unit weight of 60 pounds per cubic foot may be used to design the below-grade walls assuming the hydrostatic pressures are relieved through proper drainage.

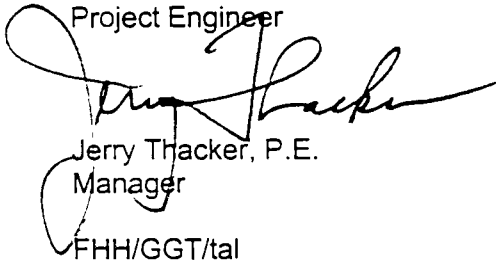
We appreciate the opportunity to be of service to you on this project. If you have any questions or comments, please call.

Respectfully,

SCI

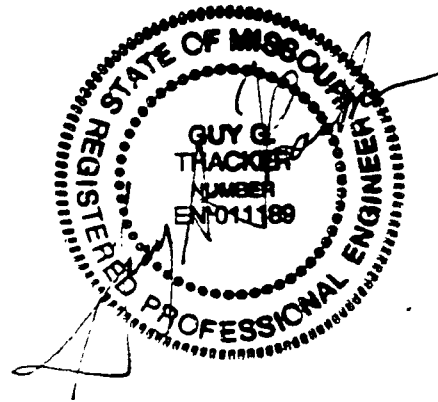


Fred H. Held III  
Project Engineer



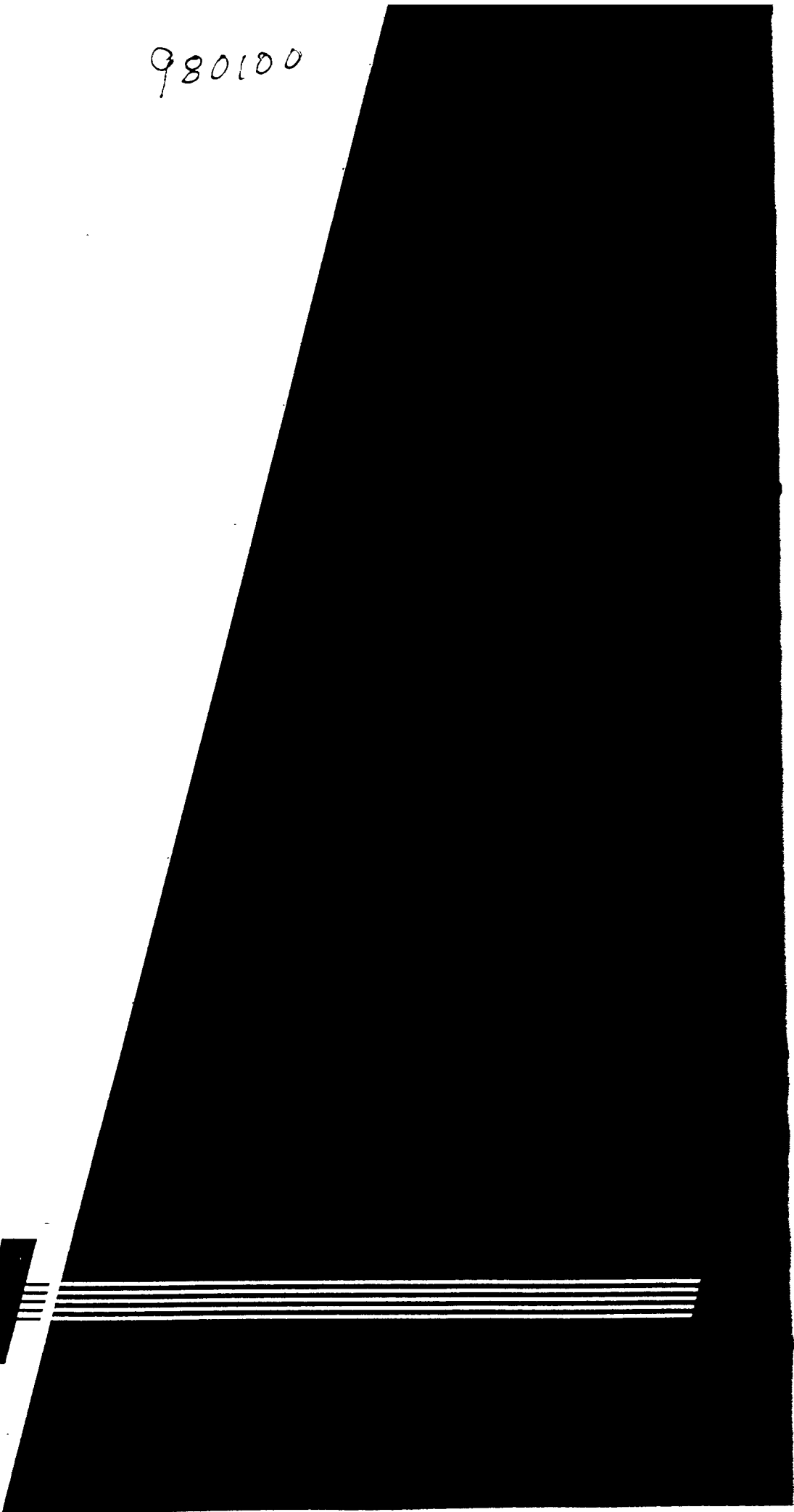
Jerry Thacker, P.E.  
Manager

FHH/GGT/tal



c: Mr. Dave Rogers, Fred Weber, Inc. (1)

980100



**SCI**





June 29, 1998

Mr. David Rogers  
Fred Weber, Inc.  
% Mr. Ronald C. Pagan, P.E.  
Kuhlmann Design Group, Inc.  
66 Progress Parkway  
Maryland Heights, MO 63043-3706

RE: Winghaven Box Culverts  
O'Fallon, Missouri  
SCI N<sup>o</sup> 980495.11

Dear Mr. Pagan:

At the request of Mr. David Rogers with Fred Weber, Inc., this letter provides geotechnical design recommendations for five box culverts planned for the Winghaven development roadways. Plan and Profile sheets prepared by Pickett, Ray & Silver, Inc. (PRS), revised March 25 or 27, 1998, depict the locations and elevations of the culverts. Three of the culverts will cross under Winghaven Drive near stations 17+00, 30+50, 59+00. One culvert will pass under David Drive near station 5+50, and one culvert will pass under Charlie Drive near station 62+50. In this letter the box culverts will be named A, B, C, D and E, respectively. Culverts A and B will be tunnels for golf carts to underpass Winghaven Drive in the uplands part of the Winghaven development. The remaining will be multiple cell box culverts for existing creeks in lowland areas to pass under planned roadways. We understand that these culverts will be cast-in-place, reinforced concrete structures that will have light to moderate loads.

We previously explored parts of the Winghaven development in our report, "Preliminary Exploration of Subsurface Conditions and Foundation Recommendations - WINGHAVEN PROJECT SITE COMMERCIAL, RESIDENTIAL, AND GOLF COURSE COMMUNITY - O'FALLON, MISSOURI," dated July 1997 (Revised January 1998). In that exploration we drilled B2 and B3 in the uplands near the golf cart underpasses, B21 in the lowland area near culvert C, and B14 in the bottoms land near culvert E. The four boring logs are included in the Appendix of this letter. These borings indicate that excavations for culverts A and B will encounter rock in the form of weathered siltstone or shale for the full depths of the structures. Also, B2 encountered auger refusal near El. 576.5 and the planned bottom of culvert A is near El. 574. Some or all of this rock may be removed in open-cut excavations with bull dozers equipped with rippers. However, intact ledges of hard rock, boulders, or sound bedrock may be encountered that could require blasting.

SCI explored the subsurface conditions near culverts C, D and E on June 25, 1998 using hand auger methods. The hand auger borings, TH1, TH2, and TH3, were located near culverts C, D and E, respectively, by measuring from existing site features and improvements shown of the plans prepared by PRS. The hand augers were advanced to termination depths of 5, 6, and 7½ feet in TH1, TH2, and TH3, respectively. The soils generally encountered were soft to medium stiff, low plastic silty clays and clayey silts. TH1 terminated in a mixture of silty clay, gravel and sand at a depth of 5 feet, which is about 3 feet above the anticipated bearing elevation of culvert C. TH2 and TH3 terminated at depths of 6 and 7½ feet, respectively, due to caving conditions in the holes. We estimate the termination elevations were near the bearing

elevations of culverts D and E. Groundwater was encountered in the hand auger borings at depths of 4 or 5 feet. The nature and thickness of the soils encountered and the results of the field sampling and testing are shown on the Borings Logs, Figures 1-1 through 1-3.

The varied conditions at the culvert locations require different allowable bearing capacities for the locations. An allowable bearing capacity of 10,000 pounds per square foot (psf) may be used to design the structural base slab for culverts A and B if they bear on the weathered siltstone or shale as indicated by B2 and B3 or if they encounter bedrock. An allowable bearing capacity of 3,000 psf may be used to design culvert C if it bears on the anticipated mixture of gravel and sand with some or no clay. An allowable bearing capacity of 1,500 psf may be used to design culvert D if it bears on the silty clay encountered in TH2. An allowable bearing capacity of 1,200 psf may be used to design culvert E.

We understand that higher bearing capacities will be required for culverts D and E. The soft soils below the base of the culverts may be removed and replaced with compacted, crushed rock, such as MODOT Type I Aggregate. The area of removal should extend down and outside the base footprint at an angle of 45 degrees to form a larger area to bear on the soft soils. The depth of removal will vary depending on the allowable bearing capacity required. We anticipate about 5 feet of soft soil will need to be removed and replaced with crushed rock to increase the allowable bearing capacity of the culverts to 2,000 or 3,000 psf.

In the lowland areas, placing fill to raise the roadway above existing grade will result in settlement as consolidation of the soft, underlying soils occurs. A delay in construction is anticipated to allow some or most of that settlement to occur prior to construction. We anticipate this delay to be about 30 to 120 days. This delay will likely not apply to culvert C since we anticipate it will bear on sand and gravel near bedrock elevations. Culverts D and E should not be constructed until most of the settlement due to the weight of the fills has occurred. Surcharging can be used as a means to accelerate consolidation due to the weight of fill. Deep fill in the lowland areas should be monitored with settlement plates to assess when most of the settlement has occurred and construction can continue.

The below-grade walls of the box culverts will be required to resist earth pressures. These include the outside walls of the culverts and the wing-walls that may extend from the culverts designed to accommodate surface grade changes.

The equivalent fluid unit weights tabulated below provide recommended lateral earth pressures for design of these walls. Values for granular material should only be used if the granular backfill extends from the wall a lateral distance of at least one-half the wall height. This table assumes that positive foundation drainage is provided to prevent buildup of hydrostatic pressure. The below-grade walls should be designed to resist an additional uniform lateral load of one-half of the surface loads.

Backfill Type	Fixed-Headed Walls (pcf)	Free-Headed Walls (pcf)
Cohesive Soil	60	50
Granular Material	45	40

A fixed-headed wall is a wall which is not permitted to deflect at the top after backfilling. A free-headed wall is designed to deflect at the top and remain fixed at the base, such as a retaining wall. A wing-wall attached to a fixed-headed wall should be considered fixed-headed unless the structural design permits independent rotation.

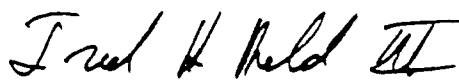
The maximum toe pressures for wing-walls should not exceed the bearing capacities recommended in this letter. Walls bearing in soil can be designed with a coefficient of friction between the base of a concrete footing and the subgrade soil of 0.3. A passive soil resistance equal to a uniform pressure of 300 psf may be used for natural soil against the face of the exterior base or a key below the base of a retaining wall. Soil backfilled against the exterior face of a retaining wall should not be assumed to provide any lateral resistance.

We recommend that all below-grade walls and retaining walls be provided with a foundation drainage system. A typical below-grade wall drain detail is shown in Figure 2. It should consist of a perforated pipe to transport the fluids collected from the granular backfill to daylight. Granular drainage material around the pipe should consist of 1-inch clean, "GP" classified crushed rock. A synthetic filter fabric indicated on Figure 2 should be Mirafi 140N or equivalent. A minimum 4-inch diameter perforated drain pipe should be used.

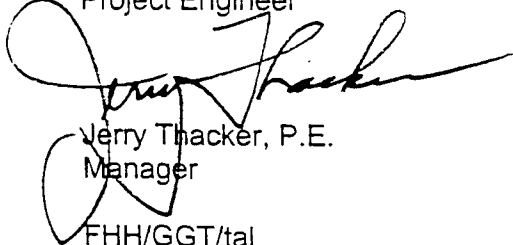
We appreciate the opportunity to be of service to you on this project. If you have any questions or comments, please call.

Respectfully,

SCI



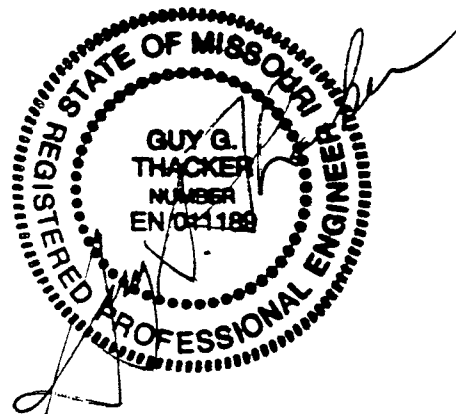
Fred H. Held III  
Project Engineer



Jerry Thacker, P.E.  
Manager

FHH/GGT/tal

c: Mr. Dave Rogers, Fred Weber, Inc. (1)





**BORING LOG  
LEGEND AND NOMENCLATURE**

Items shown in Boring Logs refer to the following:

(Where shown in parenthesis, sampling and testing were performed in general accordance with applicable ASTM standard methods or practices.)

1. **Depth** - Depth below ground surface (feet).
2. **Sample** - Types designated by letters.
  - SS** - Split-spoon sample, disturbed, obtained by driving 2-inch O.D. split-spoon sampler (ASTM D 1586).
  - NX** - Diamond core bit sample, nominal 2-inch diameter rock sample (ASTM D 2113).
  - ST** - Thin-walled tube sample, undisturbed, obtained by penetration of a 3-inch diameter tube (ASTM D 1587).
  - CS** - Continuous sample tube system, undisturbed, obtained by split barrel sampler in conjunction with auger advancement.
  - SV** - Shear vane, field test to determine strength of cohesive soil by pushing or driving a 2-inch diameter vane then shearing by torquing soil in existing and remolded states (ASTM D 2573).
  - AS** - Disturbed samples obtained from auger cuttings.
  - Recovery** - Recovery is expressed as a ratio of the length recovered to the total length pushed, driven, or cored (inches), e.g. - 9/12.
  - Blows** - Numbers indicate blows per six inches of sampler penetration when driven by a 140-pound hammer falling freely 30 inches (ASTM D 1586). When number of blows reaches 50 without six inches of sampler penetration, the result is shown as a ratio of 50 to the actual penetration, e.g. - 50/2 inches.
  - Vane Shear Strength** - Shear strength of soil expressed as the peak strength (existing state)/residual strength (remolded state).
3. **Description** - Description according to the Unified Soil Classification: Description indicates soil constituents and other classification characteristics (ASTM D 2488). A solid line indicates approximate location of stratigraphic change between soil types and the transition may be gradual.
4. **Laboratory Test Results**
  - Natural moisture content in percent (ASTM D 2216).
  - Dry density of sample tested in pounds per cubic foot (pcf).
  - Unconfined compressive strength (ASTM D 2166) in kips per square foot (ksf).
  - Liquid limit (ASTM D 4318) in percent.
  - Plastic limit (ASTM D 4318) in percent.
5. **Remarks/Other Data** - See notation at bottom of log for description of data entries.
  - RQD** - Rock Quality Designation; the ratio between the total length of core segments greater than 4 inches in length and the total length of core drilled (expressed as percentage).



PROJECT WINGHAVEN BOX CULVERTS

TEST PIT NO. TH-1

LOCATION O'Fallon, Missouri

SHEET 1 OF 1

EXCAVATOR SCI

PROJECT NO. 980495.11

SURFACE ELEVATION 524 +/-

EQUIPMENT Hand auger

DATE EXCAVATED 6-25-98

DEPTH (FT.)	FIELD SAMPLE / TEST				DESCRIPTION	UNIFIED SOIL CLASSIFICATION	SEE REMARK NO.	LABORATORY TEST RESULTS					DEPTH (FT.)
	NUMBER	SAMPLE TYPE	FIELD TEST TYPE	SHEAR STRENGTH (KSF)				MOISTURE CONTENT (%)	DRY DENSITY (PCF)	UNCONFINED COMPRESSIVE STRENGTH (KSF)	LIQUID LIMIT	PLASTIC LIMIT	
0					Grayish brown, low plastic SILTY CLAY with trace of fine roots	CL							0
1	1	BS						29					
2.5	2	BS			Brown, low plastic SILTY CLAY with trace of fine gravel	CL		19					2.5
3	3	BS			Brown, low plastic SILTY CLAY and coarse SAND to fine GRAVEL	CL,GC		19					
5					Hand auger refusal at 5.0 ft.								5
7.5													7.5
10													10
12.5													12.5
15													15
17.5													17.5

WATER LEVEL:

NO GROUNDWATER NOTED AT TIME OF EXCAVATION  
 5 FT WHILE EXCAVATING  
 FT \_\_\_\_\_ HRS AFTER EXCAVATING

REMARKS:



# TEST PIT LOG

PROJECT WINGHAVEN BOX CULVERTSTEST PIT NO. TH-2LOCATION O'Fallon, MissouriSHEET 1 OF 1EXCAVATOR SCIPROJECT NO. 980495.11SURFACE ELEVATION 516+/-EQUIPMENT Hand augerDATE EXCAVATED 6-25-98

DEPTH (FT.)	FIELD SAMPLE / TEST				DESCRIPTION	UNIFIED SOIL CLASSIFICATION	SEE REMARK NO.	LABORATORY TEST RESULTS					DEPTH (FT.)
	NUMBER	SAMPLE TYPE	FIELD TEST TYPE	SHEAR STRENGTH (KSF)				MOISTURE CONTENT (%)	DRY DENSITY (PCF)	UNCONFINED COMPRESSIVE STRENGTH (KSF)	LIQUID LIMIT	PLASTIC LIMIT	
0					4 inches TOPSOIL								0
1	1	BS			Brown with gray, low plastic SILTY CLAY with some gray, silt and trace of organics	CL		23					
2.5	2	BS	SV	2.8/ 1.4	Brown and gray, low plastic CLAYEY SILT with trace of fine sand and organics	ML		25					2.5
3	3	BS						21					
4	4	BS			Gray with brown, low plastic SILTY CLAY with trace of fine gravel	CL		24					
5													5
7.5					Hand auger terminated at 6.0 ft.								7.5
10													10
12.5													12.5
15													15
17.5													17.5

WATER LEVEL:

NO GROUNDWATER NOTED AT TIME OF EXCAVATION  
 4 FT WHILE EXCAVATING  
 FT      HRS AFTER EXCAVATING

REMARKS:



# TEST PIT LOG

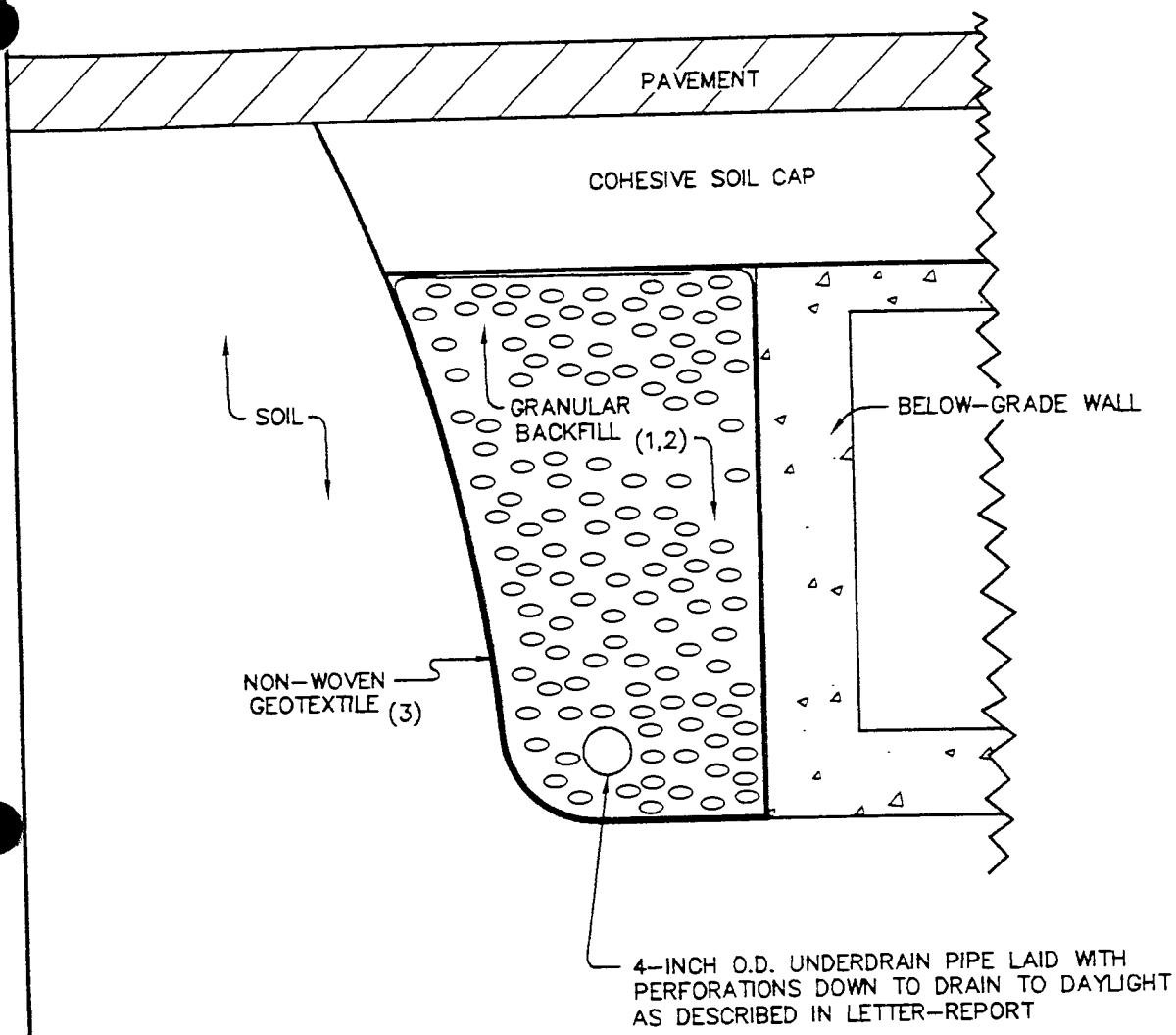
PROJECT WINGHAVEN BOX CULVERTSTEST PIT NO. TH-3LOCATION O'Fallon, MissouriSHEET 1 OF 1EXCAVATOR SCIPROJECT NO. 980495.11SURFACE ELEVATION 494 +/-EQUIPMENT Hand augerDATE EXCAVATED 6-25-98

DEPTH (FT.)	FIELD SAMPLE / TEST				DESCRIPTION	UNIFIED SOIL CLASSIFICATION	SEE REMARK NO.	LABORATORY TEST RESULTS					DEPTH (FT.)
	NUMBER	SAMPLE TYPE	FIELD TEST TYPE	SHEAR STRENGTH (KSF)				MOISTURE CONTENT (%)	DRY DENSITY (PCF)	UNCONFINED COMPRESSIVE STRENGTH (KSF)	LIQUID LIMIT	PLASTIC LIMIT	
0					Brown, low plastic SILTY CLAY	CL							0
1	1	BS			Grayish brown, fine SANDY SILTY CLAY with some fine gravel	SC		21					
2.5	2	BS			Grayish brown, low plastic CLAYEY SILT with fine sand	ML		19					2.5
5	3	BS			Brown and gray, low plastic CLAYEY SILT with some fine sand to fine gravel	ML		35					5
7.5	4	BS			Gray, low plastic CLAYEY SILT with trace of fine gravel Hand auger terminated at 7.5 ft.	ML		29					7.5
10													10
12.5													12.5
15													15
17.5													17.5

WATER LEVEL:

NO GROUNDWATER NOTED AT TIME OF EXCAVATION  
 4 FT WHILE EXCAVATING  
 FT      HRS AFTER EXCAVATING

REMARKS:



**NOTES:**

1. MINIMUM 6" FILTER MATERIAL AROUND PIPE.
2. 1" CLEAN CRUSHED LIMESTONE.
3. TYPICALLY FOUR-OUNCE PER SQUARE YARD


	333 MID RIVERS MALL DRIVE ST. PETERS, MISSOURI 63376
WINGHAVEN BOX CULVERT O'FALLON, MISSOURI	
BELOW-GRADE WALL DRAIN DETAIL	
JUNE 1998	SCI NO. 980495.11

FIGURE 2

APPENDIX



# BORING LOG

PROJECT WINGHAVEN PROJECT SITEBORING NO. B-2LOCATION O'Fallon, MissouriSHEET 1 OF 1DRILLER Midwest Drilling, Inc.PROJECT NO. 97-384-411SURFACE ELEVATION 595+/-DRILLING METHOD 4" CFADATE DRILLED 6-11-97

DEPTH (FT.)	SAMPLE				DESCRIPTION	UNIFIED SOIL CLASSIFICATION	SEE REMARK NO.	LABORATORY TEST RESULTS					DEPTH (FT.)
	NUMBER	TYPE	RECOVERY (IN/IN)	BLOWS (PER 6 IN.)				MOISTURE CONTENT (%)	DRY DENSITY (PCF)	UNCONFINED COMPRESSIVE STRENGTH (KSF)	LIQUID LIMIT	PLASTIC LIMIT	
0					6 inches TOPSOIL	CL/CH							0
2	1	SS		3	Brown and gray, medium plastic SILTY CLAY	CL		26					2
4	2	SS		3	Brown with some gray, low plastic SILTY CLAY	CL		28					4
6	3	SS		3	Brown with some gray, medium plastic SILTY CLAY	CL/CH		25					6
8	4	SS		7	Brown with some gray, high plastic CLAY	CH		29					8
12					Tan, WEATHERED SILTSTONE								12
14	5	SS		50/3				10					14
16	6	AS			Gray with some brown, SILTSTONE								16
18					Auger refusal at 17.5 ft.								18
20													20

## WATER LEVEL:

NO GROUND WATER NOTED AT TIME OF DRILLING

\_\_\_\_\_ FT WHILE DRILLING

\_\_\_\_\_ FT \_\_\_\_\_ HRS AFTER DRILLING

\_\_\_\_\_ FT \_\_\_\_\_ HRS AFTER DRILLING

## REMARKS:



# BORING LOG

PROJECT WINGHAVEN PROJECT SITE

BORING NO. B-3

LOCATION O'Fallon, Missouri

SHEET 1 OF 2

DRILLER Midwest Drilling, Inc.

PROJECT NO. 97-384-411

SURFACE ELEVATION 602+/-

DRILLING METHOD 4" CFA

DATE DRILLED 6-11-97

DEPTH (FT.)	SAMPLE				DESCRIPTION	UNIFIED SOIL CLASSIFICATION	SEE REMARK NO.	LABORATORY TEST RESULTS					DEPTH (FT.)
	NUMBER	TYPE	RECOVERY (IN/IN)	BLOWS (PER 6 IN.)				MOISTURE CONTENT (%)	DRY DENSITY (PCF)	UNCONFINED COMPRESSIVE STRENGTH (KSF)	LIQUID LIMIT	PLASTIC LIMIT	
0					1 inch TOPSOIL	CL/CH	1						0
2	1	SS		3 3 4	Brown with some gray, medium plastic SILTY CLAY	CL		26					2
4	2	SS		2 3 3	Brown with some gray, low plastic SILTY CLAY			25					4
6	3	SS		2 3 4		CH		22					6
8	4	SS		3 3 5	Brown with some gray, high plastic CLAY			33					8
12						CH							12
14	5	SS		3 6 15	Tan, high plastic SHALEY CLAY			30					14
16					Brown, WEATHERED SHALE								16
18													18
20	6	SS		27 50/3				10					20

Continued on sheet 2 of 2

**WATER LEVEL:**

- NO GROUND WATER NOTED AT TIME OF DRILLING
- \_\_\_\_\_ FT WHILE DRILLING
- \_\_\_\_\_ FT \_\_\_\_\_ HRS AFTER DRILLING
- \_\_\_\_\_ FT \_\_\_\_\_ HRS AFTER DRILLING

**REMARKS:**

1) Driller's observation





# BORING LOG

BORING NO. B-2PROJECT WINGHAVEN PROJECT SITESHEET 1 OF 1LOCATION O'Fallon, MissouriPROJECT NO. 97-384-411DRILLER Midwest Drilling, Inc.DATE DRILLED 6-11-97SURFACE ELEVATION 595+/-DRILLING METHOD 4" CFA

DEPTH (FT.)	SAMPLE				DESCRIPTION	UNIFIED SOIL CLASSIFICATION	SEE REMARK NO.	LABORATORY TEST RESULTS					DEPTH (FT.)
	NUMBER	TYPE	RECOVERY (IN/IN)	BLOWS (PER 6 IN.)				MOISTURE CONTENT (%)	DRY DENSITY (PCF)	UNCONFINED COMPRESSIVE STRENGTH (KSF)	LIQUID LIMIT	PLASTIC LIMIT	
0					6 inches TOPSOIL	CL/CH							0
2	1	SS		2 3	Brown and gray, medium plastic SILTY CLAY	CL		26					2
4	2	SS		2 3	Brown with some gray, low plastic SILTY CLAY	CL		28					4
6	3	SS		2 3	Brown with some gray, medium plastic SILTY CLAY	CL/CH		25					6
8	4	SS		3 5 7	Brown with some gray, high plastic CLAY	CH		29					8
12					Tan, WEATHERED SILTSTONE								12
14	5	SS		50/3				10					14
16	6	AS			Gray with some brown, SILTSTONE								16
18					Auger refusal at 17.5 ft.								18
20													20

## WATER LEVEL:

NO GROUND WATER NOTED AT TIME OF DRILLING

FT \_\_\_\_\_ HRS AFTER DRILLING

FT \_\_\_\_\_ HRS AFTER DRILLING

## REMARKS:



# BORING LOG

PROJECT WINGHAVEN PROJECT SITE

BORING NO. B-3

LOCATION O'Fallon, Missouri

SHEET 1 OF 2

DRILLER Midwest Drilling, Inc.

PROJECT NO. 97-384-411

SURFACE ELEVATION 602+/-

DRILLING METHOD 4" CFA

DATE DRILLED 6-11-97

DEPTH (FT.)	SAMPLE				DESCRIPTION	UNIFIED SOIL CLASSIFICATION	SEE REMARK NO.	LABORATORY TEST RESULTS					DEPTH (FT.)
	NUMBER	TYPE	RECOVERY (IN/IN)	BLOWS (PER 6 IN.)				MOISTURE CONTENT (%)	DRY DENSITY (PCF)	UNCONFINED COMPRESSIVE STRENGTH (KSF)	LIQUID LIMIT	PLASTIC LIMIT	
0					1 inch TOPSOIL	CL/CH	1						0
2	1	SS		3 3 4	Brown with some gray, medium plastic SILTY CLAY	CL/CH		26					2
4	2	SS		2 3 3	Brown with some gray, low plastic SILTY CLAY	CL		25					4
6	3	SS		2 3 4				22					6
8	4	SS		3 3 5	Brown with some gray, high plastic CLAY	CH		33					8
14	5	SS		3 6 15	Tan, high plastic SHALEY CLAY	CH		30					14
16					Brown, WEATHERED SHALE								16
20	6	SS		27 50/3				10					20

Continued on sheet 2 of 2

**WATER LEVEL:**

- NO GROUND WATER NOTED AT TIME OF DRILLING
- FT WHILE DRILLING
- FT \_\_\_\_\_ HRS AFTER DRILLING
- FT \_\_\_\_\_ HRS AFTER DRILLING

**REMARKS:**

1) Driller's observation



# BORING LOG

PROJECT WINGHAVEN PROJECT SITEBORING NO. B-3LOCATION O'Fallon, MissouriSHEET 2 OF 2DRILLER Midwest Drilling, Inc.PROJECT NO. 97-384-411SURFACE ELEVATION 602+/-DRILLING METHOD 4" CFADATE DRILLED 6-11-97

DEPTH (FT.)	SAMPLE				DESCRIPTION	UNIFIED SOIL CLASSIFICATION	SEE REMARK NO.	LABORATORY TEST RESULTS					DEPTH (FT.)	
	NUMBER	TYPE	RECOVERY (IN/IN)	BLOWS (PER 6 IN.)				MOISTURE CONTENT (%)	DRY DENSITY (PCF)	UNCONFINED COMPRESSIVE STRENGTH (KSF)	LIQUID LIMIT	PLASTIC LIMIT		
22					Brown, WEATHERED SHALE								22	
24	7	SS		50/3				12						24
26					Drilling terminated at 25.0 ft.								26	
28														28
30														30
32														32
34														34
36														36
38														38
40														40
42														42

## WATER LEVEL:

NO GROUND WATER NOTED AT TIME OF DRILLING

\_\_\_\_\_ FT WHILE DRILLING

\_\_\_\_\_ FT \_\_\_\_\_ HRS AFTER DRILLING

\_\_\_\_\_ FT \_\_\_\_\_ HRS AFTER DRILLING

## REMARKS:



# BORING LOG

PROJECT WINGHAVEN PROJECT SITEBORING NO. B-14LOCATION O'Fallon, MissouriSHEET 1 OF 1DRILLER Midwest Drilling, Inc.PROJECT NO. 97-384-411SURFACE ELEVATION 494+/-DRILLING METHOD 4" CFADATE DRILLED 6-9-97

DEPTH (FT.)	SAMPLE				DESCRIPTION	UNIFIED SOIL CLASSIFICATION	SEE REMARK NO.	LABORATORY TEST RESULTS					DEPTH (FT.)	
	NUMBER	TYPE	RECOVERY (IN/IN)	BLOWS (PER 6 IN.)				MOISTURE CONTENT (%)	DRY DENSITY (PCF)	UNCONFINED COMPRESSIVE STRENGTH (KSF)	LIQUID LIMIT	PLASTIC LIMIT		
0					5 inches TOPSOIL	CL	1						0	
2	1	SS		3 2 2	Gray and brown, low plastic SILTY CLAY				23					2
4	2	SS		2 2 4					22					4
6	3	SS		0 1 2					28					6
8	4	SS		0 1 1					31					8
10					Drilling terminated at 10.0 ft.								10	
12													12	
14													14	
16													16	
18													18	
20													20	

## WATER LEVEL:

NO GROUND WATER NOTED AT TIME OF DRILLING  
5.5 FT WHILE DRILLING  
 FT \_\_\_\_\_ HRS AFTER DRILLING  
 FT \_\_\_\_\_ HRS AFTER DRILLING

## REMARKS:

1) Driller's observation



# BORING LOG

PROJECT WINGHAVEN PROJECT SITEBORING NO. B-21LOCATION O'Fallon, MissouriSHEET 1 OF 1DRILLER Midwest Drilling, Inc.PROJECT NO. 97-384-411SURFACE ELEVATION 524+/-DRILLING METHOD 4" CFADATE DRILLED 6-10-97

DEPTH (FT.)	SAMPLE				DESCRIPTION	UNIFIED SOIL CLASSIFICATION	SEE REMARK NO.	LABORATORY TEST RESULTS					DEPTH (FT.)
	NUMBER	TYPE	RECOVERY (IN/IN)	BLOWS (PER 6 IN.)				MOISTURE CONTENT (%)	DRY DENSITY (PCF)	UNCONFINED COMPRESSIVE STRENGTH (KSF)	LIQUID LIMIT	PLASTIC LIMIT	
0					3 inches TOPSOIL		1						0
1	1	SS		3	Brown and gray, low plastic CLAYEY SILT to SILTY CLAY	ML/CL		25					2
2				2									
3				1									
4	2	SS		3	Brown and gray, low plastic SILTY CLAY with some rock fragments	CL		22					4
5				2									
6				5									
6	3	SS		15	ROCK FRAGMENTS with some brown and gray, low plastic silty clay	GC		21					6
7				18									
8				8									8
8	4	SS		50/1	ROCK and ROCK FRAGMENTS		2						8
10					Drilling terminated at 10.0 ft.								10
12													12
14													14
16													16
18													18
20													20

## WATER LEVEL:

NO GROUND WATER NOTED AT TIME OF DRILLING  
 6 FT WHILE DRILLING  
 FT \_\_\_ HRS AFTER DRILLING  
 FT \_\_\_ HRS AFTER DRILLING

## REMARKS:

- 1) Driller's observation
- 2) Driller's observation

# HYDRAULIC ANALYSIS

David Dr. (Winghaven 97034)

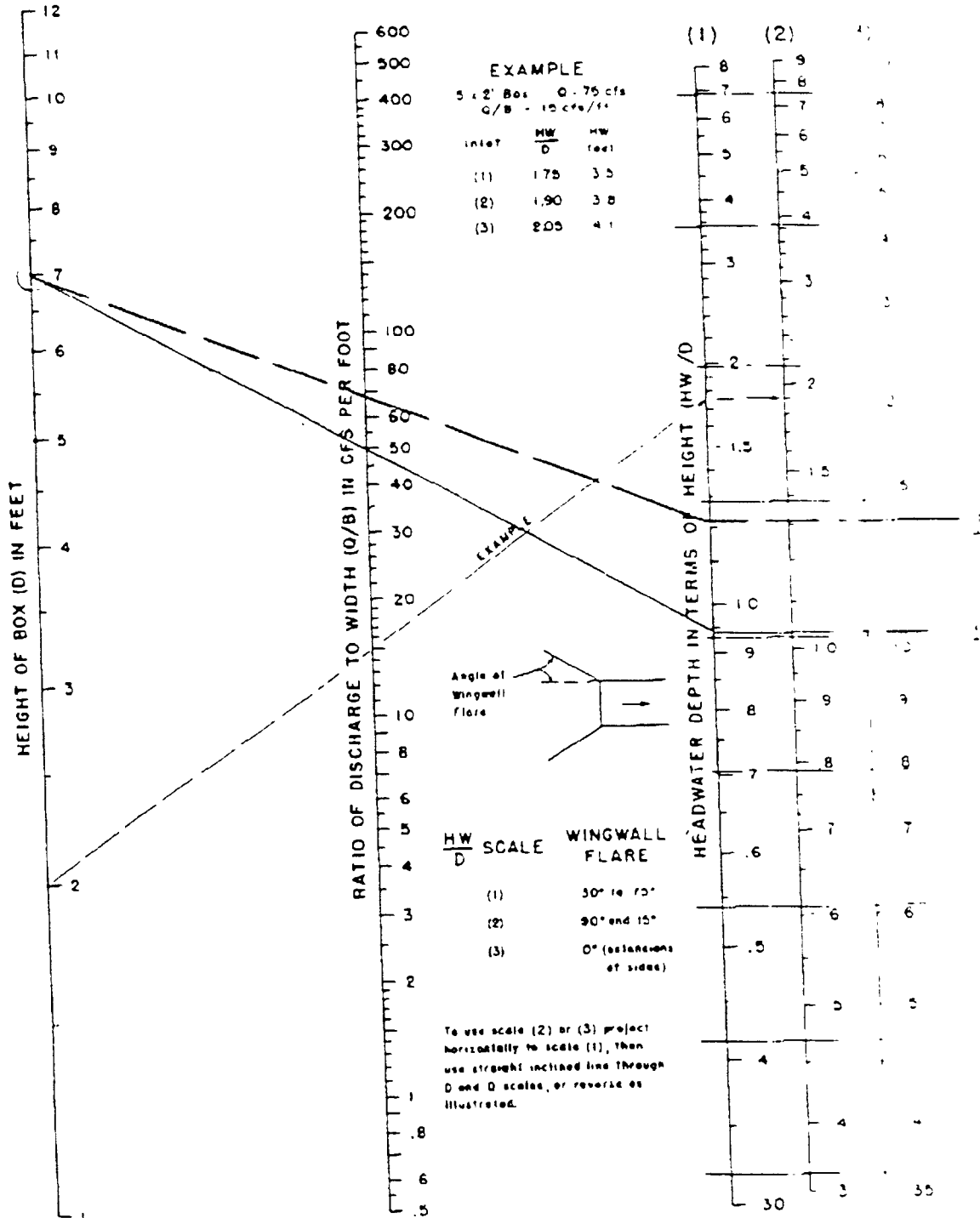


$780.8 \div 2 = 390.4 = 8 \cdot 48.8$

$(1085 \div 2 = 542.5 = \dots)$

**CHART 8**

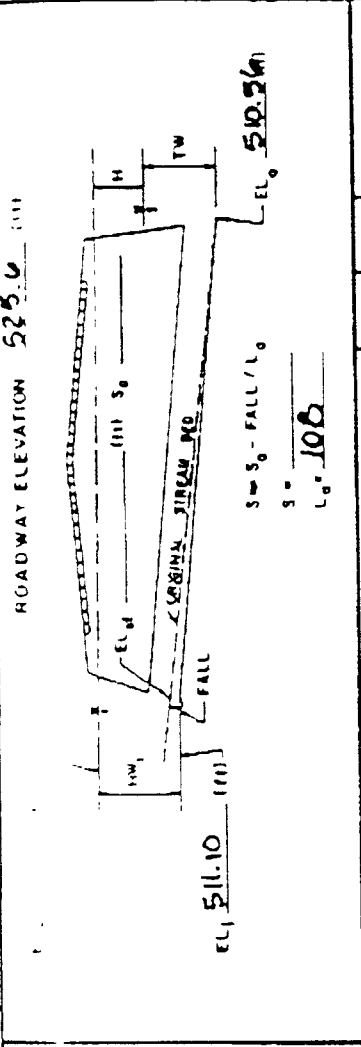
3. 7'h x 8'w



**HEADWATER DEPTH FOR BOX CULVERTS WITH INLET CONTROL**

BUREAU OF PUBLIC ROADS JAN 1963

PROJECT Winghaven David Lr STATION 5+30 CULVERT DESIGN FORM  
 DESIGNER/DATE 185 / 12/23/97  
 REVIEWER/DATE \_\_\_\_\_ / \_\_\_\_\_



HYDROLOGICAL DATA  
 DRAINAGE AREA  STREAM SLOPE  
 CHANNEL SHAPE  OTHER  
 ROUTING  OTHER

DESIGN FLOWS/TAILWATER  
 R 1 (YEARS) 15 FLOW (CFS) 17808 TW (ft) \_\_\_\_\_  
100 1085

CULVERT DESCRIPTION: MATERIAL - SHAPE - SIZE - ENTRANCE	TOTAL FLOW Q (cfs)	FLOW PER BARREL Q/N (1)	INLET CONTROL			OUTLET CONTROL			COMMENTS		
			HW/D (2)	TW (5)	FALL (3)	EL <sub>i</sub> (4)	Q <sub>c</sub> (6)	H <sub>o</sub> (8)		EL <sub>o</sub> (10)	
2 - 7' h x 8' w (154)	1808	204	12	8.4	-	519.2	4.2	5.6	1.32	517.4	inlet control
2 - 7' x 8' (1004)	1085	342	136	9.52	-	520.6	5.2	6.1	2.58	519.24	inlet control

TECHNICAL FOOTNOTES:  
 (1) USE Q/NB FOR BOX CULVERTS  
 (2) HW<sub>i</sub>/D = HW<sub>i</sub>/D OR HW<sub>i</sub>/D FROM DESIGN CHARTS  
 (3) FALL = HW<sub>i</sub> - (EL<sub>in</sub> - EL<sub>o</sub>); FALL IS ZERO FOR CULVERTS ON GRADE  
 (4) EL<sub>in</sub> = HW<sub>i</sub> + EL<sub>i</sub> (INVERT OF INLET CONTROL SECTION)  
 (5) TW BASED ON DOWN STREAM CONTROL OR FLOW DEPTH CHANNEL  
 (6) Q<sub>c</sub> = TW \* (2.0 + D/2) (WHICHEVER IS GREATER)  
 (7) H<sub>o</sub> = [1 + h<sub>o</sub> \* (29 \* L / R<sup>1.33</sup>)] \* V<sup>2</sup> / 2g  
 (8) EL<sub>o</sub> = EL<sub>in</sub> + H<sub>o</sub>

SUBSCRIPT DEFINITIONS:  
 1. APPROXIMATE  
 2. CULVERT FACE  
 3. DESIGN HEADWATER  
 4. HEADWATER IN INLET CONTROL  
 5. HEADWATER IN OUTLET CONTROL  
 6. INLET CONTROL SECTION  
 7. OUTLET CONTROL SECTION  
 8. STREAMBED AT CULVERT FACE  
 9. TAILWATER

COMMENTS / DISCUSSION \_\_\_\_\_

CULVERT BARREL SELECTED:  
 SIZE 7' h x 8' w \* 2  
 SHAPE \_\_\_\_\_  
 MATERIAL: CONC  
 ENTRANCE N/D

260 x 5  
 17A SF 626  
 43A MF 93  
 208.58  
 171.90  
 750.78



# PICKETT RAY & SILVER

CIVIL ENGINEERS

PLANNERS

ADG. LAND SURVEYORS  
MH FILE \_\_\_\_\_

98010



JUN 29 1998

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TO: RON PAGAN @ 434-8280

FROM: DON DANSON

PROJECT: WINGHAVEN

PROJECT NO.: 97-034D

DATE AND TIME: 6-29-98

TOTAL NO. OF PAGES, INCLUDING COVER SHEET: 3

TELECOM OPERATOR:

PLEASE NOTIFY US IMMEDIATELY IF THE MESSAGE IS INCOMPLETE OR UNCLEAR. THANK YOU.

# PICKETT RAY & SILVER

33 Mid Rivers Mall Dr  
Peters, MD 63376

Civil Engineers  
Planners  
Land Surveyors

397 1211

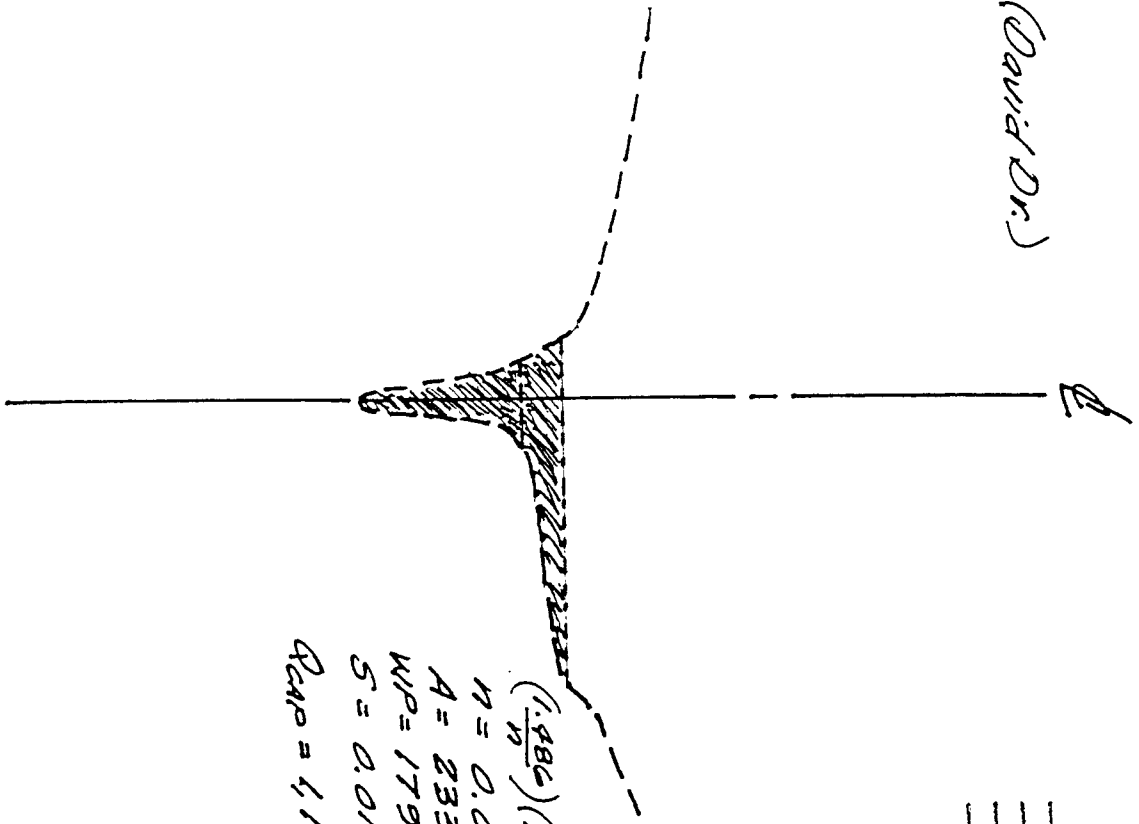
PROJECT NAME \_\_\_\_\_  
PROJECT #/JOB ORDER # \_\_\_\_\_  
DATE \_\_\_\_\_  
DESIGNER \_\_\_\_\_  
PAGE \_\_\_\_\_

SECTION "B-B"

1" = 100' H.  
1" = 5' V.

@ Box Culvert (David Dr.)

520  
515  
510



KDG, MH FILE \_\_\_\_\_

JUN 24 1998


$$\left(\frac{1.486}{n}\right) (A) (MWP)^{2/3} (S)^{1/2} = Q$$

$n = 0.04$   
 $A = 233 \text{ sq. ft.}$   
 $WP = 179 \text{ L.F.}$   
 $S = 0.0131 \text{ ft.}$   
 $Q_{\text{cap}} = 4,176.58 \text{ cfs}$



97-034

TR-55 TABULAR HYDROGRAPH METHOD  
 Type II Distribution  
 (24 hr. Duration Storm)

Executed: 04-28-1998 16:06:28  
 Watershed file: --> DAV-POST.WSD  
 Hydrograph file: --> DAV-POST.HYD

WINGHAVEN - BOX CULVERT @ DAVID DRIVE  
 50 YEAR / 24 HOUR DESIGN STORM

>>>> Input Parameters Used to Compute Hydrograph <<<<

Subarea Description	AREA (acres)	CN	Tc (hrs)	* Tt (hrs)	Precip. (in)	Runoff (in)	Ia/p input/used
GRASS / PAVED	256.01	74.0	0.40	0.00	6.40	3.52	.11 .10

\* Travel time from subarea outfall to composite watershed outfall point.  
 Total area = 256.01 acres or 0.4000 sq.mi  
 Peak discharge = 834 cfs

>>>> Computer Modifications of Input Parameters <<<<

Subarea Description	Input Values		Rounded Values		Ia/p	Ia/p Messages
	Tc (hr)	* Tt (hr)	Tc (hr)	* Tt (hr)	Interpolated (Yes/No)	
GRASS / PAVED	0.35	0.00	0.40	0.00	No	--

\* Travel time from subarea outfall to composite watershed outfall point.

TR-55 TABULAR HYDROGRAPH METHOD  
 Type II Distribution  
 (24 hr. Duration Storm)

Executed: 04-28-1998 16:06:28  
 Watershed file: --> DAV-POST.WSD  
 Hydrograph file: --> DAV-POST.HYD

WINGHAVEN - BOX CULVERT @ DAVID DRIVE  
 50 YEAR / 24 HOUR DESIGN STORM

>>> Summary of Subarea Times to Peak <<<

Subarea	Peak Discharge at Composite Outfall (cfs)	Time to Peak at Composite Outfall (hrs)
----- GRASS / PAVED -----	----- 834 -----	----- 12.3 -----
Composite Watershed	834	12.3

TR-55 TABULAR HYDROGRAPH METHOD  
 Type II Distribution  
 (24 hr. Duration Storm)

Executed: 04-28-1998 16:06:28  
 Watershed file: --> DAV-POST.WSD  
 Hydrograph file: --> DAV-POST.HYD

WINGHAVEN - BOX CULVERT @ DAVID DRIVE  
 50 YEAR / 24 HOUR DESIGN STORM

Composite Hydrograph Summary (cfs)

Subarea Description	11.0 hr	11.3 hr	11.6 hr	11.9 hr	12.0 hr	12.1 hr	12.2 hr	12.3 hr	12.4 hr
GRASS / PAVED	25	35	51	108	199	382	659	834	808
Total (cfs)	25	35	51	108	199	382	659	834	808

Subarea Description	12.5 hr	12.6 hr	12.7 hr	12.8 hr	13.0 hr	13.2 hr	13.4 hr	13.6 hr	13.8 hr
GRASS / PAVED	607	420	304	230	146	108	89	77	69
Total (cfs)	607	420	304	230	146	108	89	77	69

Subarea Description	14.0 hr	14.3 hr	14.6 hr	15.0 hr	15.5 hr	16.0 hr	16.5 hr	17.0 hr	17.5 hr
GRASS / PAVED	62	54	48	44	39	35	31	30	28
Total (cfs)	62	54	48	44	39	35	31	30	28

Subarea Description	18.0 hr	19.0 hr	20.0 hr	22.0 hr	26.0 hr
GRASS / PAVED	25	23	20	17	0
Total (cfs)	25	23	20	17	0

TR-55 TABULAR HYDROGRAPH METHOD  
 Type II Distribution  
 (24 hr. Duration Storm)

Executed: 04-28-1998 16:06:28  
 Watershed file: --> DAV-POST.WSD  
 Hydrograph file: --> DAV-POST.HYD

WINGHAVEN - BOX CULVERT @ DAVID DRIVE  
 50 YEAR / 24 HOUR DESIGN STORM

Time (hrs)	Flow (cfs)	Time (hrs)	Flow (cfs)
11.0	25	14.8	46
11.1	28	14.9	45
11.2	32	15.0	44
11.3	35	15.1	43
11.4	40	15.2	42
11.5	46	15.3	41
11.6	51	15.4	40
11.7	70	15.5	39
11.8	89	15.6	38
11.9	108	15.7	37
12.0	199	15.8	37
12.1	382	15.9	36
12.2	659	16.0	35
12.3	834	16.1	34
12.4	808	16.2	33
12.5	607	16.3	33
12.6	420	16.4	32
12.7	304	16.5	31
12.8	230	16.6	31
12.9	188	16.7	31
13.0	146	16.8	30
13.1	127	16.9	30
13.2	108	17.0	30
13.3	98	17.1	30
13.4	89	17.2	29
13.5	83	17.3	29
13.6	77	17.4	28
13.7	73	17.5	28
13.8	69	17.6	27
13.9	66	17.7	27
14.0	62	17.8	26
14.1	59	17.9	26
14.2	57	18.0	25
14.3	54	18.1	25
14.4	52	18.2	25
14.5	50	18.3	24
14.6	48	18.4	24
14.7	47	18.5	24

TR-55 TABULAR HYDROGRAPH METHOD  
 Type II Distribution  
 (24 hr. Duration Storm)

Executed: 04-28-1998 16:06:28  
 Watershed file: --> DAV-POST.WSD  
 Hydrograph file: --> DAV-POST.HYD

WINGHAVEN - BOX CULVERT @ DAVID DRIVE  
 50 YEAR / 24 HOUR DESIGN STORM

Time (hrs)	Flow (cfs)	Time (hrs)	Flow (cfs)
18.6	24	22.4	15
18.7	24	22.5	15
18.8	23	22.6	14
18.9	23	22.7	14
19.0	23	22.8	14
19.1	23	22.9	13
19.2	22	23.0	13
19.3	22	23.1	12
19.4	22	23.2	12
19.5	22	23.3	11
19.6	21	23.4	11
19.7	21	23.5	11
19.8	21	23.6	10
19.9	20	23.7	10
20.0	20	23.8	9
20.1	20	23.9	9
20.2	20	24.0	8
20.3	20	24.1	8
20.4	19	24.2	8
20.5	19	24.3	7
20.6	19	24.4	7
20.7	19	24.5	6
20.8	19	24.6	6
20.9	19	24.7	6
21.0	18	24.8	5
21.1	18	24.9	5
21.2	18	25.0	4
21.3	18	25.1	4
21.4	18	25.2	3
21.5	18	25.3	3
21.6	18	25.4	3
21.7	17	25.5	2
21.8	17	25.6	2
21.9	17	25.7	1
22.0	17	25.8	1
22.1	17	25.9	0
22.2	16		
22.3	16		

WINGHAVEN - BOX CULVERT @ DAVID DRIVE  
 50 YEAR / 24 HOUR DESIGN STORM

Tc COMPUTATIONS FOR:

SHEET FLOW (Applicable to Tc only)

Segment ID		1	
Surface description		GRASS	
Manning's roughness coeff., n		0.0240	
Flow length, L (total < or = 300)	ft	150.0	
Two-yr 24-hr rainfall, P2	in	3.500	
Land slope, s	ft/ft	0.0300	
		0.8	
$T = \frac{.007 * (n * L)}{0.5 * P2 + 0.4 * s}$		hrs	0.04 = 0.04

SHALLOW CONCENTRATED FLOW

Segment ID		2	
Surface (paved or unpaved)?		Unpaved	
Flow length, L	ft	100.0	
Watercourse slope, s	ft/ft	0.0700	
		0.5	
Avg.V = Csf * (s)	ft/s	4.2688	
where: Unpaved Csf = 16.1345			
Paved Csf = 20.3282			
T = L / (3600*V)	hrs	0.01	= 0.01

CHANNEL FLOW

Segment ID		3	4
Cross Sectional Flow Area, a	sq.ft	9.62	233.00
Wetted perimeter, Pw	ft	11.00	179.00
Hydraulic radius, r = a/Pw	ft	0.875	1.302
Channel slope, s	ft/ft	0.0230	0.0130
Manning's roughness coeff., n		0.0130	0.0400
		2/3	1/2
$V = \frac{1.49 * r^{2/3} * s^{1/2}}{n}$		ft/s	%15.8974 5.0633
Flow length, L	ft	1300	5070
T = L / (3600*V)	hrs	0.02	+ 0.28 = 0.30

.....  
 TOTAL TIME (hrs) 0.35



SUMMARY SHEET FOR Tc or Tt COMPUTATIONS  
(Solved for Time using TR-55 Methods)

WINGHAVEN - BOX CULVERT @ DAVID DRIVE  
50 YEAR / 24 HOUR DESIGN STORM

Subarea descr.	Tc or Tt	Time (hrs)
-----	-----	-----
	Tc	0.35

WINGHAVEN - BOX CULVERT @ DAVID DRIVE  
50 YEAR / 24 HOUR DESIGN STORM

RUNOFF CURVE NUMBER SUMMARY

.....

<u>Subarea Description</u>	<u>Area (acres)</u>	<u>CN (weighted)</u>
	256.01	74

WINGHAVEN - BOX CULVERT @ DAVID DRIVE  
50 YEAR / 24 HOUR DESIGN STORM

RUNOFF CURVE NUMBER DATA

.....

Composite Area:

SURFACE DESCRIPTION	AREA (acres)	CN
GRASS (GOLF COURSE)	54.44	61
PAVED (SINGLE FAMILY RES.)	159.31	75
PAVED (MULTI-FAMILY RES.)	35.41	85
PAVED (COMMERCIAL)	6.85	98
COMPOSITE AREA --->	256.01	74.0 ( 74 )

.....

>>>> GRAPHICAL PEAK DISCHARGE METHOD <<<<<

WINGHAVEN - BOX CULVERT @ DAVID DRIVE  
50 YEAR / 24 HOUR DESIGN STORM

CALCULATED  
DISK FILE: DAV-POST.GPD

Drainage Area	(acres)	256.01---	0.4000 sq.mi.
Runoff Curve Number	(CN)	74	
Time of Concentration, Tc	(hrs)	0.35	
Rainfall Distribution	(Type)	II	
Pond and Swamp Areas	(%)	---	0.0 acres

	Storm #1	Storm #2	Storm #3
	-----	-----	-----
Frequency (years)	50		
Rainfall, P, 24-hr (in)	6.4		
Initial Abstraction, Ia (in)	0.703	0.703	0.703
Ia/p Ratio	0.110	0.000	0.000
Unit Discharge, * qu (csm/in)	625	0	0
Runoff, Q (in)	3.52	0.00	0.00
Pond & Swamp Adjustment Factor	1.00	1.00	1.00
PEAK DISCHARGE, qp (cfs)	892	0	0

Summary of Computations for qu

Ia/p	#1	0.100	0.000	0.000
C0	#1	2.553	0.000	0.000
C1	#1	-0.615	0.000	0.000
C2	#1	-0.164	0.000	0.000
qu (csm)	#1	630.355	0.000	0.000
Ia/p	#2	0.300	0.000	0.000
C0	#2	2.465	0.000	0.000
C1	#2	-0.623	0.000	0.000
C2	#2	-0.117	0.000	0.000
qu (csm)	#2	530.808	0.000	0.000
* qu (csm)		625	0	0

\* Interpolated for computed Ia/p ratio (between Ia/p #1 & Ia/p #2)  
If computed Ia/p exceeds Ia/p limits, bounding limit for Ia/p is used.

$$\log(qu) = C0 + ( C1 * \log(Tc) ) + ( C2 * (\log(Tc))^2 )$$

$$QP (cfs) = qu(csm) * Area(sq.mi.) * Q(in.) * (Pond \& Swamp Adj.)$$

WINGHAVEN - BOX CULVERT @ DAVID DRIVE  
 100YEAR / 24 HOUR DESIGN STORM

CALCULATED  
 DISK FILE: DAV-POST.GPD

Drainage Area (acres) 256.01---> 0.4000 sq.mi.  
 Runoff Curve Number (CN) 74  
 Time of Concentration, Tc (hrs) 0.35  
 Rainfall Distribution (Type) II  
 Pond and Swamp Areas (%) ---> 0.0 acres

	Storm #1	Storm #2	Storm #3
	-----	-----	-----
Frequency (years)	100		
Rainfall, P, 24-hr (in)	7.2		
Initial Abstraction, Ia (in)	0.703	0.703	0.703
Ia/p Ratio	0.098	0.000	0.000
Unit Discharge, * qu (csm/in)	630	0	0
Runoff, Q (in)	4.22	0.00	0.00
Pond & Swamp Adjustment Factor	1.00	1.00	1.00
PEAK DISCHARGE, qp (cfs)	1063	0	0

Summary of Computations for qu

		Storm #1	Storm #2	Storm #3
Ia/p	#1	0.100	0.000	0.000
C0	#1	2.553	0.000	0.000
C1	#1	-0.615	0.000	0.000
C2	#1	-0.164	0.000	0.000
qu (csm)	#1	630.355	0.000	0.000
Ia/p	#2	0.100	0.000	0.000
C0	#2	2.553	0.000	0.000
C1	#2	-0.615	0.000	0.000
C2	#2	-0.164	0.000	0.000
qu (csm)	#2	630.355	0.000	0.000
* qu (csm)		630	0	0

\* Interpolated for computed Ia/p ratio (between Ia/p #1 & Ia/p #2)  
 If computed Ia/p exceeds Ia/p limits, bounding limit for Ia/p is used.

$$\log(qu) = C0 + (C1 * \log(Tc)) + (C2 * (\log(Tc))^2)$$

$$qp (cfs) = qu(csm) * Area(sq.mi.) * Q(in.) * (Pond \& Swamp Adj.)$$

**PICKETT RAY & SILVER**

333 Mid Rivers Mall Dr  
St. Peters, MD 63376

Civil Engineers  
Planners  
Land Surveyors

397-1211

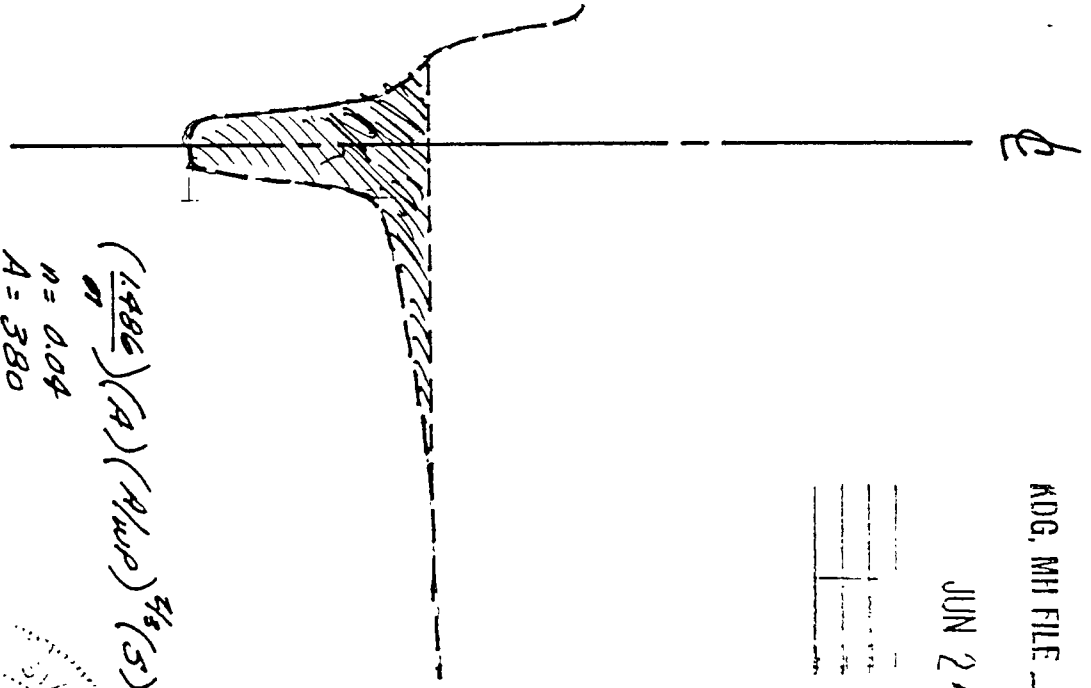
PROJECT NAME \_\_\_\_\_  
PROJECT #/JOB ORDER # \_\_\_\_\_  
DATE \_\_\_\_\_  
DESIGNER \_\_\_\_\_  
PAGE \_\_\_\_\_

SECTION "C-C"

1" = 100' H.  
1" = 5' V.

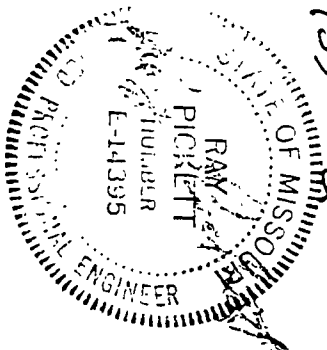
@ Box Culvert (Charlita Dr.)

500  
495  
490



$$\frac{(1.486)}{n} (A) (A/wP)^{4/3} (S)^{1/2} = Q$$

$n = 0.04$   
 $A = 380$   
 $WP = 240$   
 $S = 0.0056/ft.$   
 $Q_{cap} = 1935 cfs$



KDG, MH FILE 980100

JUN 24 1998


97-034

TR-55 TABULAR HYDROGRAPH METHOD  
 Type II Distribution  
 (24 hr. Duration Storm)

Executed: 04-29-1998 13:29:57  
 Watershed file: --> CHL-POST.WSD  
 Hydrograph file: --> CHL-POST.HYD

WINGHAVEN - BOX CULVERT @ CHARLIE DRIVE  
 100YEAR / 24 HOUR DESIGN STORM

>>>> Input Parameters Used to Compute Hydrograph <<<<

Subarea Description	AREA (acres)	CN	Tc (hrs)	* Tt (hrs)	Precip. (in)	Runoff (in)	Ia/p input/used
GRASS / PAVED	1557.10	83.0	0.75	0.00	7.20	5.22	.06 .10

\* Travel time from subarea outfall to composite watershed outfall point.  
 Total area = 1557.10 acres or 2.4330 sq.mi  
 Peak discharge = 5385 cfs

>>>> Computer Modifications of Input Parameters <<<<

Subarea Description	Input Values		Rounded Values		Ia/p	Ia/p Messages
	Tc (hr)	* Tt (hr)	Tc (hr)	* Tt (hr)	Interpolated (Yes/No)	
GRASS / PAVED	0.74	0.00	0.75	0.00	No	Computed Ia/p < .1

\* Travel time from subarea outfall to composite watershed outfall point.

TR-55 TABULAR HYDROGRAPH METHOD  
 Type II Distribution  
 (24 hr. Duration Storm)

Executed: 04-29-1998 13:29:57  
 Watershed file: --> CHL-POST.WSD  
 Hydrograph file: --> CHL-POST.HYD

WINGHAVEN - BOX CULVERT @ CHARLIE DRIVE  
 100YEAR / 24 HOUR DESIGN STORM

>>> Summary of Subarea Times to Peak <<<<

Subarea	Peak Discharge at Composite Outfall (cfs)	Time to Peak at Composite Outfall (hrs)
----- GRASS / PAVED -----	----- 5385 -----	----- 12.6 -----
Composite Watershed	5385	12.6



TR-55 TABULAR HYDROGRAPH METHOD  
 Type II Distribution  
 (24 hr. Duration Storm)

Executed: 04-29-1998 13:29:57  
 Watershed file: --> CHL-POST.WSD  
 Hydrograph file: --> CHL-POST.HYD

WINGHAVEN - BOX CULVERT @ CHARLIE DRIVE  
 100YEAR / 24 HOUR DESIGN STORM

Composite Hydrograph Summary (cfs)

Subarea Description	11.0 hr	11.3 hr	11.6 hr	11.9 hr	12.0 hr	12.1 hr	12.2 hr	12.3 hr	12.4 hr
GRASS / PAVED	165	229	305	457	584	864	1461	2464	3734
Total (cfs)	165	229	305	457	584	864	1461	2464	3734

Subarea Description	12.5 hr	12.6 hr	12.7 hr	12.8 hr	13.0 hr	13.2 hr	13.4 hr	13.6 hr	13.8 hr
GRASS / PAVED	4826	5385	5207	4686	3200	2184	1562	1181	940
Total (cfs)	4826	5385	5207	4686	3200	2184	1562	1181	940

Subarea Description	14.0 hr	14.3 hr	14.6 hr	15.0 hr	15.5 hr	16.0 hr	16.5 hr	17.0 hr	17.5 hr
GRASS / PAVED	775	622	521	445	394	343	305	279	254
Total (cfs)	775	622	521	445	394	343	305	279	254

Subarea Description	18.0 hr	19.0 hr	20.0 hr	22.0 hr	26.0 hr
GRASS / PAVED	241	216	191	152	0
Total (cfs)	241	216	191	152	0

TR-55 TABULAR HYDROGRAPH METHOD  
 Type II Distribution  
 (24 hr. Duration Storm)

Executed: 04-29-1998 13:29:57  
 Watershed file: --> CHL-POST.WSD  
 Hydrograph file: --> CHL-POST.HYD

WINGHAVEN - BOX CULVERT @ CHARLIE DRIVE  
 100YEAR / 24 HOUR DESIGN STORM

Time (hrs)	Flow (cfs)	Time (hrs)	Flow (cfs)
11.0	165	14.8	483
11.1	186	14.9	464
11.2	208	15.0	445
11.3	229	15.1	435
11.4	254	15.2	425
11.5	280	15.3	414
11.6	305	15.4	404
11.7	356	15.5	394
11.8	406	15.6	384
11.9	457	15.7	374
12.0	584	15.8	363
12.1	864	15.9	353
12.2	1461	16.0	343
12.3	2464	16.1	335
12.4	3734	16.2	328
12.5	4826	16.3	320
12.6	5385	16.4	313
12.7	5207	16.5	305
12.8	4686	16.6	300
12.9	3943	16.7	295
13.0	3200	16.8	289
13.1	2692	16.9	284
13.2	2184	17.0	279
13.3	1873	17.1	274
13.4	1562	17.2	269
13.5	1372	17.3	264
13.6	1181	17.4	259
13.7	1060	17.5	254
13.8	940	17.6	251
13.9	857	17.7	249
14.0	775	17.8	246
14.1	724	17.9	244
14.2	673	18.0	241
14.3	622	18.1	238
14.4	588	18.2	236
14.5	555	18.3	234
14.6	521	18.4	231
14.7	502	18.5	228

TR-55 TABULAR HYDROGRAPH METHOD  
 Type II Distribution  
 (24 hr. Duration Storm)

Executed: 04-29-1998 13:29:57  
 Watershed file: --> CHL-POST.WSD  
 Hydrograph file: --> CHL-POST.HYD

WINGHAVEN - BOX CULVERT @ CHARLIE DRIVE  
 100YEAR / 24 HOUR DESIGN STORM

Time (hrs)	Flow (cfs)	Time (hrs)	Flow (cfs)
18.6	226	22.4	137
18.7	224	22.5	133
18.8	221	22.6	129
18.9	218	22.7	125
19.0	216	22.8	122
19.1	214	22.9	118
19.2	211	23.0	114
19.3	208	23.1	110
19.4	206	23.2	106
19.5	204	23.3	103
19.6	201	23.4	99
19.7	198	23.5	95
19.8	196	23.6	91
19.9	194	23.7	87
20.0	191	23.8	84
20.1	189	23.9	80
20.2	187	24.0	76
20.3	185	24.1	72
20.4	183	24.2	68
20.5	181	24.3	65
20.6	179	24.4	61
20.7	177	24.5	57
20.8	175	24.6	53
20.9	173	24.7	49
21.0	172	24.8	46
21.1	170	24.9	42
21.2	168	25.0	38
21.3	166	25.1	34
21.4	164	25.2	30
21.5	162	25.3	27
21.6	160	25.4	23
21.7	158	25.5	19
21.8	156	25.6	15
21.9	154	25.7	11
22.0	152	25.8	8
22.1	148	25.9	4
22.2	144		
22.3	141		

WINGHAVEN - BOX CULVERT @ CHARLIE DRIVE  
 100YEAR / 24 HOUR DESIGN STORM

Tc COMPUTATIONS FOR:

SHEET FLOW (Applicable to Tc only)

Segment ID		1
Surface description	GRASS	
Manning's roughness coeff., n		0.0240
Flow length, L (total < or = 300)	ft	100.0
Two-yr 24-hr rainfall, P2	in	3.500
Land slope, s	ft/ft	0.0400

$$T = \frac{0.007 * (n * L)^{0.8}}{0.5 * P2^{0.4} * s} \text{ hrs} = 0.03$$

SHALLOW CONCENTRATED FLOW

Segment ID		2
Surface (paved or unpaved)?	Unpaved	
Flow length, L	ft	500.0
Watercourse slope, s	ft/ft	0.0180

$$\text{Avg. V} = \text{Csf} * (s)^{0.5} \text{ ft/s} = 2.1647$$

where: Unpaved Csf = 16.1345  
 Paved Csf = 20.3282

$$T = L / (3600 * V) \text{ hrs} = 0.06$$

CHANNEL FLOW

Segment ID		3	4
Cross Sectional Flow Area, a	sq.ft	1760.00	380.00
Wetted perimeter, Pw	ft	242.00	240.00
Hydraulic radius, r = a/Pw	ft	7.273	1.583
Channel slope, s	ft/ft	0.0094	0.0056
Manning's roughness coeff., n		0.0400	0.0400

$$V = \frac{1.49 * r^{2/3} * s^{1/2}}{n} \text{ ft/s} = 13.5567 \quad 3.7868$$

Flow length, L	ft	14400	4780
----------------	----	-------	------

$$T = L / (3600 * V) \text{ hrs} = 0.30 + 0.35 = 0.65$$

.....  
 TOTAL TIME (hrs) = 0.74

SUMMARY SHEET FOR Tc or Tt COMPUTATIONS  
(Solved for Time using TR-55 Methods)

WINGHAVEN - BOX CULVERT @ CHARLIE DRIVE  
100YEAR / 24 HOUR DESIGN STORM

Subarea descr.	Tc or Tt	Time (hrs)
-----	-----	-----
	Tc	0.74

WINGHAVEN - BOX CULVEPT @ CHARLIE DRIVE  
100YEAR / 24 HOUR DESIGN STORM

RUNOFF CURVE NUMBER SUMMARY

.....

<u>Subarea Description</u>	<u>Area (acres)</u>	<u>CN (weighted)</u>
	1557.08	83

WINGHAVEN - BOX CULVERT @ CHARLIE DRIVE  
100YEAR / 24 HOUR DESIGN STORM

RUNOFF CURVE NUMBER DATA

.....

Composite Area:

SURFACE DESCRIPTION	AREA (acres)	CN
GRASS (GOLF COURSE)	164.74	61
PAVED (SINGLE FAMILY RES.)	707.40	75
PAVED (MULTI-FAMILY RES.)	62.57	85
PAVED (COMMERCIAL)	622.37	98
COMPOSITE AREA --->	1557.08	83.1 ( 83 )

.....

>>>> GRAPHICAL PEAK DISCHARGE METHOD <<<<<

WINGHAVEN - BOX CULVERT @ CHARLIE DRIVE  
 100 YEAR / 24 HOUR DESIGN STORM

CALCULATED  
 DISK FILE: CHL-POST.GPD

Drainage Area (acres) 1557.1---> 2.4330 sq.mi.  
 Runoff Curve Number (CN) 83  
 Time of Concentration, Tc (hrs) .74  
 Rainfall Distribution (Type) II  
 Pond and Swamp Areas (%) ---> 0.0 acres

	Storm #1	Storm #2	Storm #3
Frequency (years)	100		
Rainfall, P, 24-hr (in)	7.2		
Initial Abstraction, Ia (in)	0.410	0.410	0.410
Ia/p Ratio	0.057	0.000	0.000
Unit Discharge, * qu (csm/in)	427	0	0
Runoff, Q (in)	5.22	0.00	0.00
Pond & Swamp Adjustment Factor	1.00	1.00	1.00
PEAK DISCHARGE, qp (cfs)	5425	0	0

Summary of Computations for qu

Ia/p #1	0.100	0.000	0.000
C0 #1	2.553	0.000	0.000
C1 #1	-0.615	0.000	0.000
C2 #1	-0.164	0.000	0.000
qu (csm) #1	427.428	0.000	0.000
Ia/p #2	0.100	0.000	0.000
C0 #2	2.553	0.000	0.000
C1 #2	-0.615	0.000	0.000
C2 #2	-0.164	0.000	0.000
qu (csm) #2	427.428	0.000	0.000
* qu (csm)	427	0	0

\* Interpolated for computed Ia/p ratio (between Ia/p #1 & Ia/p #2)  
 If computed Ia/p exceeds Ia/p limits, bounding limit for Ia/p is used.

$$\log(qu) = C0 + (C1 * \log(Tc)) + (C2 * (\log(Tc))^2)$$

$$QP (cfs) = qu(csm) * Area(sq.mi.) * Q(in.) * (Pond \& Swamp Adj.)$$



# PICKETT RAY & SILVER

33 Mid Rivers Mall Dr  
 Peters, MO 63376

Civil Engineers  
 Planners  
 Land Surveyors

397-1211

PROJECT NAME \_\_\_\_\_

PROJECT #/JOB ORDER # \_\_\_\_\_

DATE \_\_\_\_\_

DESIGNER \_\_\_\_\_

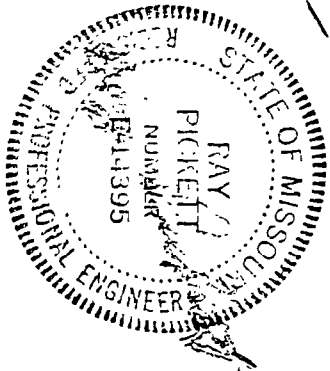
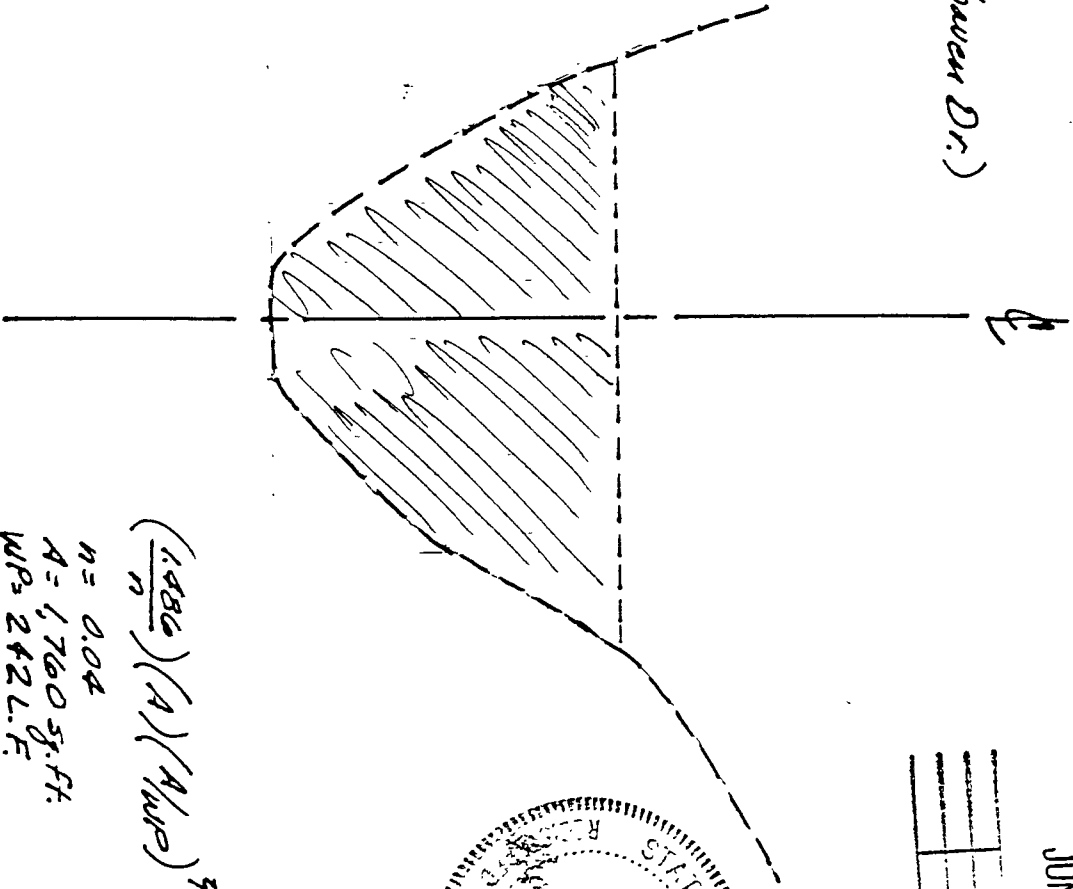
PAGE \_\_\_\_\_

SECTION "A-A":

1" = 100' H.  
 1" = 5' V.

@ Box Culvert (Wingbauer Dr.)

530  
525  
520  
515



K08, MH FILE \_\_\_\_\_

JUN 24 1998


$$\left(\frac{1.486}{n}\right)(A)(A/WP)^{4/3}(S)^{1/2} = Q$$

$n = 0.04$   
 $A = 4,760 \text{ sq. ft.}$   
 $WP = 242 \text{ L.F.}$   
 $S = 0.0094 \text{ ft/ft}$   
 $Q_{cap} = 23,796 \text{ cfs}$

71-034

TR-55 TABULAR HYDROGRAPH METHOD  
 Type II Distribution  
 (24 hr. Duration Storm)

Executed: 04-29-1998 13:21:43  
 Watershed file: --> WH-POST .WSD  
 Hydrograph file: --> WH-POST .HYD

WINGHAVEN - BOX CULVERT @ WINGHAVEN DRIVE  
 100YEAR / 24 HOUR DESIGN STORM

>>>> Input Parameters Used to Compute Hydrograph <<<<

Subarea Description	AREA (acres)	CN	Tc (hrs)	* Tt (hrs)	Precip. (in)	Runoff (in)	Ia/p input/used
GRASS / PAVED	1220.70	80.0	0.40	0.00	7.20	4.88	.07 .10

\* Travel time from subarea outfall to composite watershed outfall point.  
 Total area = 1220.70 acres or 1.9073 sq.mi .  
 Peak discharge = 5510 cfs

>>>> Computer Modifications of Input Parameters <<<<

Subarea Description	Input Values		Rounded Values		Ia/p	Ia/p Messages
	Tc (hr)	* Tt (hr)	Tc (hr)	* Tt (hr)	Interpolated (Yes/No)	
GRASS / PAVED	0.39	0.00	0.40	0.00	No	Computed Ia/p < .1

\* Travel time from subarea outfall to composite watershed outfall point.

## TR-55 TABULAR HYDROGRAPH METHOD

Type II Distribution  
(24 hr. Duration Storm)

Executed: 04-29-1998 13:21:43  
Watershed file: --> WH-POST .WSD  
Hydrograph file: --> WH-POST .HYD

WINGHAVEN - BOX CULVERT @ WINGHAVEN DRIVE  
100YEAR / 24 HOUR DESIGN STORM

>>> Summary of Subarea Times to Peak <<<<

Subarea	Peak Discharge at Composite Outfall (cfs)	Time to Peak at Composite Outfall (hrs)
GRASS / PAVED	5510	12.3
Composite Watershed	5510	12.3

:

TR-55 TABULAR HYDROGRAPH METHOD  
 Type II Distribution  
 (24 hr. Duration Storm)

Executed: 04-29-1998 13:21:43  
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 Hydrograph file: --> WH-POST .HYD

WINGHAVEN - BOX CULVERT @ WINGHAVEN DRIVE  
 100YEAR / 24 HOUR DESIGN STORM

Composite Hydrograph Summary (cfs)

Subarea Description	11.0 hr	11.3 hr	11.6 hr	11.9 hr	12.0 hr	12.1 hr	12.2 hr	12.3 hr	12.4 hr
GRASS / PAVED	168	233	335	717	1312	2522	4356	5510	5343
Total (cfs)	168	233	335	717	1312	2522	4356	5510	5343

Subarea Description	12.5 hr	12.6 hr	12.7 hr	12.8 hr	13.0 hr	13.2 hr	13.4 hr	13.6 hr	13.8 hr
GRASS / PAVED	4012	2774	2010	1517	968	717	586	512	456
Total (cfs)	4012	2774	2010	1517	968	717	586	512	456

Subarea Description	14.0 hr	14.3 hr	14.6 hr	15.0 hr	15.5 hr	16.0 hr	16.5 hr	17.0 hr	17.5 hr
GRASS / PAVED	410	354	316	289	261	233	205	195	186
Total (cfs)	410	354	316	289	261	233	205	195	186

Subarea Description	18.0 hr	19.0 hr	20.0 hr	22.0 hr	26.0 hr
GRASS / PAVED	168	149	130	112	0
Total (cfs)	168	149	130	112	0

TR-55 TABULAR HYDROGRAPH METHOD  
 Type II Distribution  
 (24 hr. Duration Storm)

Executed: 04-29-1998 13:21:43  
 Watershed file: --> WH-POST .WSD  
 Hydrograph file: --> WH-POST .HYD

WINGHAVEN - BOX CULVERT @ WINGHAVEN DRIVE  
 100YEAR / 24 HOUR DESIGN STORM

Time (hrs)	Flow (cfs)	Time (hrs)	Flow (cfs)
11.0	168	14.8	302
11.1	190	14.9	296
11.2	211	15.0	289
11.3	233	15.1	283
11.4	267	15.2	278
11.5	301	15.3	272
11.6	335	15.4	267
11.7	462	15.5	261
11.8	590	15.6	255
11.9	717	15.7	250
12.0	1312	15.8	244
12.1	2522	15.9	239
12.2	4356	16.0	233
12.3	5510	16.1	227
12.4	5343	16.2	222
12.5	4012	16.3	216
12.6	2774	16.4	211
12.7	2010	16.5	205
12.8	1517	16.6	203
12.9	1242	16.7	201
13.0	968	16.8	199
13.1	842	16.9	197
13.2	717	17.0	195
13.3	651	17.1	193
13.4	586	17.2	191
13.5	549	17.3	190
13.6	512	17.4	188
13.7	484	17.5	186
13.8	456	17.6	182
13.9	433	17.7	179
14.0	410	17.8	175
14.1	391	17.9	172
14.2	373	18.0	168
14.3	354	18.1	166
14.4	341	18.2	164
14.5	329	18.3	162
14.6	316	18.4	160
14.7	309	18.5	158

TR-55 TABULAR HYDROGRAPH METHOD  
 Type II Distribution  
 (24 hr. Duration Storm)

Executed: 04-29-1998 13:21:43  
 Watershed file: --> WH-POST .WSD  
 Hydrograph file: --> WH-POST .HYD

WINGHAVEN - BOX CULVERT @ WINGHAVEN DRIVE  
 100YEAR / 24 HOUR DESIGN STORM

Time (hrs)	Flow (cfs)	Time (hrs)	Flow (cfs)
18.6	157	22.4	101
18.7	155	22.5	98
18.8	153	22.6	95
18.9	151	22.7	92
19.0	149	22.8	90
19.1	147	22.9	87
19.2	145	23.0	84
19.3	143	23.1	81
19.4	141	23.2	78
19.5	140	23.3	76
19.6	138	23.4	73
19.7	136	23.5	70
19.8	134	23.6	67
19.9	132	23.7	64
20.0	130	23.8	62
20.1	129	23.9	59
20.2	128	24.0	56
20.3	127	24.1	53
20.4	126	24.2	50
20.5	126	24.3	48
20.6	125	24.4	45
20.7	124	24.5	42
20.8	123	24.6	39
20.9	122	24.7	36
21.0	121	24.8	34
21.1	120	24.9	31
21.2	119	25.0	28
21.3	118	25.1	25
21.4	117	25.2	22
21.5	116	25.3	20
21.6	116	25.4	17
21.7	115	25.5	14
21.8	114	25.6	11
21.9	113	25.7	8
22.0	112	25.8	6
22.1	109	25.9	3
22.2	106		
22.3	104		

WINGHAVEN - BOX CULVERT @ WINGHAVEN DRIVE  
 100YEAR / 24 HOUR DESIGN STORM

Tc COMPUTATIONS FOR:

SHEET FLOW (Applicable to Tc only)

Segment ID		1
Surface description		GRASS
Manning's roughness coeff., n		0.0240
Flow length, L (total < or = 300)	ft	100.0
Two-yr 24-hr rainfall, P2	in	3.500
Land slope, s	ft/ft	0.0400

$$T = \frac{.007 * (n * L)^{0.8}}{0.5 * P2^{0.4} * s} \quad \text{hrs} \quad 0.03 \quad = \quad 0.03$$

SHALLOW CONCENTRATED FLOW

Segment ID		2
Surface (paved or unpaved)?		Unpaved
Flow length, L	ft	500.0
Watercourse slope, s	ft/ft	0.0180

$$\text{Avg. } V = Csf * (s)^{0.5} \quad \text{ft/s} \quad 2.1647$$

where: Unpaved Csf = 16.1345  
 Paved Csf = 20.3282

$$T = L / (3600 * V) \quad \text{hrs} \quad 0.06 \quad = \quad 0.06$$

CHANNEL FLOW

Segment ID		3
Cross Sectional Flow Area, a	sq.ft	1760.00
Wetted perimeter, Pw	ft	242.00
Hydraulic radius, r = a/Pw	ft	7.273
Channel slope, s	ft/ft	0.0094
Manning's roughness coeff., n		0.0400

$$V = \frac{1.49 * r^{2/3} * s^{1/2}}{n} \quad \text{ft/s} \quad 13.5567$$

Flow length, L ft 14400

$$T = L / (3600 * V) \quad \text{hrs} \quad 0.30 \quad = \quad 0.30$$

.....  
 TOTAL TIME (hrs) 0.39

SUMMARY SHEET FOR Tc or Tt COMPUTATIONS  
(Solved for Time using TR-55 Methods)

WINGHAVEN - BOX CULVERT @ WINGHAVEN DRIVE  
100YEAR / 24 HOUR DESIGN STORM

<u>Subarea descr.</u>	<u>Tc or Tt</u>	<u>Time (hrs)</u>
	Tc	0.39



WINGHAVEN - BOX CULVERT @ WINGHAVEN DRIVE  
100YEAR / 24 HOUR DESIGN STORM

RUNOFF CURVE NUMBER SUMMARY

.....

Subarea Description	Area (acres)	CN (weighted)
-----	-----	-----
	1220.97	80

WINGHAVEN - BOX CULVERT @ WINGHAVEN DRIVE  
100YEAR / 24 HOUR DESIGN STORM

RUNOFF CURVE NUMBER DATA

.....

Composite Area:

SURFACE DESCRIPTION	AREA (acres)	CN
GRASS (GOLF COURSE)	164.74	61
PAVED (SINGLE FAMILY RES.)	647.42	75
PAVED (MULTI-FAMILY RES.)	47.08	85
PAVED (COMMERCIAL)	361.73	98
COMPOSITE AREA --->	1220.97	80.3 ( 80 )

.....

>>>> GRAPHICAL PEAK DISCHARGE METHOD <<<<<

WINGHAVEN - BOX CULVERT @ WINGHAVEN DRIVE  
100YEAR / 24 HOUR DESIGN STORM

CALCULATED  
DISK FILE: WH-POST .GPD

Drainage Area (acres) 1220.9---> 1.9077 sq.mi.  
Runoff Curve Number (CN) 80  
Time of Concentration, Tc (hrs) .39  
Rainfall Distribution (Type) II  
Pond and Swamp Areas (%) ---> 0.0 acres

	Storm #1	Storm #2	Storm #3
Frequency (years)	100		
Rainfall, P, 24-hr (in)	7.2		
Initial Abstraction, Ia (in)	0.500	0.500	0.500
Ia/p Ratio	0.069	0.000	0.000
Unit Discharge, * qu (csm/in)	599	0	0
Runoff, Q (in)	4.88	0.000	0.000
Pond & Swamp Adjustment Factor	1.00	1.00	1.00
PEAK DISCHARGE, qp (cfs)	5574	0	0

Summary of Computations for qu

Ia/p #1	0.100	0.000	0.000
C0 #1	2.553	0.000	0.000
C1 #1	-0.615	0.000	0.000
C2 #1	-0.164	0.000	0.000
qu (csm) #1	598.886	0.000	0.000
Ia/p #2	0.100	0.000	0.000
C0 #2	2.553	0.000	0.000
C1 #2	-0.615	0.000	0.000
C2 #2	-0.164	0.000	0.000
qu (csm) #2	598.886	0.000	0.000
* qu (csm)	599	0	0

\* Interpolated for computed Ia/p ratio (between Ia/p #1 & Ia/p #2)  
If computed Ia/p exceeds Ia/p limits, bounding limit for Ia/p is used.

$$\log(\text{qu}) = C0 + (C1 * \log(\text{Tc})) + (C2 * (\log(\text{Tc}))^2)$$

$$\text{qp (cfs)} = \text{qu(csm)} * \text{Area(sq.mi.)} * \text{Q(in.)} * (\text{Pond \& Swamp Adj})$$

# BOX CULVERT DESIGN

JVS 17JUL98

OM CULVERT BR#A500  
 OM file: A506LRF1.pol  
 OM Date: 17Jul98  
 OM Hydraulic Design  
 OM Quintuple Box Culvert (No Haunch)  
 OM 5-Cell Box 12'x 12' Design as 4-Cell  
 OM Load Factor Design  
 OM Rigid Frame Method  
 OM Top and Bot Slab Different  
 OM Exterior and Interior Wall Different  
 OM  
 OM Minumum Fill Ht Condition (1.0 Ft)  
 OM

BCU  
18 July 98

STDLOD 2, 0, 0, 0, 0  
 SWPRES 1, 2, 60, 15, 62.4  
 BOXDIM 1, 4, 12, 12, 2, 10  
 SLBTHK 1, 11.5, 11.5, 9.5, 8, 1111  
 H&SKEW 1, 90, 90, 0, 0, 0  
 REEBAR 18, 9, 1, 11, 4, .016  
 CONCOV 2, 3, 2, 1.5, .5, .5  
 MATPRP 120, 60, 24, 3, 0, 0  
 PRTCTL 1, 1, 1, 0  
 F&HCTL 1, 1, 1  
 DESCTL 1, 0, 1, 0, 0, 9

CONSTANT DATA

STANDARD LIVE LOAD				-	DESIGN METHOD				-	PRINT CONTROL			
TRUCK	OMIT	STRESS	OVERLD	-	SERVICE	LOAD	-	10th Pt	INFL	LOC.	NEG		
CODE	L.L.	0-FILL	AXLE	-	LOAD	FACTOR	-	MOMENT	LINE	MOMENT			
HS20	NO	NO	0.		NO	YES		YES	YES	1.00			

MATERIAL PROPERTIES							-	THICKNESS	
SOIL	STEEL	STEEL	CONCRETE	CONCRETE	CON.SHEAR	-	INCREMENTS		
WEIGHT	Fy	Fs	STRENGTH	SHEAR	W/ STIRRUP	-	SLAB	WALL	
120.	60000.	24000.	3000.	0.	0.		0.50	0.50	

CONCRETE COVER				-	DESIGN	-	PRINT	-	REINFORCING			
EXTERIOR		INTERIOR		-	SAME	-	BAR	-	BAR SPACING		BAR SIZE	
TOP	BOT	WALL	(ALL)	-	THICKNESS	-	TABLE	-	MAX	MIN	MAX	MIN
SLAB	SLAB			-	SLAB WALL	-		-				
2.00	3.00	2.00	1.50		NO	NO	YES		18.0	9.0	11	4

CRACK PARAMETER Z = 98.0  
 MODULAR RATIO N = 9.0

SUPERIMPOSED DEAD LOADS						-	SPECIAL LIVE LOADS		
UNIFORM			CONCENTRATED LOAD			-	WHEEL	FILL	OVERSTRESS
LOAD	WT.	X1	WT.	X2	WT.	X3	LOAD	HEIGHT	FACTOR
0.000	0.00	0.0	0.00	0.0	0.00	0.0	0.000	0.000	1.00

DATA FOR STRUCTURE NUMBER 1

CULVERT	-	SPAN	-	CLEAR	-	DESIGN	-	CENTERLINE	-	SKEW	-	SKEW	-	FLOOR
TYPE	-	LENGTH	-	HEIGHT	-	FILL	-	LENGTH	-	LEFT	-	RIGHT	-	TYPE
QDRPLE		12.00		12.00		2.00		10.00		90		90		FULL

SLAB THICKNESSES				-	LIVE	-	SOIL	-	WATER
TOP	BOT.	EXT.	INT.	-	LOAD	-	PRESSURE	-	PRESSURE
SLAB	SLAB	WALL	WALL	-	SURCHARGE	-	MAX	MIN	
11.50F	11.50F	9.50F	8.00F		2.00		60.0	15.0	62.4

TOP HAUNCH	BOTTOM HAUNCH	-	RIGID OR	-	CHECK	-	BAR SPACING
HEIGHT	HEIGHT	-	FLEXIBLE	-	MILITARY	-	INCREMENT
0.0	0.0		RIGID		NO		1 INCH

BOTH HEADWALLS ELIMINATED.

\*\*\*\*\* LOAD FACTOR DESIGN \*\*\*\*\*  
 \*\*\*\*\* STRESSES AT CRITICAL SECTIONS \*\*\*\*\*

\*\*\* MAXIMUM REINFORCEMENT RATIO (As/bd) = .016

MEMBER NUMBER = 1  
 MEMBER THICKNESS = 9.50  
 EXTERIOR WAL

	-MOMENT-	-AXIAL-	-SHEAR-	-Po-	-Mu-	-Mbal-	-Pbal-	-STEEL-	-SHEAR-	-ALL.-	-ALL.-
	FORCE							AREA	STRESS	MOM.	SHEAR
LT	-20.9	9.6	6.9	242.4	20.9	28.0	50.7	0.94	103.2	22.2	109.5
MID	8.4	11.3	2.4	223.0	8.4	24.0	80.0	0.38	33.7	10.6	109.5
MID-	-9.2	7.3	2.4	225.0	9.2	24.0	71.5	0.37	36.1	10.7	109.5
RT	-17.8	4.8	4.9	237.5	17.8	27.0	56.5	0.79	73.2	18.6	109.5

MEMBER NUMBER = 2  
 MEMBER THICKNESS = 11.50  
 TOP SLAB

	-MOMENT-	-AXIAL-	-SHEAR-	-Po-	-Mu-	-Mbal-	-Pbal-	-STEEL-	-SHEAR-	-ALL.-	-ALL.-
	FORCE							AREA	STRESS	MOM.	SHEAR
LT	-18.4	5.4	9.9	276.7	18.4	40.0	93.3	0.68	107.6	19.7	109.5
MID	27.0	0.2	5.0	284.8	27.0	45.0	89.6	0.83	51.9	27.1	109.5
RT	-20.5	-2.4	9.3	281.2	22.4	42.0	87.7	0.75	101.2	21.8	109.5

MEMBER NUMBER = 3  
 MEMBER THICKNESS = 8.00  
 INTERIOR WAL

	-MOMENT-	-AXIAL-	-SHEAR-	-Po-	-Mu-	-Mbal-	-Pbal-	-STEEL-	-SHEAR-	-ALL.-	-ALL.-
	FORCE							AREA	STRESS	MOM.	SHEAR
LT	-11.6	5.6	1.5	197.7	11.6	16.0	45.2	0.46	28.8	12.1	109.5
MID	2.6	6.9	1.5	186.8	5.0	14.0	56.6	0.19	28.8	6.1	109.5
RT	-11.0	7.2	1.6	196.7	11.0	16.0	46.2	0.44	31.1	11.8	109.5

MEMBER NUMBER = 4  
 MEMBER THICKNESS = 11.50  
 BOTTOM SLAB

	-MOMENT-	-AXIAL-	-SHEAR-	-Po-	-Mu-	-Mbal-	-Pbal-	-STEEL-	-SHEAR-	-ALL.-	-ALL.-
	FORCE							AREA	STRESS	MOM.	SHEAR
LT	-21.8	4.7	7.0	283.9	21.8	38.0	71.0	0.93	85.9	22.9	109.5
MID	14.2	-0.6	2.3	272.6	15.5	40.0	105.1	0.46	23.7	15.4	109.5
RT	-29.2*	-0.6	7.7	294.1	29.2	41.0	58.1	1.11	94.4	29.1	109.5

MEMBER NUMBER = 5  
 MEMBER THICKNESS = 11.50  
 TOP SLAB

	-MOMENT-	-AXIAL-	-SHEAR-	-Po-	-Mu-	-Mbal-	-Pbal-	-STEEL-	-SHEAR-	-ALL.-	-ALL.-
	FORCE							AREA	STRESS	MOM.	SHEAR
LT	-19.6*	-0.2	10.1	278.0	19.6	41.0	91.7	0.69	109.9*	19.5	109.5
MID	25.3	0.3	5.3	282.9	25.3	44.0	92.0	0.77	54.7	25.4	109.5
RT	-18.6	2.1	9.4	277.0	18.6	40.0	93.0	0.65	102.3	19.1	109.5

MEMBER NUMBER = 6  
 MEMBER THICKNESS = 8.00  
 INTERIOR WAL

	-MOMENT-	-AXIAL-	-SHEAR-	-Po-	-Mu-	-Mbal-	-Pbal-	-STEEL-	-SHEAR-	-ALL.-	-ALL.-
	FORCE							AREA	STRESS	MOM.	SHEAR
LT	-10.2	6.5	1.4	195.3	10.2	16.0	47.7	0.40	27.3	11.0	109.5
MID	1.5	6.0	1.4	186.8	5.0	14.0	56.6	0.19	27.3	6.0	109.5
RT	-6.4	11.1	1.5	189.0	6.4	15.0	54.2	0.25	28.8	8.2	109.5

MEMBER NUMBER = 7  
 MEMBER THICKNESS = 11.50  
 BOTTOM SLAB

	-MOMENT-	-AXIAL-	-SHEAR-	-Po-	-Mu-	-Mbal-	-Pbal-	-STEEL-	-SHEAR-	-ALL.-	-ALL.-
	FORCE							AREA	STRESS	MOM.	SHEAR
LT	-30.4	-3.7	5.9	299.8	33.0	42.0	51.0	1.16	72.2	32.4	109.5
MID	10.3	10.1	2.0	268.5	11.5	39.0	110.2	0.34	21.1	14.0	109.5
RT	-29.2	7.5	6.8	294.2	29.2	41.0	58.0	1.17	82.9	30.8	109.5

NOTE: ASTERISK IMPLIES DESIGN VALUES EXCEED CRITICAL VALUES

\*\*\*\*\* ATTENTION: OVERSTRESS DUE TO FIXED THICKNESS



A CORNER BAR(T)				A CORNER BAR(B)				A TSLAB+		A TSLAB-	
H	V	SZ	SPG	H	V	SZ	SPG	SZ	SPG	SZ	SPG
46	39	7	9.0	70	62	9	9.0	8	9.0	8	9.0

A BSLAB+		A BSLAB-		B EXTIN		B EXTOUT		B INTWL		C1
SZ	SPG	SZ	SPG	SZ	SPG	SZ	SPG	SZ	SPG	BARS
6	9.0	10	9.0	5	9.0	8	9.0	7	9.0	192

\*\* THE HEIGHT OF C.H.C.U. \*\*  
 BOTTOM SLAB = 4.50 IN  
 TOP SLAB = 5.75 IN

** T.SLAB *	B.SLAB *	WALL *	INWALL *	*** VOLUME ***	*** STEEL **
IN	IN	IN	IN	CY/FT	LB/FT
11.50	11.50	9.50	8.00	5.254	1364

\*\* REINFORCING STEEL BAR SCHEDULE \*\*

-----

* LOCATN *	BAR	* NO.	* SZ	* TYP	* LNTH	* WT.	* H LEG	* V LEG
TOP SLAB POSV	MAIN A100	14	8	STR	51- 2	1913		
BOT SLAB POSV	MAIN A200	14	6	STR	51- 2	1076		
TOP SLAB NEGV	MAIN A300	14	8	STR	51- 2	1913		
BOT SLAB NEGV	MAIN A400	14	10	STR	51- 2	3082		
CORNER (TOP)	A1	28	7	6	7- 1	405	3-10	3- 3
CORNER (BOTTOM)	A2	28	9	6	11- 0	1047	5-10	5- 2
EXTWALL IN	B1	28	5	STR	13- 5	392		
EXTWALL OUT	B2	28	8	STR	11- 4	847		
INTWALL	B3	42	7	STR	13- 5	1152		
LONGTD ( 1)	C1	192	4	STR	9- 8	1240		
TOTAL						13067		

\*\*\*\*\* SPLICE LENGTHS CHART \*\*\*\*\*

BAR	SIZE	SPLICE LENGTH
A200	6	2- 3
A400	10	6- 4
B1	5	1- 8
B3	7	3- 0
C1	4	2- 2

\*\* MOMENT \* AXIAL FORCE \* SHEAR FOR LOAD FACTOR DESIGN AT TENTH POINT \*\*

M-PT	+MOMENT	-MOMENT	+A. F.	-A. F.	+SHEAR	-SHEAR
1- 0	11.097	-24.364	10.555	9.605	8.245	-4.036
1- 1	6.267	-14.938	10.555	9.605	6.645	-3.238
1- 2	7.471	-12.560	11.720	8.440	5.176	-2.533
1- 3	8.761	-11.235	11.720	8.440	3.837	-1.921
1- 4	8.402	-9.228	11.345	7.292	2.630	-1.403
1- 5	6.887	-7.820	3.804	6.169	2.423	-1.847
1- 6	7.744	-7.446	9.605	5.744	2.754	-2.793
1- 7	7.991	-8.138	9.605	4.847	2.992	-3.607
1- 8	7.268	-8.551	9.605	4.054	3.137	-4.290
1- 9	10.454	-13.656	8.440	4.980	3.188	-4.843
1-10	14.568	-20.233	8.440	4.756	3.145	-5.264
2- 0	14.568	-20.233	-3.146	5.457	11.007	-0.794
2- 1	19.802	-14.406	-2.621	5.430	9.750	-1.011
2- 2	23.706	-10.148	0.287	5.430	8.520	-2.032
2- 3	26.556	-7.010	0.256	4.713	7.321	-3.079
2- 4	27.044	-4.505	0.219	4.624	6.157	-4.140
2- 5	26.416	-3.082	-1.034	4.624	5.032	-5.200
2- 6	24.484	-3.046	-0.142	3.720	3.950	-6.245
2- 7	20.926	-4.549	-0.548	2.767	2.916	-7.263
2- 8	17.307	-8.396	4.626	-2.681	1.932	-8.239
2- 9	13.643	-14.125	2.022	-3.146	1.004	-9.160
2-10	9.668	-22.702	2.317	-2.147	0.135	-10.012
3- 0	11.182	-12.464	7.740	5.723	1.452	-1.569
3- 1	8.987	-10.056	7.740	5.440	1.452	-1.569
3- 2	6.792	-7.415	7.740	5.440	1.452	-1.569
3- 3	4.648	-4.915	7.490	5.168	1.452	-1.569
3- 4	2.562	-2.272	6.911	10.589	1.452	-1.569
3- 5	1.514	-1.205	11.734	9.544	1.452	-1.569
3- 6	3.942	-3.040	10.182	7.991	1.452	-1.569
3- 7	6.531	-5.161	9.394	7.535	1.452	-1.569
3- 8	9.178	-7.365	9.017	7.319	1.452	-1.569
3- 9	11.849	-9.582	9.017	7.319	1.452	-1.569
3-10	14.533	-11.845	8.659	7.112	1.452	-1.569
4- 0	11.445	-24.364	-4.147	4.678	7.953	1.981
4- 1	13.616	-16.187	-0.794	4.678	6.821	1.068
4- 2	14.850	-9.423	-0.635	4.678	5.690	0.155
4- 3	14.645	-4.069	-0.635	4.678	4.558	-0.758
4- 4	14.152	0.123	-0.635	5.977	3.427	-1.802
4- 5	13.739	1.215	-4.037	6.504	2.296	-2.933
4- 6	12.337	-2.113	-4.081	6.696	1.164	-4.065
4- 7	9.917	-6.823	-4.113	7.989	0.105	-5.196
4- 8	6.859	-12.915	0.525	3.351	-0.808	-6.328
4- 9	3.649	-21.690	4.745	-0.635	-1.721	-7.459
4-10	0.867	-31.839	4.745	-0.635	-2.634	-8.591
5- 0	9.869	-21.211	4.672	0.029	11.067	0.666
5- 1	14.874	-14.936	4.994	-0.727	9.916	-0.157
5- 2	19.233	-10.045	5.266	-0.667	8.755	-1.587
5- 3	23.039	-5.720	6.638	-0.667	7.592	-2.571
5- 4	24.657	-4.265	0.327	-4.300	6.438	-3.610
5- 5	25.309	-4.702	0.327	-4.300	5.301	-4.691
5- 6	24.491	-5.705	0.327	-4.300	4.192	-5.804
5- 7	22.766	-7.287	3.805	-1.337	3.120	-6.937
5- 8	19.509	-9.844	1.578	2.131	2.094	-8.080

5- 9	15.357	-14.017	1.395	2.131	1.125	-9.221
5-10	10.709	-20.282	1.164	2.132	0.221	-10.349
6- 0	7.129	-11.002	7.016	6.469	1.375	-1.451
6- 1	5.722	-8.747	7.016	6.469	1.375	-1.451
6- 2	4.316	-6.512	6.721	5.224	1.375	-1.451
6- 3	2.909	-4.301	6.454	5.224	1.375	-1.451
6- 4	1.543	-2.160	5.989	10.057	1.375	-1.451
6- 5	1.031	-1.031	8.617	9.303	1.375	-1.451
6- 6	2.986	-1.326	11.471	11.094	1.375	-1.451
6- 7	5.146	-2.719	8.163	11.094	1.375	-1.451
6- 8	7.369	-4.126	7.761	11.094	1.375	-1.451
6- 9	9.618	-5.533	7.372	11.094	1.375	-1.451
6-10	11.873	-6.940	7.372	11.094	1.375	-1.451
7- 0	1.138	-32.868	3.889	-3.865	6.606	2.721
7- 1	4.928	-23.512	5.541	-3.053	5.693	1.808
7- 2	7.752	-15.505	5.284	-3.053	4.779	0.894
7- 3	9.066	-8.868	5.284	-3.053	3.866	-0.019
7- 4	8.308	-3.795	4.346	0.760	2.953	-0.932
7- 5	10.251	-1.346	10.125	0.760	2.040	-1.995
7- 6	11.196	-1.839	10.125	0.760	1.127	-3.127
7- 7	11.094	-8.514	-5.285	8.359	0.214	-4.258
7- 8	9.650	-14.757	-5.285	8.882	-0.699	-5.389
7- 9	7.719	-22.501	-4.945	7.765	-1.612	-6.521
7-10	4.906	-31.633	-4.945	7.342	-2.525	-7.652

\*\*\*\*\* INFLUENCE LINES FOR MOMENT \*\*\*\*\*

	***** MEMBER NO. 1 *****										
	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9	1.0
100	-1.43	-1.15	-0.87	-0.59	-0.31	-0.03	0.25	0.53	0.81	1.10	1.38
105	-1.31	-1.06	-0.82	-0.58	-0.34	-0.10	0.14	0.38	0.62	0.87	1.11
110	-1.17	-0.97	-0.77	-0.56	-0.36	-0.16	0.05	0.25	0.45	0.66	0.86
115	-1.04	-0.87	-0.70	-0.54	-0.37	-0.20	-0.04	0.13	0.30	0.47	0.63
120	-0.90	-0.77	-0.64	-0.50	-0.37	-0.24	-0.10	0.03	0.16	0.29	0.43
125	-0.77	-0.67	-0.56	-0.46	-0.36	-0.26	-0.16	-0.06	0.04	0.14	0.24
130	-0.63	-0.56	-0.49	-0.42	-0.35	-0.28	-0.21	-0.14	-0.07	0.00	0.07
135	-0.50	-0.45	-0.41	-0.37	-0.33	-0.29	-0.25	-0.20	-0.16	-0.12	-0.08
140	-0.36	-0.35	-0.33	-0.32	-0.30	-0.29	-0.27	-0.26	-0.24	-0.23	-0.21
145	-0.23	-0.24	-0.25	-0.26	-0.27	-0.28	-0.29	-0.30	-0.31	-0.32	-0.33
150	-0.11	-0.14	-0.17	-0.21	-0.24	-0.27	-0.30	-0.33	-0.37	-0.40	-0.43
155	0.01	-0.04	-0.09	-0.15	-0.20	-0.25	-0.31	-0.36	-0.41	-0.47	-0.52
160	0.13	0.05	-0.02	-0.09	-0.16	-0.23	-0.31	-0.38	-0.45	-0.52	-0.59
165	0.24	0.15	0.06	-0.03	-0.12	-0.21	-0.30	-0.39	-0.48	-0.57	-0.66
170	0.34	0.23	0.13	0.02	-0.08	-0.18	-0.29	-0.39	-0.50	-0.60	-0.71
175	0.43	0.31	0.19	0.08	-0.04	-0.16	-0.28	-0.39	-0.51	-0.63	-0.75
180	0.51	0.38	0.26	0.13	0.00	-0.13	-0.26	-0.39	-0.52	-0.65	-0.78
185	0.59	0.45	0.31	0.17	0.03	-0.10	-0.24	-0.38	-0.52	-0.66	-0.80
190	0.65	0.50	0.36	0.21	0.07	-0.08	-0.22	-0.37	-0.52	-0.66	-0.81
195	0.70	0.55	0.40	0.25	0.10	-0.05	-0.21	-0.36	-0.51	-0.66	-0.81
200	0.74	0.59	0.43	0.28	0.12	-0.03	-0.19	-0.34	-0.50	-0.66	-0.81
205	0.77	0.61	0.46	0.30	0.14	-0.02	-0.18	-0.33	-0.49	-0.65	-0.81
210	0.80	0.64	0.48	0.32	0.16	0.00	-0.16	-0.32	-0.48	-0.64	-0.80
215	0.81	0.65	0.49	0.33	0.17	0.01	-0.15	-0.31	-0.48	-0.64	-0.80
220	0.83	0.67	0.50	0.34	0.18	0.02	-0.15	-0.31	-0.47	-0.63	-0.79
225	0.84	0.67	0.51	0.35	0.19	0.02	-0.14	-0.30	-0.47	-0.63	-0.79
230	0.84	0.68	0.51	0.35	0.19	0.03	-0.14	-0.30	-0.46	-0.62	-0.79
235	0.84	0.68	0.51	0.35	0.19	0.03	-0.13	-0.30	-0.46	-0.62	-0.78
240	0.83	0.67	0.51	0.35	0.19	0.03	-0.13	-0.29	-0.45	-0.62	-0.78
245	0.82	0.67	0.51	0.35	0.19	0.03	-0.13	-0.29	-0.45	-0.61	-0.77
250	0.81	0.65	0.50	0.34	0.18	0.02	-0.13	-0.29	-0.45	-0.60	-0.76
255	0.79	0.64	0.49	0.33	0.18	0.02	-0.13	-0.29	-0.44	-0.60	-0.75
260	0.77	0.62	0.47	0.32	0.17	0.02	-0.14	-0.29	-0.44	-0.59	-0.74
265	0.75	0.60	0.45	0.31	0.16	0.01	-0.14	-0.29	-0.43	-0.58	-0.73
270	0.72	0.58	0.44	0.29	0.15	0.00	-0.14	-0.28	-0.43	-0.57	-0.71
275	0.69	0.55	0.42	0.28	0.14	0.00	-0.14	-0.28	-0.42	-0.56	-0.70
280	0.66	0.53	0.39	0.26	0.13	-0.01	-0.14	-0.28	-0.41	-0.54	-0.68
285	0.63	0.50	0.37	0.24	0.11	-0.01	-0.14	-0.27	-0.40	-0.53	-0.66
290	0.59	0.47	0.35	0.22	0.10	-0.02	-0.14	-0.27	-0.39	-0.51	-0.63
295	0.55	0.44	0.32	0.20	0.09	-0.03	-0.14	-0.26	-0.37	-0.49	-0.60
300	0.51	0.40	0.29	0.19	0.08	-0.03	-0.14	-0.25	-0.36	-0.46	-0.57
305	0.47	0.37	0.27	0.17	0.07	-0.04	-0.14	-0.24	-0.34	-0.44	-0.54
310	0.43	0.33	0.24	0.15	0.05	-0.04	-0.13	-0.22	-0.32	-0.41	-0.50
315	0.38	0.30	0.21	0.13	0.04	-0.04	-0.13	-0.21	-0.30	-0.38	-0.47
320	0.34	0.27	0.19	0.11	0.03	-0.04	-0.12	-0.20	-0.28	-0.35	-0.43
325	0.30	0.23	0.16	0.09	0.02	-0.05	-0.11	-0.18	-0.25	-0.32	-0.39
330	0.26	0.20	0.14	0.08	0.01	-0.05	-0.11	-0.17	-0.23	-0.29	-0.35
335	0.22	0.16	0.11	0.06	0.01	-0.05	-0.10	-0.15	-0.20	-0.26	-0.31
340	0.17	0.13	0.09	0.04	0.00	-0.05	-0.09	-0.14	-0.18	-0.22	-0.27
345	0.13	0.10	0.06	0.02	-0.01	-0.05	-0.08	-0.12	-0.15	-0.19	-0.22
350	0.09	0.06	0.03	0.01	-0.02	-0.05	-0.07	-0.10	-0.13	-0.15	-0.18
355	0.04	0.03	0.01	-0.01	-0.03	-0.05	-0.06	-0.08	-0.10	-0.12	-0.13
360	0.00	-0.01	-0.02	-0.03	-0.04	-0.04	-0.05	-0.06	-0.07	-0.08	-0.09
365	-0.05	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04
370	-0.09	-0.08	-0.07	-0.06	-0.05	-0.04	-0.03	-0.02	-0.01	0.00	0.01

375	-0.14	-0.12	-0.10	-0.08	-0.06	-0.04	-0.02	0.00	0.02	0.04	0.06
380	-0.18	-0.15	-0.13	-0.10	-0.07	-0.04	-0.01	0.02	0.05	0.08	0.11
385	-0.23	-0.19	-0.15	-0.11	-0.08	-0.04	0.00	0.04	0.08	0.12	0.16
390	-0.28	-0.23	-0.18	-0.13	-0.08	-0.04	0.01	0.06	0.11	0.16	0.21
395	-0.33	-0.27	-0.21	-0.15	-0.09	-0.03	0.02	0.08	0.14	0.20	0.26
400	-0.38	-0.31	-0.24	-0.17	-0.10	-0.03	0.04	0.10	0.17	0.24	0.31
405	-0.43	-0.35	-0.27	-0.19	-0.11	-0.03	0.05	0.13	0.21	0.28	0.36
410	-0.48	-0.39	-0.30	-0.21	-0.12	-0.03	0.06	0.15	0.24	0.33	0.42
415	-0.53	-0.43	-0.33	-0.23	-0.13	-0.03	0.07	0.17	0.27	0.37	0.47
420	-0.58	-0.47	-0.36	-0.25	-0.14	-0.03	0.08	0.19	0.30	0.41	0.52
425	-0.63	-0.51	-0.39	-0.27	-0.15	-0.03	0.09	0.21	0.33	0.45	0.57
430	-0.68	-0.55	-0.42	-0.29	-0.16	-0.03	0.10	0.23	0.36	0.49	0.63
435	-0.74	-0.59	-0.45	-0.31	-0.17	-0.03	0.11	0.25	0.40	0.54	0.68
440	-0.79	-0.64	-0.48	-0.33	-0.18	-0.03	0.12	0.27	0.43	0.58	0.73
445	-0.84	-0.68	-0.52	-0.35	-0.19	-0.03	0.13	0.30	0.46	0.62	0.78
450	-0.89	-0.72	-0.55	-0.38	-0.20	-0.03	0.14	0.32	0.49	0.66	0.84
455	-0.95	-0.76	-0.58	-0.40	-0.21	-0.03	0.15	0.34	0.52	0.71	0.89
460	-1.00	-0.81	-0.61	-0.42	-0.22	-0.03	0.16	0.36	0.55	0.75	0.94
465	-1.06	-0.85	-0.65	-0.44	-0.23	-0.03	0.18	0.38	0.59	0.79	1.00
470	-1.11	-0.89	-0.68	-0.46	-0.25	-0.03	0.19	0.40	0.62	0.83	1.05
475	-1.16	-0.94	-0.71	-0.48	-0.26	-0.03	0.20	0.42	0.65	0.88	1.10
480	-1.22	-0.98	-0.74	-0.51	-0.27	-0.03	0.21	0.44	0.68	0.92	1.16
485	-1.27	-1.02	-0.78	-0.53	-0.28	-0.03	0.22	0.46	0.71	0.96	1.21
490	-1.33	-1.07	-0.81	-0.55	-0.29	-0.03	0.23	0.49	0.75	1.00	1.26
495	-1.38	-1.11	-0.84	-0.57	-0.30	-0.03	0.24	0.51	0.78	1.05	1.32
500	-1.44	-1.16	-0.88	-0.60	-0.31	-0.03	0.25	0.53	0.81	1.09	1.37

\*\*\*\*\* MEMBER NO. 2 \*\*\*\*\*

	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9	1.0
100	1.38	1.12	0.87	0.62	0.37	0.11	-0.14	-0.39	-0.64	-0.90	-1.15
105	1.11	1.45	1.16	0.87	0.57	0.28	-0.01	-0.30	-0.60	-0.89	-1.18
110	0.86	1.80	1.46	1.13	0.80	0.46	0.13	-0.20	-0.54	-0.87	-1.21
115	0.63	1.53	1.79	1.41	1.04	0.66	0.28	-0.09	-0.47	-0.85	-1.22
120	0.43	1.28	2.13	1.71	1.29	0.87	0.45	0.03	-0.39	-0.81	-1.23
125	0.24	1.05	1.86	2.03	1.57	1.10	0.64	0.17	-0.29	-0.76	-1.22
130	0.07	0.84	1.60	2.36	1.85	1.35	0.84	0.33	-0.18	-0.69	-1.20
135	-0.08	0.64	1.36	2.08	2.16	1.61	1.05	0.50	-0.05	-0.61	-1.16
140	-0.21	0.46	1.14	1.81	2.48	1.89	1.29	0.69	0.09	-0.51	-1.11
145	-0.33	0.30	0.93	1.56	2.19	2.18	1.54	0.89	0.25	-0.39	-1.04
150	-0.43	0.15	0.74	1.32	1.91	2.49	1.81	1.12	0.43	-0.26	-0.94
155	-0.52	0.02	0.56	1.11	1.65	2.19	2.09	1.36	0.63	-0.10	-0.83
160	-0.59	-0.09	0.40	0.90	1.40	1.90	2.40	1.63	0.85	0.08	-0.69
165	-0.66	-0.20	0.26	0.72	1.18	1.63	2.09	1.91	1.10	0.29	-0.53
170	-0.71	-0.29	0.13	0.55	0.97	1.39	1.81	2.22	1.37	0.51	-0.34
175	-0.75	-0.36	0.02	0.40	0.78	1.16	1.54	1.92	1.66	0.77	-0.12
180	-0.78	-0.43	-0.09	0.26	0.60	0.95	1.29	1.64	1.98	1.06	0.13
185	-0.80	-0.48	-0.17	0.14	0.45	0.76	1.07	1.38	1.70	1.37	0.41
190	-0.81	-0.53	-0.25	0.03	0.31	0.59	0.87	1.15	1.43	1.71	0.72
195	-0.81	-0.56	-0.31	-0.06	0.20	0.45	0.70	0.95	1.20	1.46	1.07
200	-0.81	-0.58	-0.36	-0.13	0.10	0.32	0.55	0.78	1.00	1.23	1.46
205	-0.81	-0.60	-0.40	-0.19	0.01	0.22	0.42	0.62	0.83	1.03	1.24
210	-0.80	-0.62	-0.43	-0.25	-0.06	0.12	0.31	0.49	0.67	0.86	1.04
215	-0.80	-0.63	-0.46	-0.30	-0.13	0.04	0.20	0.37	0.54	0.71	0.87
220	-0.79	-0.64	-0.49	-0.34	-0.19	-0.03	0.12	0.27	0.42	0.57	0.73
225	-0.79	-0.65	-0.51	-0.37	-0.24	-0.10	0.04	0.18	0.32	0.46	0.60
230	-0.79	-0.66	-0.53	-0.40	-0.28	-0.15	-0.02	0.11	0.23	0.36	0.49
235	-0.78	-0.66	-0.55	-0.43	-0.31	-0.19	-0.07	0.04	0.16	0.28	0.40
240	-0.78	-0.67	-0.56	-0.45	-0.34	-0.23	-0.12	-0.01	0.10	0.21	0.32
245	-0.77	-0.67	-0.56	-0.46	-0.36	-0.25	-0.15	-0.05	0.05	0.16	0.26
250	-0.76	-0.66	-0.57	-0.47	-0.37	-0.27	-0.18	-0.08	0.02	0.12	0.21
255	-0.75	-0.66	-0.57	-0.47	-0.38	-0.29	-0.20	-0.10	-0.01	0.08	0.18
260	-0.74	-0.65	-0.56	-0.47	-0.39	-0.30	-0.21	-0.12	-0.03	0.06	0.15
265	-0.73	-0.64	-0.56	-0.47	-0.39	-0.30	-0.21	-0.13	-0.04	0.04	0.13
270	-0.71	-0.63	-0.55	-0.47	-0.38	-0.30	-0.22	-0.13	-0.05	0.03	0.12

275	-0.70	-0.62	-0.54	-0.46	-0.38	-0.30	-0.21	-0.13	-0.05	0.03	0.11
280	-0.68	-0.60	-0.52	-0.44	-0.37	-0.29	-0.21	-0.13	-0.05	0.02	0.10
285	-0.66	-0.58	-0.51	-0.43	-0.35	-0.28	-0.20	-0.13	-0.05	0.02	0.10
290	-0.63	-0.56	-0.49	-0.41	-0.34	-0.27	-0.19	-0.12	-0.05	0.02	0.10
295	-0.60	-0.53	-0.46	-0.39	-0.32	-0.26	-0.19	-0.12	-0.05	0.02	0.09
300	-0.57	-0.51	-0.44	-0.37	-0.31	-0.24	-0.18	-0.11	-0.05	0.02	0.09
305	-0.54	-0.48	-0.42	-0.35	-0.29	-0.23	-0.17	-0.11	-0.05	0.01	0.08
310	-0.50	-0.45	-0.39	-0.33	-0.28	-0.22	-0.17	-0.11	-0.05	0.00	0.06
315	-0.47	-0.42	-0.37	-0.32	-0.26	-0.21	-0.16	-0.11	-0.06	-0.01	0.04
320	-0.43	-0.39	-0.34	-0.30	-0.25	-0.21	-0.16	-0.12	-0.07	-0.03	0.02
325	-0.39	-0.35	-0.32	-0.28	-0.24	-0.20	-0.16	-0.13	-0.09	-0.05	-0.01
330	-0.35	-0.32	-0.29	-0.26	-0.23	-0.20	-0.17	-0.14	-0.10	-0.07	-0.04
335	-0.31	-0.29	-0.26	-0.24	-0.22	-0.19	-0.17	-0.15	-0.12	-0.10	-0.08
340	-0.27	-0.25	-0.24	-0.22	-0.21	-0.19	-0.17	-0.16	-0.14	-0.13	-0.11
345	-0.22	-0.22	-0.21	-0.20	-0.19	-0.19	-0.18	-0.17	-0.17	-0.16	-0.15
350	-0.18	-0.18	-0.18	-0.18	-0.18	-0.19	-0.19	-0.19	-0.19	-0.19	-0.19
355	-0.13	-0.14	-0.15	-0.16	-0.17	-0.18	-0.19	-0.20	-0.21	-0.22	-0.23
360	-0.09	-0.11	-0.13	-0.14	-0.16	-0.18	-0.20	-0.22	-0.24	-0.26	-0.28
365	-0.04	-0.07	-0.10	-0.12	-0.15	-0.18	-0.21	-0.24	-0.26	-0.29	-0.32
370	0.01	-0.03	-0.07	-0.10	-0.14	-0.18	-0.21	-0.25	-0.29	-0.33	-0.36
375	0.06	0.01	-0.04	-0.08	-0.13	-0.18	-0.22	-0.27	-0.31	-0.36	-0.41
380	0.11	0.05	0.00	-0.06	-0.12	-0.17	-0.23	-0.28	-0.34	-0.39	-0.45
385	0.16	0.09	0.03	-0.04	-0.10	-0.17	-0.23	-0.30	-0.36	-0.43	-0.49
390	0.21	0.13	0.06	-0.01	-0.09	-0.16	-0.24	-0.31	-0.39	-0.46	-0.53
395	0.26	0.18	0.09	0.01	-0.07	-0.16	-0.24	-0.32	-0.41	-0.49	-0.57
400	0.31	0.22	0.13	0.03	-0.06	-0.15	-0.24	-0.33	-0.43	-0.52	-0.61
405	0.36	0.26	0.16	0.06	-0.04	-0.14	-0.24	-0.34	-0.45	-0.55	-0.65
410	0.42	0.31	0.20	0.09	-0.02	-0.13	-0.24	-0.35	-0.46	-0.57	-0.68
415	0.47	0.35	0.23	0.11	-0.01	-0.12	-0.24	-0.36	-0.48	-0.60	-0.72
420	0.52	0.39	0.27	0.14	0.01	-0.11	-0.24	-0.37	-0.49	-0.62	-0.75
425	0.57	0.44	0.30	0.17	0.03	-0.10	-0.24	-0.37	-0.51	-0.64	-0.78
430	0.63	0.48	0.34	0.20	0.05	-0.09	-0.23	-0.38	-0.52	-0.66	-0.81
435	0.68	0.53	0.38	0.22	0.07	-0.08	-0.23	-0.38	-0.53	-0.68	-0.84
440	0.73	0.57	0.41	0.25	0.09	-0.07	-0.23	-0.39	-0.54	-0.70	-0.86
445	0.78	0.62	0.45	0.28	0.11	-0.05	-0.22	-0.39	-0.56	-0.72	-0.89
450	0.84	0.66	0.49	0.31	0.14	-0.04	-0.21	-0.39	-0.57	-0.74	-0.92
455	0.89	0.71	0.52	0.34	0.16	-0.03	-0.21	-0.39	-0.57	-0.76	-0.94
460	0.94	0.75	0.56	0.37	0.18	-0.01	-0.20	-0.39	-0.58	-0.77	-0.96
465	1.00	0.80	0.60	0.40	0.20	0.00	-0.19	-0.39	-0.59	-0.79	-0.99
470	1.05	0.84	0.64	0.43	0.22	0.02	-0.19	-0.39	-0.60	-0.80	-1.01
475	1.10	0.89	0.68	0.46	0.25	0.03	-0.18	-0.39	-0.61	-0.82	-1.03
480	1.16	0.93	0.71	0.49	0.27	0.05	-0.17	-0.39	-0.61	-0.83	-1.06
485	1.21	0.98	0.75	0.52	0.29	0.07	-0.16	-0.39	-0.62	-0.85	-1.08
490	1.26	1.03	0.79	0.55	0.32	0.08	-0.15	-0.39	-0.63	-0.86	-1.10
495	1.32	1.07	0.83	0.59	0.34	0.10	-0.15	-0.39	-0.63	-0.88	-1.12
500	1.37	1.12	0.87	0.62	0.37	0.12	-0.14	-0.39	-0.64	-0.89	-1.14

\*\*\*\*\* MEMBER NO. 3 \*\*\*\*\*

	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9	1.0
100	-1.00	-0.80	-0.60	-0.40	-0.20	0.01	0.21	0.41	0.61	0.81	1.01
105	-1.01	-0.80	-0.60	-0.39	-0.19	0.02	0.22	0.43	0.63	0.84	1.04
110	-1.01	-0.80	-0.59	-0.39	-0.18	0.03	0.24	0.44	0.65	0.86	1.07
115	-1.00	-0.80	-0.59	-0.38	-0.17	0.04	0.25	0.46	0.67	0.88	1.08
120	-0.99	-0.78	-0.57	-0.37	-0.16	0.05	0.26	0.47	0.68	0.89	1.10
125	-0.97	-0.77	-0.56	-0.35	-0.14	0.06	0.27	0.48	0.69	0.89	1.10
130	-0.95	-0.74	-0.54	-0.34	-0.13	0.07	0.28	0.48	0.69	0.89	1.10
135	-0.92	-0.72	-0.52	-0.32	-0.12	0.08	0.28	0.48	0.69	0.89	1.09
140	-0.88	-0.69	-0.49	-0.30	-0.10	0.09	0.29	0.48	0.68	0.87	1.07
145	-0.84	-0.65	-0.47	-0.28	-0.09	0.10	0.29	0.47	0.66	0.85	1.04
150	-0.79	-0.61	-0.43	-0.26	-0.08	0.10	0.28	0.46	0.64	0.82	1.00
155	-0.74	-0.57	-0.40	-0.23	-0.06	0.11	0.28	0.45	0.62	0.79	0.96
160	-0.69	-0.53	-0.37	-0.21	-0.05	0.11	0.27	0.43	0.59	0.74	0.90
165	-0.62	-0.48	-0.33	-0.19	-0.04	0.11	0.25	0.40	0.55	0.69	0.84
170	-0.56	-0.43	-0.29	-0.16	-0.03	0.10	0.24	0.37	0.50	0.63	0.76

175	-0.49	-0.37	-0.26	-0.14	-0.02	0.10	0.21	0.33	0.45	0.56	0.68
180	-0.42	-0.32	-0.22	-0.12	-0.02	0.08	0.19	0.29	0.39	0.49	0.59
185	-0.34	-0.26	-0.18	-0.09	-0.01	0.07	0.15	0.24	0.32	0.40	0.48
190	-0.26	-0.20	-0.14	-0.07	-0.01	0.05	0.12	0.18	0.24	0.30	0.37
195	-0.18	-0.14	-0.10	-0.05	-0.01	0.03	0.07	0.11	0.16	0.20	0.24
200	-0.09	-0.07	-0.05	-0.03	-0.02	0.00	0.02	0.04	0.06	0.08	0.10
205	-0.01	-0.01	-0.01	-0.02	-0.02	-0.02	-0.02	-0.03	-0.03	-0.03	-0.03
210	0.07	0.05	0.03	0.00	-0.02	-0.04	-0.07	-0.09	-0.11	-0.14	-0.16
215	0.16	0.11	0.07	0.03	-0.02	-0.06	-0.10	-0.15	-0.19	-0.23	-0.28
220	0.23	0.17	0.11	0.05	-0.01	-0.07	-0.13	-0.20	-0.26	-0.32	-0.38
225	0.31	0.23	0.15	0.07	0.00	-0.08	-0.16	-0.24	-0.32	-0.40	-0.47
230	0.38	0.29	0.19	0.10	0.01	-0.09	-0.18	-0.28	-0.37	-0.47	-0.56
235	0.45	0.34	0.23	0.13	0.02	-0.09	-0.20	-0.31	-0.42	-0.53	-0.63
240	0.52	0.39	0.27	0.15	0.03	-0.09	-0.21	-0.33	-0.46	-0.58	-0.70
245	0.58	0.44	0.31	0.18	0.04	-0.09	-0.22	-0.36	-0.49	-0.62	-0.76
250	0.63	0.49	0.35	0.20	0.06	-0.08	-0.23	-0.37	-0.52	-0.66	-0.80
255	0.68	0.53	0.38	0.23	0.07	-0.08	-0.23	-0.38	-0.54	-0.69	-0.84
260	0.73	0.57	0.41	0.25	0.09	-0.07	-0.23	-0.39	-0.55	-0.71	-0.87
265	0.77	0.60	0.44	0.27	0.10	-0.06	-0.23	-0.40	-0.56	-0.73	-0.90
270	0.81	0.63	0.46	0.29	0.12	-0.05	-0.22	-0.40	-0.57	-0.74	-0.91
275	0.84	0.66	0.48	0.31	0.13	-0.04	-0.22	-0.39	-0.57	-0.75	-0.92
280	0.86	0.68	0.50	0.32	0.15	-0.03	-0.21	-0.39	-0.57	-0.75	-0.92
285	0.87	0.69	0.51	0.34	0.16	-0.02	-0.20	-0.38	-0.56	-0.74	-0.92
290	0.88	0.70	0.52	0.34	0.17	-0.01	-0.19	-0.37	-0.55	-0.73	-0.91
295	0.88	0.71	0.53	0.35	0.17	0.00	-0.18	-0.36	-0.54	-0.71	-0.89
300	0.88	0.70	0.53	0.35	0.18	0.00	-0.17	-0.35	-0.52	-0.70	-0.87
305	0.86	0.69	0.52	0.35	0.18	0.01	-0.16	-0.33	-0.50	-0.67	-0.84
310	0.85	0.68	0.52	0.35	0.18	0.01	-0.15	-0.32	-0.49	-0.65	-0.82
315	0.83	0.67	0.51	0.34	0.18	0.02	-0.14	-0.31	-0.47	-0.63	-0.79
320	0.81	0.65	0.50	0.34	0.18	0.02	-0.14	-0.29	-0.45	-0.61	-0.77
325	0.79	0.63	0.48	0.33	0.18	0.02	-0.13	-0.28	-0.43	-0.59	-0.74
330	0.76	0.61	0.47	0.32	0.17	0.03	-0.12	-0.27	-0.41	-0.56	-0.71
335	0.73	0.59	0.45	0.31	0.17	0.03	-0.11	-0.26	-0.40	-0.54	-0.68
340	0.70	0.57	0.43	0.30	0.16	0.03	-0.11	-0.24	-0.38	-0.51	-0.65
345	0.67	0.54	0.41	0.28	0.15	0.03	-0.10	-0.23	-0.36	-0.49	-0.62
350	0.63	0.51	0.39	0.27	0.15	0.03	-0.10	-0.22	-0.34	-0.46	-0.58
355	0.60	0.48	0.37	0.25	0.14	0.02	-0.09	-0.20	-0.32	-0.43	-0.55
360	0.56	0.45	0.34	0.24	0.13	0.02	-0.08	-0.19	-0.30	-0.40	-0.51
365	0.51	0.41	0.32	0.22	0.12	0.02	-0.08	-0.18	-0.28	-0.37	-0.47
370	0.47	0.38	0.29	0.20	0.11	0.02	-0.07	-0.16	-0.25	-0.34	-0.43
375	0.42	0.34	0.26	0.18	0.10	0.02	-0.07	-0.15	-0.23	-0.31	-0.39
380	0.38	0.30	0.23	0.16	0.09	0.01	-0.06	-0.13	-0.20	-0.28	-0.35
385	0.33	0.26	0.20	0.14	0.07	0.01	-0.05	-0.12	-0.18	-0.24	-0.30
390	0.27	0.22	0.17	0.12	0.06	0.01	-0.04	-0.10	-0.15	-0.20	-0.26
395	0.22	0.18	0.14	0.09	0.05	0.01	-0.04	-0.08	-0.12	-0.17	-0.21
400	0.17	0.14	0.10	0.07	0.04	0.00	-0.03	-0.06	-0.09	-0.13	-0.16
405	0.11	0.09	0.07	0.05	0.02	0.00	-0.02	-0.04	-0.06	-0.09	-0.11
410	0.06	0.05	0.03	0.02	0.01	0.00	-0.01	-0.02	-0.03	-0.04	-0.05
415	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
420	-0.05	-0.04	-0.03	-0.02	-0.01	0.00	0.01	0.02	0.03	0.04	0.05
425	-0.11	-0.09	-0.07	-0.04	-0.02	0.00	0.02	0.04	0.06	0.09	0.11
430	-0.17	-0.13	-0.10	-0.07	-0.03	0.00	0.03	0.06	0.10	0.13	0.16
435	-0.22	-0.18	-0.14	-0.09	-0.05	0.00	0.04	0.09	0.13	0.18	0.22
440	-0.28	-0.23	-0.17	-0.11	-0.06	0.00	0.05	0.11	0.17	0.22	0.28
445	-0.34	-0.27	-0.20	-0.14	-0.07	0.00	0.07	0.13	0.20	0.27	0.33
450	-0.40	-0.32	-0.24	-0.16	-0.08	0.00	0.08	0.16	0.23	0.31	0.39
455	-0.45	-0.36	-0.27	-0.18	-0.09	0.00	0.09	0.18	0.27	0.36	0.45
460	-0.51	-0.41	-0.31	-0.21	-0.10	0.00	0.10	0.20	0.31	0.41	0.51
465	-0.57	-0.46	-0.34	-0.23	-0.11	0.00	0.11	0.23	0.34	0.46	0.57
470	-0.63	-0.51	-0.38	-0.25	-0.13	0.00	0.13	0.25	0.38	0.51	0.63
475	-0.69	-0.55	-0.41	-0.28	-0.14	0.00	0.14	0.28	0.42	0.55	0.69
480	-0.75	-0.60	-0.45	-0.30	-0.15	0.00	0.15	0.30	0.45	0.60	0.75
485	-0.81	-0.65	-0.49	-0.32	-0.16	0.00	0.16	0.33	0.49	0.65	0.82
490	-0.87	-0.70	-0.52	-0.35	-0.17	0.00	0.18	0.35	0.53	0.70	0.88
495	-0.94	-0.75	-0.56	-0.37	-0.18	0.00	0.19	0.38	0.57	0.75	0.94
500	-1.00	-0.80	-0.60	-0.40	-0.20	0.00	0.20	0.40	0.61	0.81	1.01



\*\*\*\*\* MEMBER NO. 4 \*\*\*\*\*

	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9	1.0
100	1.43	1.07	0.73	0.43	0.15	-0.09	-0.30	-0.47	-0.62	-0.73	-0.81
105	1.31	0.96	0.65	0.37	0.12	-0.10	-0.28	-0.43	-0.56	-0.65	-0.70
110	1.17	0.85	0.57	0.31	0.09	-0.10	-0.26	-0.39	-0.48	-0.55	-0.58
115	1.04	0.75	0.49	0.26	0.06	-0.10	-0.24	-0.34	-0.41	-0.44	-0.45
120	0.90	0.64	0.41	0.20	0.04	-0.10	-0.21	-0.28	-0.32	-0.33	-0.31
125	0.77	0.53	0.33	0.15	0.01	-0.10	-0.17	-0.22	-0.23	-0.21	-0.16
130	0.63	0.42	0.25	0.10	-0.01	-0.09	-0.13	-0.15	-0.14	-0.09	-0.01
135	0.50	0.32	0.17	0.06	-0.03	-0.08	-0.09	-0.08	-0.04	0.04	0.15
140	0.36	0.21	0.10	0.01	-0.04	-0.06	-0.05	-0.01	0.06	0.17	0.31
145	0.23	0.11	0.03	-0.03	-0.06	-0.05	-0.01	0.06	0.16	0.30	0.47
150	0.11	0.02	-0.04	-0.07	-0.07	-0.03	0.04	0.13	0.27	0.43	0.62
155	-0.01	-0.08	-0.11	-0.11	-0.08	-0.02	0.08	0.21	0.36	0.55	0.78
160	-0.13	-0.16	-0.17	-0.15	-0.09	0.00	0.12	0.28	0.46	0.68	0.93
165	-0.24	-0.25	-0.23	-0.18	-0.10	0.02	0.17	0.34	0.55	0.80	1.07
170	-0.34	-0.33	-0.28	-0.21	-0.10	0.04	0.21	0.41	0.64	0.91	1.21
175	-0.43	-0.40	-0.33	-0.24	-0.11	0.05	0.25	0.47	0.73	1.01	1.33
180	-0.51	-0.46	-0.38	-0.26	-0.11	0.07	0.28	0.53	0.80	1.11	1.45
185	-0.59	-0.52	-0.41	-0.28	-0.11	0.08	0.31	0.57	0.87	1.19	1.55
190	-0.65	-0.57	-0.45	-0.30	-0.12	0.10	0.34	0.62	0.93	1.27	1.64
195	-0.70	-0.60	-0.47	-0.31	-0.12	0.11	0.36	0.65	0.97	1.33	1.71
200	-0.74	-0.63	-0.49	-0.32	-0.12	0.11	0.38	0.68	1.01	1.37	1.77
205	-0.77	-0.66	-0.51	-0.33	-0.12	0.12	0.39	0.69	1.03	1.40	1.80
210	-0.80	-0.68	-0.53	-0.35	-0.13	0.11	0.39	0.70	1.04	1.41	1.81
215	-0.81	-0.69	-0.54	-0.36	-0.15	0.10	0.38	0.69	1.03	1.40	1.81
220	-0.83	-0.71	-0.56	-0.38	-0.16	0.08	0.36	0.67	1.01	1.38	1.79
225	-0.84	-0.72	-0.57	-0.39	-0.18	0.06	0.34	0.64	0.98	1.35	1.75
230	-0.84	-0.73	-0.59	-0.41	-0.20	0.03	0.30	0.61	0.94	1.31	1.70
235	-0.84	-0.73	-0.60	-0.43	-0.23	0.00	0.27	0.56	0.89	1.25	1.64
240	-0.83	-0.74	-0.61	-0.45	-0.25	-0.03	0.23	0.51	0.83	1.19	1.57
245	-0.82	-0.74	-0.62	-0.47	-0.28	-0.07	0.18	0.46	0.77	1.11	1.49
250	-0.81	-0.73	-0.62	-0.48	-0.31	-0.11	0.13	0.40	0.70	1.03	1.40
255	-0.79	-0.73	-0.63	-0.50	-0.34	-0.14	0.08	0.34	0.63	0.95	1.30
260	-0.77	-0.72	-0.63	-0.52	-0.37	-0.18	0.03	0.27	0.55	0.86	1.20
265	-0.75	-0.71	-0.64	-0.53	-0.39	-0.22	-0.02	0.21	0.47	0.77	1.10
270	-0.72	-0.70	-0.64	-0.54	-0.42	-0.26	-0.08	0.14	0.39	0.68	0.99
275	-0.69	-0.68	-0.63	-0.55	-0.44	-0.30	-0.13	0.08	0.32	0.59	0.89
280	-0.66	-0.66	-0.63	-0.56	-0.46	-0.34	-0.18	0.02	0.24	0.50	0.79
285	-0.63	-0.64	-0.62	-0.57	-0.48	-0.37	-0.22	-0.04	0.17	0.41	0.69
290	-0.59	-0.62	-0.61	-0.57	-0.50	-0.40	-0.26	-0.10	0.10	0.33	0.59
295	-0.55	-0.59	-0.59	-0.57	-0.51	-0.42	-0.30	-0.15	0.04	0.25	0.50
300	-0.51	-0.56	-0.58	-0.56	-0.52	-0.44	-0.33	-0.19	-0.02	0.19	0.42
305	-0.47	-0.53	-0.56	-0.56	-0.52	-0.46	-0.36	-0.23	-0.07	0.12	0.35
310	-0.43	-0.50	-0.54	-0.55	-0.52	-0.47	-0.38	-0.26	-0.11	0.07	0.28
315	-0.38	-0.47	-0.52	-0.54	-0.52	-0.48	-0.40	-0.29	-0.15	0.02	0.22
320	-0.34	-0.43	-0.50	-0.52	-0.52	-0.49	-0.42	-0.32	-0.19	-0.03	0.17
325	-0.30	-0.40	-0.47	-0.51	-0.52	-0.49	-0.43	-0.34	-0.22	-0.07	0.12
330	-0.26	-0.37	-0.45	-0.49	-0.51	-0.49	-0.44	-0.36	-0.25	-0.11	0.07
335	-0.22	-0.33	-0.42	-0.48	-0.50	-0.49	-0.45	-0.38	-0.28	-0.14	0.03
340	-0.17	-0.30	-0.40	-0.46	-0.49	-0.49	-0.46	-0.39	-0.30	-0.17	-0.01
345	-0.13	-0.26	-0.37	-0.44	-0.48	-0.48	-0.46	-0.40	-0.32	-0.20	-0.04
350	-0.09	-0.23	-0.34	-0.42	-0.46	-0.48	-0.46	-0.41	-0.33	-0.22	-0.07
355	-0.04	-0.19	-0.31	-0.40	-0.45	-0.47	-0.46	-0.42	-0.35	-0.24	-0.10
360	0.00	-0.16	-0.28	-0.37	-0.43	-0.46	-0.46	-0.42	-0.36	-0.26	-0.13
365	0.05	-0.12	-0.25	-0.35	-0.42	-0.45	-0.45	-0.43	-0.37	-0.28	-0.15
370	0.09	-0.08	-0.22	-0.32	-0.40	-0.44	-0.45	-0.43	-0.38	-0.29	-0.17
375	0.14	-0.04	-0.18	-0.30	-0.38	-0.43	-0.44	-0.43	-0.38	-0.30	-0.19
380	0.18	0.00	-0.15	-0.27	-0.36	-0.41	-0.44	-0.43	-0.39	-0.32	-0.21
385	0.23	0.04	-0.12	-0.24	-0.34	-0.40	-0.43	-0.43	-0.40	-0.33	-0.23
390	0.28	0.08	-0.08	-0.22	-0.32	-0.39	-0.42	-0.43	-0.40	-0.34	-0.25
395	0.33	0.12	-0.05	-0.19	-0.29	-0.37	-0.41	-0.43	-0.41	-0.36	-0.27
400	0.38	0.17	-0.01	-0.16	-0.27	-0.36	-0.41	-0.43	-0.41	-0.37	-0.29

405	0.43	0.21	0.02	-0.13	-0.25	-0.34	-0.40	-0.42	-0.42	-0.38	-0.31
410	0.48	0.25	0.06	-0.10	-0.23	-0.33	-0.39	-0.42	-0.43	-0.40	-0.33
415	0.53	0.30	0.10	-0.07	-0.21	-0.31	-0.38	-0.43	-0.43	-0.41	-0.36
420	0.58	0.34	0.13	-0.04	-0.19	-0.30	-0.38	-0.43	-0.44	-0.43	-0.38
425	0.63	0.38	0.17	-0.01	-0.16	-0.28	-0.37	-0.43	-0.45	-0.44	-0.40
430	0.68	0.43	0.21	0.02	-0.14	-0.27	-0.37	-0.43	-0.46	-0.46	-0.43
435	0.74	0.47	0.24	0.04	-0.12	-0.26	-0.36	-0.43	-0.47	-0.48	-0.46
440	0.79	0.52	0.28	0.07	-0.10	-0.24	-0.36	-0.44	-0.48	-0.50	-0.48
445	0.84	0.56	0.32	0.10	-0.08	-0.23	-0.35	-0.44	-0.49	-0.52	-0.51
450	0.89	0.61	0.35	0.13	-0.06	-0.22	-0.35	-0.44	-0.51	-0.54	-0.54
455	0.95	0.65	0.39	0.16	-0.04	-0.21	-0.34	-0.45	-0.52	-0.56	-0.56
460	1.00	0.70	0.43	0.19	-0.02	-0.19	-0.34	-0.45	-0.53	-0.58	-0.59
465	1.06	0.74	0.47	0.22	0.00	-0.18	-0.33	-0.45	-0.54	-0.60	-0.62
470	1.11	0.79	0.50	0.25	0.02	-0.17	-0.33	-0.46	-0.55	-0.62	-0.65
475	1.16	0.84	0.54	0.28	0.04	-0.16	-0.32	-0.46	-0.56	-0.64	-0.68
480	1.22	0.88	0.58	0.31	0.07	-0.14	-0.32	-0.46	-0.58	-0.66	-0.71
485	1.27	0.93	0.62	0.34	0.09	-0.13	-0.31	-0.47	-0.59	-0.68	-0.74
490	1.33	0.98	0.65	0.37	0.11	-0.12	-0.31	-0.47	-0.60	-0.70	-0.76
495	1.38	1.02	0.69	0.40	0.13	-0.10	-0.30	-0.47	-0.61	-0.72	-0.79
500	1.44	1.07	0.73	0.43	0.15	-0.09	-0.30	-0.48	-0.62	-0.74	-0.82

\*\*\*\*\* MEMBER NO. 5 \*\*\*\*\*

	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9	1.0
100	-0.14	-0.22	-0.29	-0.37	-0.44	-0.52	-0.59	-0.67	-0.74	-0.82	-0.89
105	-0.14	-0.22	-0.29	-0.37	-0.44	-0.52	-0.59	-0.67	-0.75	-0.82	-0.90
110	-0.14	-0.22	-0.29	-0.37	-0.44	-0.52	-0.59	-0.67	-0.74	-0.82	-0.90
115	-0.14	-0.21	-0.29	-0.36	-0.44	-0.51	-0.59	-0.67	-0.74	-0.82	-0.89
120	-0.13	-0.21	-0.28	-0.36	-0.43	-0.51	-0.58	-0.66	-0.74	-0.81	-0.89
125	-0.12	-0.20	-0.27	-0.35	-0.42	-0.50	-0.58	-0.65	-0.73	-0.80	-0.88
130	-0.10	-0.18	-0.26	-0.33	-0.41	-0.49	-0.56	-0.64	-0.72	-0.79	-0.87
135	-0.08	-0.15	-0.23	-0.31	-0.39	-0.47	-0.55	-0.63	-0.70	-0.78	-0.86
140	-0.04	-0.12	-0.20	-0.28	-0.37	-0.45	-0.53	-0.61	-0.69	-0.77	-0.85
145	0.00	-0.08	-0.17	-0.25	-0.33	-0.42	-0.50	-0.59	-0.67	-0.75	-0.84
150	0.06	-0.03	-0.12	-0.21	-0.30	-0.38	-0.47	-0.56	-0.65	-0.74	-0.83
155	0.13	0.03	-0.06	-0.16	-0.25	-0.34	-0.44	-0.53	-0.63	-0.72	-0.82
160	0.21	0.11	0.01	-0.09	-0.20	-0.30	-0.40	-0.50	-0.60	-0.70	-0.81
165	0.31	0.20	0.09	-0.02	-0.13	-0.24	-0.35	-0.47	-0.58	-0.69	-0.80
170	0.43	0.30	0.18	0.06	-0.06	-0.18	-0.30	-0.43	-0.55	-0.67	-0.79
175	0.56	0.43	0.29	0.16	0.02	-0.11	-0.25	-0.38	-0.52	-0.65	-0.79
180	0.71	0.57	0.42	0.27	0.12	-0.03	-0.18	-0.33	-0.48	-0.63	-0.78
185	0.89	0.72	0.56	0.39	0.22	0.05	-0.11	-0.28	-0.45	-0.62	-0.78
190	1.09	0.90	0.71	0.53	0.34	0.15	-0.04	-0.22	-0.41	-0.60	-0.79
195	1.31	1.10	0.89	0.68	0.47	0.26	0.05	-0.16	-0.37	-0.58	-0.79
200	1.56	1.32	1.09	0.85	0.61	0.38	0.14	-0.09	-0.33	-0.57	-0.80
205	1.20	1.57	1.31	1.04	0.78	0.51	0.25	-0.02	-0.28	-0.55	-0.82
210	0.88	1.86	1.56	1.26	0.96	0.67	0.37	0.07	-0.23	-0.53	-0.83
215	0.60	1.54	1.84	1.51	1.17	0.84	0.50	0.17	-0.16	-0.50	-0.83
220	0.34	1.25	2.15	1.77	1.40	1.03	0.66	0.29	-0.08	-0.46	-0.83
225	0.12	0.98	1.84	2.07	1.66	1.24	0.83	0.42	0.01	-0.41	-0.82
230	-0.07	0.75	1.57	2.38	1.93	1.48	1.02	0.57	0.11	-0.34	-0.80
235	-0.24	0.54	1.31	2.09	2.23	1.73	1.23	0.73	0.23	-0.27	-0.76
240	-0.38	0.35	1.08	1.81	2.54	2.00	1.46	0.91	0.37	-0.17	-0.72
245	-0.49	0.19	0.87	1.56	2.24	2.29	1.70	1.11	0.52	-0.07	-0.65
250	-0.59	0.05	0.69	1.32	1.96	2.60	1.97	1.33	0.70	0.06	-0.57
255	-0.67	-0.07	0.52	1.11	1.70	2.30	2.25	1.57	0.89	0.21	-0.47
260	-0.73	-0.18	0.37	0.92	1.46	2.01	2.56	1.83	1.10	0.38	-0.35
265	-0.77	-0.27	0.24	0.74	1.24	1.74	2.25	2.11	1.34	0.57	-0.20
270	-0.80	-0.34	0.12	0.58	1.04	1.50	1.96	2.41	1.60	0.79	-0.03
275	-0.81	-0.40	0.02	0.44	0.85	1.27	1.69	2.10	1.88	1.03	0.17
280	-0.82	-0.44	-0.07	0.31	0.69	1.06	1.44	1.82	2.19	1.30	0.40
285	-0.82	-0.48	-0.14	0.20	0.54	0.88	1.22	1.56	1.90	1.60	0.66
290	-0.81	-0.51	-0.20	0.10	0.41	0.71	1.02	1.32	1.62	1.93	0.96
295	-0.80	-0.53	-0.25	0.02	0.29	0.56	0.84	1.11	1.38	1.65	1.29
300	-0.78	-0.54	-0.29	-0.05	0.19	0.44	0.68	0.93	1.17	1.41	1.66

305	-0.77	-0.55	-0.33	-0.11	0.11	0.33	0.55	0.76	0.98	1.20	1.42
310	-0.76	-0.56	-0.36	-0.17	0.03	0.23	0.42	0.62	0.82	1.02	1.21
315	-0.75	-0.57	-0.40	-0.22	-0.04	0.14	0.32	0.49	0.67	0.85	1.03
320	-0.75	-0.59	-0.43	-0.27	-0.10	0.06	0.22	0.38	0.54	0.70	0.86
325	-0.75	-0.60	-0.45	-0.31	-0.16	-0.01	0.13	0.28	0.43	0.58	0.72
330	-0.75	-0.62	-0.48	-0.35	-0.21	-0.08	0.06	0.20	0.33	0.47	0.60
335	-0.76	-0.63	-0.50	-0.38	-0.25	-0.13	0.00	0.12	0.25	0.37	0.50
340	-0.76	-0.64	-0.53	-0.41	-0.29	-0.18	-0.06	0.06	0.18	0.29	0.41
345	-0.77	-0.66	-0.55	-0.44	-0.33	-0.21	-0.10	0.01	0.12	0.23	0.34
350	-0.77	-0.67	-0.56	-0.46	-0.35	-0.25	-0.14	-0.04	0.07	0.17	0.28
355	-0.78	-0.68	-0.58	-0.48	-0.38	-0.28	-0.17	-0.07	0.03	0.13	0.23
360	-0.79	-0.69	-0.59	-0.49	-0.40	-0.30	-0.20	-0.10	0.00	0.09	0.19
365	-0.79	-0.70	-0.60	-0.51	-0.41	-0.31	-0.22	-0.12	-0.03	0.07	0.16
370	-0.80	-0.70	-0.61	-0.52	-0.42	-0.33	-0.23	-0.14	-0.05	0.05	0.14
375	-0.80	-0.71	-0.62	-0.52	-0.43	-0.34	-0.25	-0.15	-0.06	0.03	0.12
380	-0.80	-0.71	-0.62	-0.53	-0.44	-0.35	-0.25	-0.16	-0.07	0.02	0.11
385	-0.80	-0.71	-0.62	-0.53	-0.44	-0.35	-0.26	-0.17	-0.08	0.01	0.10
390	-0.79	-0.70	-0.62	-0.53	-0.44	-0.35	-0.27	-0.18	-0.09	0.00	0.08
395	-0.78	-0.70	-0.61	-0.53	-0.44	-0.36	-0.27	-0.19	-0.10	-0.01	0.07
400	-0.77	-0.69	-0.61	-0.52	-0.44	-0.36	-0.28	-0.19	-0.11	-0.03	0.05
405	-0.75	-0.68	-0.60	-0.52	-0.44	-0.36	-0.28	-0.20	-0.12	-0.04	0.03
410	-0.74	-0.66	-0.59	-0.51	-0.44	-0.36	-0.29	-0.22	-0.14	-0.07	0.01
415	-0.72	-0.65	-0.58	-0.51	-0.44	-0.37	-0.30	-0.23	-0.16	-0.09	-0.02
420	-0.69	-0.63	-0.57	-0.50	-0.44	-0.37	-0.31	-0.25	-0.18	-0.12	-0.06
425	-0.67	-0.61	-0.55	-0.50	-0.44	-0.38	-0.32	-0.27	-0.21	-0.15	-0.09
430	-0.64	-0.59	-0.54	-0.49	-0.44	-0.39	-0.34	-0.29	-0.24	-0.19	-0.13
435	-0.62	-0.57	-0.53	-0.48	-0.44	-0.40	-0.35	-0.31	-0.27	-0.22	-0.18
440	-0.59	-0.55	-0.51	-0.48	-0.44	-0.41	-0.37	-0.33	-0.30	-0.26	-0.23
445	-0.56	-0.53	-0.50	-0.47	-0.44	-0.42	-0.39	-0.36	-0.33	-0.30	-0.28
450	-0.52	-0.50	-0.48	-0.46	-0.44	-0.43	-0.41	-0.39	-0.37	-0.35	-0.33
455	-0.49	-0.48	-0.47	-0.46	-0.45	-0.44	-0.42	-0.41	-0.40	-0.39	-0.38
460	-0.45	-0.45	-0.45	-0.45	-0.45	-0.45	-0.44	-0.44	-0.44	-0.44	-0.44
465	-0.42	-0.42	-0.43	-0.44	-0.45	-0.46	-0.46	-0.47	-0.48	-0.49	-0.49
470	-0.38	-0.40	-0.41	-0.43	-0.45	-0.47	-0.48	-0.50	-0.52	-0.53	-0.55
475	-0.34	-0.37	-0.39	-0.42	-0.45	-0.47	-0.50	-0.53	-0.56	-0.58	-0.61
480	-0.30	-0.34	-0.37	-0.41	-0.45	-0.48	-0.52	-0.56	-0.59	-0.63	-0.67
485	-0.26	-0.31	-0.35	-0.40	-0.45	-0.49	-0.54	-0.59	-0.63	-0.68	-0.72
490	-0.22	-0.28	-0.33	-0.39	-0.44	-0.50	-0.56	-0.61	-0.67	-0.73	-0.78
495	-0.18	-0.24	-0.31	-0.38	-0.44	-0.51	-0.57	-0.64	-0.71	-0.77	-0.84
500	-0.14	-0.21	-0.29	-0.36	-0.44	-0.51	-0.59	-0.67	-0.74	-0.82	-0.89

\*\*\*\*\* MEMBER NO. 6 \*\*\*\*\*

	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9	1.0
100	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
105	-0.06	-0.05	-0.04	-0.03	-0.02	0.00	0.01	0.02	0.03	0.05	0.06
110	-0.13	-0.10	-0.08	-0.05	-0.03	-0.01	0.02	0.04	0.07	0.09	0.11
115	-0.18	-0.15	-0.11	-0.08	-0.04	-0.01	0.03	0.06	0.10	0.13	0.17
120	-0.24	-0.20	-0.15	-0.10	-0.06	-0.01	0.03	0.08	0.13	0.17	0.22
125	-0.30	-0.24	-0.18	-0.13	-0.07	-0.01	0.04	0.10	0.16	0.21	0.27
130	-0.35	-0.29	-0.22	-0.15	-0.08	-0.02	0.05	0.12	0.18	0.25	0.32
135	-0.40	-0.33	-0.25	-0.17	-0.10	-0.02	0.06	0.14	0.21	0.29	0.37
140	-0.45	-0.37	-0.28	-0.19	-0.11	-0.02	0.07	0.15	0.24	0.33	0.41
145	-0.50	-0.41	-0.31	-0.21	-0.12	-0.02	0.07	0.17	0.26	0.36	0.46
150	-0.55	-0.44	-0.34	-0.23	-0.13	-0.02	0.08	0.19	0.29	0.39	0.50
155	-0.59	-0.48	-0.36	-0.25	-0.14	-0.02	0.09	0.20	0.31	0.43	0.54
160	-0.63	-0.51	-0.39	-0.27	-0.15	-0.02	0.10	0.22	0.34	0.46	0.58
165	-0.67	-0.54	-0.41	-0.28	-0.15	-0.02	0.10	0.23	0.36	0.49	0.62
170	-0.70	-0.57	-0.43	-0.29	-0.16	-0.02	0.11	0.25	0.38	0.52	0.66
175	-0.73	-0.59	-0.45	-0.31	-0.16	-0.02	0.12	0.26	0.41	0.55	0.69
180	-0.76	-0.62	-0.47	-0.32	-0.17	-0.02	0.13	0.28	0.43	0.58	0.73
185	-0.79	-0.64	-0.48	-0.33	-0.17	-0.02	0.14	0.30	0.45	0.61	0.76
190	-0.82	-0.66	-0.49	-0.33	-0.17	-0.01	0.15	0.31	0.47	0.63	0.79
195	-0.84	-0.67	-0.50	-0.34	-0.17	-0.01	0.16	0.33	0.49	0.66	0.83
200	-0.86	-0.69	-0.51	-0.34	-0.17	0.00	0.17	0.34	0.52	0.69	0.86

205	-0.87	-0.69	-0.52	-0.34	-0.17	0.01	0.18	0.36	0.54	0.71	0.89
210	-0.88	-0.70	-0.52	-0.34	-0.16	0.02	0.20	0.37	0.55	0.73	0.91
215	-0.87	-0.69	-0.51	-0.33	-0.15	0.03	0.21	0.39	0.57	0.75	0.93
220	-0.86	-0.68	-0.50	-0.32	-0.14	0.04	0.22	0.40	0.58	0.76	0.94
225	-0.85	-0.67	-0.49	-0.31	-0.13	0.05	0.23	0.40	0.58	0.76	0.94
230	-0.83	-0.65	-0.47	-0.30	-0.12	0.06	0.23	0.41	0.59	0.76	0.94
235	-0.80	-0.62	-0.45	-0.28	-0.11	0.07	0.24	0.41	0.58	0.76	0.93
240	-0.76	-0.60	-0.43	-0.26	-0.09	0.07	0.24	0.41	0.58	0.74	0.91
245	-0.72	-0.56	-0.40	-0.24	-0.08	0.08	0.24	0.40	0.56	0.72	0.88
250	-0.68	-0.52	-0.37	-0.22	-0.07	0.09	0.24	0.39	0.55	0.70	0.85
255	-0.63	-0.48	-0.34	-0.20	-0.05	0.09	0.23	0.38	0.52	0.67	0.81
260	-0.57	-0.44	-0.31	-0.17	-0.04	0.09	0.23	0.36	0.49	0.63	0.76
265	-0.51	-0.39	-0.27	-0.15	-0.03	0.09	0.21	0.34	0.46	0.58	0.70
270	-0.45	-0.34	-0.23	-0.13	-0.02	0.09	0.20	0.31	0.41	0.52	0.63
275	-0.38	-0.29	-0.20	-0.10	-0.01	0.08	0.18	0.27	0.36	0.46	0.55
280	-0.31	-0.23	-0.16	-0.08	0.00	0.08	0.15	0.23	0.31	0.38	0.46
285	-0.24	-0.18	-0.12	-0.06	0.00	0.06	0.12	0.18	0.24	0.30	0.36
290	-0.16	-0.12	-0.08	-0.04	0.00	0.05	0.09	0.13	0.17	0.21	0.25
295	-0.08	-0.06	-0.04	-0.02	0.00	0.03	0.05	0.07	0.09	0.11	0.13
300	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
305	0.08	0.06	0.04	0.02	0.00	-0.03	-0.05	-0.07	-0.09	-0.11	-0.13
310	0.16	0.12	0.08	0.04	0.00	-0.05	-0.09	-0.13	-0.17	-0.21	-0.25
315	0.24	0.18	0.12	0.06	0.00	-0.06	-0.12	-0.18	-0.24	-0.30	-0.36
320	0.31	0.23	0.16	0.08	0.00	-0.08	-0.15	-0.23	-0.31	-0.38	-0.46
325	0.38	0.29	0.20	0.10	0.01	-0.08	-0.18	-0.27	-0.36	-0.46	-0.55
330	0.45	0.34	0.23	0.13	0.02	-0.09	-0.20	-0.31	-0.41	-0.52	-0.63
335	0.51	0.39	0.27	0.15	0.03	-0.09	-0.21	-0.34	-0.46	-0.58	-0.70
340	0.57	0.44	0.31	0.17	0.04	-0.09	-0.23	-0.36	-0.49	-0.63	-0.76
345	0.63	0.48	0.34	0.20	0.05	-0.09	-0.23	-0.38	-0.52	-0.67	-0.81
350	0.68	0.52	0.37	0.22	0.07	-0.09	-0.24	-0.39	-0.55	-0.70	-0.85
355	0.72	0.56	0.40	0.24	0.08	-0.08	-0.24	-0.40	-0.56	-0.72	-0.88
360	0.76	0.60	0.43	0.26	0.09	-0.07	-0.24	-0.41	-0.58	-0.74	-0.91
365	0.80	0.62	0.45	0.28	0.11	-0.07	-0.24	-0.41	-0.58	-0.76	-0.93
370	0.83	0.65	0.47	0.30	0.12	-0.06	-0.23	-0.41	-0.59	-0.76	-0.94
375	0.85	0.67	0.49	0.31	0.13	-0.05	-0.23	-0.40	-0.58	-0.76	-0.94
380	0.86	0.68	0.50	0.32	0.14	-0.04	-0.22	-0.40	-0.58	-0.76	-0.94
385	0.87	0.69	0.51	0.33	0.15	-0.03	-0.21	-0.39	-0.57	-0.75	-0.93
390	0.88	0.70	0.52	0.34	0.16	-0.02	-0.20	-0.37	-0.55	-0.73	-0.91
395	0.87	0.69	0.52	0.34	0.17	-0.01	-0.18	-0.36	-0.54	-0.71	-0.89
400	0.86	0.69	0.51	0.34	0.17	0.00	-0.17	-0.34	-0.52	-0.69	-0.86
405	0.84	0.67	0.50	0.34	0.17	0.01	-0.16	-0.33	-0.49	-0.66	-0.83
410	0.82	0.66	0.49	0.33	0.17	0.01	-0.15	-0.31	-0.47	-0.63	-0.79
415	0.79	0.64	0.48	0.33	0.17	0.02	-0.14	-0.30	-0.45	-0.61	-0.76
420	0.76	0.62	0.47	0.32	0.17	0.02	-0.13	-0.28	-0.43	-0.58	-0.73
425	0.73	0.59	0.45	0.31	0.16	0.02	-0.12	-0.26	-0.41	-0.55	-0.69
430	0.70	0.57	0.43	0.29	0.16	0.02	-0.11	-0.25	-0.38	-0.52	-0.66
435	0.67	0.54	0.41	0.28	0.15	0.02	-0.10	-0.23	-0.36	-0.49	-0.62
440	0.63	0.51	0.39	0.27	0.15	0.02	-0.10	-0.22	-0.34	-0.46	-0.58
445	0.59	0.48	0.36	0.25	0.14	0.02	-0.09	-0.20	-0.31	-0.43	-0.54
450	0.55	0.44	0.34	0.23	0.13	0.02	-0.08	-0.19	-0.29	-0.39	-0.50
455	0.50	0.41	0.31	0.21	0.12	0.02	-0.07	-0.17	-0.26	-0.36	-0.46
460	0.45	0.37	0.28	0.19	0.11	0.02	-0.07	-0.15	-0.24	-0.33	-0.41
465	0.40	0.33	0.25	0.17	0.10	0.02	-0.06	-0.14	-0.21	-0.29	-0.37
470	0.35	0.29	0.22	0.15	0.08	0.02	-0.05	-0.12	-0.18	-0.25	-0.32
475	0.30	0.24	0.18	0.13	0.07	0.01	-0.04	-0.10	-0.16	-0.21	-0.27
480	0.24	0.20	0.15	0.10	0.06	0.01	-0.03	-0.08	-0.13	-0.17	-0.22
485	0.18	0.15	0.11	0.08	0.04	0.01	-0.03	-0.06	-0.10	-0.13	-0.17
490	0.13	0.10	0.08	0.05	0.03	0.01	-0.02	-0.04	-0.07	-0.09	-0.11
495	0.06	0.05	0.04	0.03	0.02	0.00	-0.01	-0.02	-0.03	-0.05	-0.06
500	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

\*\*\*\*\* MEMBER NO. 7 \*\*\*\*\*

	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9	1.0
100	0.18	-0.04	-0.24	-0.40	-0.53	-0.63	-0.70	-0.74	-0.74	-0.71	-0.66

105	0.30	0.06	-0.15	-0.33	-0.48	-0.59	-0.68	-0.73	-0.75	-0.74	-0.69
110	0.43	0.17	-0.06	-0.25	-0.42	-0.55	-0.65	-0.71	-0.75	-0.75	-0.73
115	0.55	0.28	0.04	-0.17	-0.35	-0.50	-0.61	-0.70	-0.75	-0.77	-0.76
120	0.68	0.39	0.14	-0.09	-0.29	-0.45	-0.58	-0.68	-0.75	-0.78	-0.79
125	0.81	0.51	0.23	-0.01	-0.22	-0.40	-0.54	-0.66	-0.74	-0.79	-0.81
130	0.94	0.62	0.33	0.07	-0.15	-0.34	-0.51	-0.64	-0.73	-0.80	-0.84
135	1.07	0.73	0.43	0.16	-0.08	-0.29	-0.47	-0.61	-0.72	-0.81	-0.85
140	1.19	0.84	0.52	0.24	-0.02	-0.24	-0.43	-0.58	-0.71	-0.81	-0.87
145	1.31	0.94	0.62	0.32	0.05	-0.18	-0.39	-0.56	-0.70	-0.80	-0.88
150	1.42	1.04	0.70	0.39	0.12	-0.13	-0.34	-0.53	-0.68	-0.79	-0.88
155	1.52	1.14	0.78	0.47	0.18	-0.08	-0.30	-0.49	-0.65	-0.78	-0.88
160	1.61	1.22	0.86	0.53	0.24	-0.03	-0.26	-0.46	-0.63	-0.77	-0.87
165	1.69	1.30	0.93	0.59	0.29	0.02	-0.22	-0.43	-0.60	-0.75	-0.86
170	1.77	1.36	0.99	0.65	0.34	0.07	-0.18	-0.39	-0.57	-0.72	-0.84
175	1.82	1.42	1.04	0.70	0.39	0.11	-0.14	-0.35	-0.54	-0.69	-0.81
180	1.86	1.46	1.08	0.74	0.43	0.15	-0.10	-0.32	-0.50	-0.65	-0.77
185	1.89	1.49	1.11	0.77	0.46	0.18	-0.06	-0.28	-0.46	-0.61	-0.73
190	1.90	1.50	1.13	0.79	0.49	0.21	-0.03	-0.24	-0.42	-0.57	-0.68
195	1.89	1.50	1.13	0.80	0.50	0.24	0.00	-0.20	-0.37	-0.51	-0.62
200	1.86	1.48	1.12	0.80	0.51	0.26	0.03	-0.16	-0.32	-0.45	-0.55
205	1.81	1.44	1.10	0.79	0.52	0.27	0.06	-0.12	-0.27	-0.38	-0.47
210	1.74	1.39	1.06	0.77	0.51	0.29	0.09	-0.07	-0.20	-0.30	-0.37
215	1.65	1.32	1.02	0.75	0.51	0.30	0.12	-0.02	-0.13	-0.21	-0.26
220	1.56	1.24	0.96	0.71	0.50	0.31	0.16	0.04	-0.05	-0.11	-0.14
225	1.44	1.16	0.90	0.68	0.48	0.32	0.19	0.10	0.03	0.00	0.00
230	1.32	1.06	0.83	0.63	0.47	0.33	0.23	0.16	0.12	0.11	0.14
235	1.19	0.96	0.76	0.59	0.45	0.34	0.27	0.22	0.21	0.23	0.29
240	1.05	0.85	0.68	0.53	0.43	0.35	0.30	0.29	0.31	0.36	0.44
245	0.91	0.73	0.59	0.48	0.40	0.35	0.34	0.35	0.40	0.48	0.59
250	0.76	0.62	0.51	0.42	0.37	0.36	0.37	0.42	0.49	0.60	0.75
255	0.62	0.50	0.42	0.37	0.35	0.36	0.40	0.48	0.59	0.73	0.90
260	0.47	0.38	0.33	0.31	0.32	0.36	0.43	0.54	0.68	0.85	1.05
265	0.33	0.27	0.24	0.25	0.29	0.36	0.46	0.60	0.76	0.96	1.19
270	0.19	0.16	0.16	0.19	0.26	0.36	0.49	0.65	0.84	1.07	1.33
275	0.05	0.05	0.08	0.14	0.23	0.36	0.51	0.70	0.92	1.17	1.45
280	-0.07	-0.05	0.00	0.09	0.20	0.35	0.53	0.74	0.99	1.26	1.57
285	-0.19	-0.14	-0.07	0.04	0.17	0.34	0.55	0.78	1.04	1.34	1.67
290	-0.29	-0.23	-0.14	-0.01	0.15	0.34	0.56	0.81	1.09	1.41	1.76
295	-0.38	-0.30	-0.19	-0.05	0.12	0.33	0.56	0.83	1.13	1.46	1.83
300	-0.45	-0.36	-0.24	-0.09	0.10	0.31	0.56	0.84	1.16	1.50	1.88
305	-0.51	-0.42	-0.28	-0.12	0.07	0.30	0.56	0.85	1.17	1.52	1.91
310	-0.57	-0.46	-0.32	-0.16	0.05	0.28	0.54	0.84	1.17	1.53	1.92
315	-0.61	-0.50	-0.36	-0.19	0.02	0.25	0.52	0.82	1.15	1.51	1.91
320	-0.64	-0.54	-0.39	-0.22	-0.02	0.22	0.49	0.79	1.12	1.48	1.88
325	-0.67	-0.56	-0.42	-0.25	-0.05	0.18	0.45	0.75	1.08	1.44	1.83
330	-0.69	-0.59	-0.45	-0.29	-0.09	0.14	0.41	0.70	1.03	1.39	1.77
335	-0.70	-0.61	-0.48	-0.32	-0.12	0.10	0.36	0.65	0.97	1.32	1.70
340	-0.71	-0.62	-0.50	-0.35	-0.16	0.06	0.30	0.59	0.90	1.24	1.62
345	-0.71	-0.63	-0.52	-0.38	-0.20	0.01	0.25	0.52	0.82	1.16	1.52
350	-0.71	-0.64	-0.54	-0.40	-0.24	-0.04	0.19	0.45	0.74	1.07	1.42
355	-0.70	-0.64	-0.55	-0.43	-0.27	-0.09	0.13	0.38	0.66	0.97	1.31
360	-0.68	-0.64	-0.56	-0.45	-0.31	-0.14	0.07	0.30	0.57	0.87	1.20
365	-0.67	-0.63	-0.57	-0.47	-0.35	-0.19	0.00	0.23	0.48	0.77	1.08
370	-0.64	-0.63	-0.58	-0.49	-0.38	-0.24	-0.06	0.15	0.39	0.66	0.97
375	-0.62	-0.61	-0.58	-0.51	-0.41	-0.28	-0.12	0.07	0.30	0.56	0.85
380	-0.59	-0.60	-0.58	-0.53	-0.44	-0.33	-0.18	0.00	0.21	0.45	0.73
385	-0.56	-0.59	-0.58	-0.54	-0.47	-0.37	-0.24	-0.07	0.13	0.35	0.61
390	-0.53	-0.57	-0.58	-0.55	-0.50	-0.41	-0.29	-0.14	0.04	0.26	0.50
395	-0.49	-0.55	-0.57	-0.56	-0.52	-0.44	-0.34	-0.20	-0.03	0.17	0.40
400	-0.46	-0.53	-0.56	-0.56	-0.54	-0.47	-0.38	-0.26	-0.10	0.09	0.31
405	-0.43	-0.50	-0.55	-0.57	-0.55	-0.50	-0.42	-0.31	-0.17	0.01	0.22
410	-0.39	-0.48	-0.54	-0.57	-0.56	-0.53	-0.46	-0.36	-0.22	-0.06	0.14
415	-0.36	-0.46	-0.53	-0.57	-0.57	-0.55	-0.49	-0.40	-0.28	-0.12	0.06
420	-0.33	-0.44	-0.52	-0.57	-0.58	-0.57	-0.52	-0.44	-0.33	-0.18	-0.01
425	-0.29	-0.42	-0.51	-0.56	-0.59	-0.58	-0.54	-0.48	-0.37	-0.24	-0.08
430	-0.26	-0.39	-0.49	-0.56	-0.59	-0.60	-0.57	-0.51	-0.42	-0.29	-0.14

435	-0.23	-0.37	-0.48	-0.55	-0.60	-0.61	-0.59	-0.54	-0.45	-0.34	-0.19
440	-0.20	-0.35	-0.46	-0.55	-0.60	-0.62	-0.61	-0.56	-0.49	-0.38	-0.24
445	-0.17	-0.33	-0.45	-0.54	-0.60	-0.63	-0.62	-0.59	-0.52	-0.42	-0.29
450	-0.14	-0.30	-0.43	-0.53	-0.60	-0.64	-0.64	-0.61	-0.55	-0.46	-0.34
455	-0.11	-0.28	-0.42	-0.52	-0.60	-0.64	-0.65	-0.63	-0.58	-0.49	-0.38
460	-0.08	-0.26	-0.40	-0.51	-0.60	-0.64	-0.66	-0.65	-0.60	-0.52	-0.41
465	-0.05	-0.23	-0.38	-0.50	-0.59	-0.65	-0.67	-0.66	-0.62	-0.55	-0.45
470	-0.02	-0.21	-0.37	-0.49	-0.59	-0.65	-0.68	-0.68	-0.64	-0.58	-0.48
475	0.01	-0.18	-0.35	-0.48	-0.58	-0.65	-0.69	-0.69	-0.66	-0.61	-0.51
480	0.04	-0.16	-0.33	-0.47	-0.57	-0.65	-0.69	-0.70	-0.68	-0.63	-0.54
485	0.08	-0.13	-0.31	-0.45	-0.57	-0.65	-0.70	-0.71	-0.70	-0.65	-0.57
490	0.11	-0.10	-0.29	-0.44	-0.56	-0.64	-0.70	-0.72	-0.71	-0.67	-0.60
495	0.14	-0.08	-0.27	-0.42	-0.55	-0.64	-0.70	-0.73	-0.73	-0.69	-0.63
500	0.18	-0.05	-0.24	-0.41	-0.54	-0.64	-0.70	-0.74	-0.74	-0.72	-0.66











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MEMBER NO. 4

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	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9	1.0	A.F.
100	-0.30	-0.28	-0.25	-0.23	-0.20	-0.18	-0.15	-0.13	-0.10	-0.08	-0.05	-0.22
105	-0.28	-0.26	-0.23	-0.21	-0.18	-0.16	-0.13	-0.11	-0.08	-0.06	-0.03	-0.19
110	-0.26	-0.24	-0.21	-0.19	-0.16	-0.14	-0.11	-0.09	-0.06	-0.04	-0.01	-0.16
115	-0.24	-0.22	-0.19	-0.17	-0.14	-0.12	-0.09	-0.07	-0.04	-0.02	0.01	-0.13
120	-0.22	-0.20	-0.17	-0.15	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	-0.10
125	-0.20	-0.17	-0.15	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	-0.08
130	-0.18	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	-0.05
135	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	-0.03
140	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	0.12	-0.01
145	-0.11	-0.08	-0.06	-0.03	-0.01	0.02	0.04	0.07	0.09	0.12	0.14	0.01
150	-0.08	-0.06	-0.03	-0.01	0.02	0.04	0.07	0.09	0.12	0.14	0.17	0.02
155	-0.06	-0.04	-0.01	0.01	0.04	0.06	0.09	0.11	0.14	0.16	0.19	0.04
160	-0.04	-0.02	0.01	0.03	0.06	0.08	0.11	0.13	0.16	0.18	0.21	0.06
165	-0.02	0.00	0.03	0.05	0.08	0.10	0.13	0.15	0.18	0.20	0.23	0.07
170	0.00	0.02	0.05	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.08
175	0.01	0.04	0.06	0.09	0.11	0.14	0.16	0.19	0.21	0.24	0.26	0.09
180	0.03	0.05	0.08	0.10	0.13	0.15	0.18	0.20	0.23	0.25	0.28	0.10
185	0.04	0.07	0.09	0.12	0.14	0.17	0.19	0.22	0.24	0.27	0.29	0.11
190	0.05	0.08	0.10	0.13	0.15	0.18	0.20	0.23	0.25	0.28	0.30	0.11
195	0.06	0.09	0.11	0.14	0.16	0.19	0.21	0.24	0.26	0.29	0.31	0.12
200	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.30	0.32	0.12
205	0.08	0.10	0.13	0.15	0.18	0.20	0.23	0.25	0.28	0.30	0.33	0.12
210	0.08	0.11	0.13	0.16	0.18	0.21	0.23	0.26	0.28	0.31	0.33	0.12
215	0.08	0.11	0.13	0.16	0.18	0.21	0.23	0.26	0.28	0.31	0.33	0.12
220	0.08	0.11	0.13	0.16	0.18	0.21	0.23	0.26	0.28	0.31	0.33	0.13
225	0.08	0.10	0.13	0.15	0.18	0.20	0.23	0.25	0.28	0.30	0.33	0.13
230	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.30	0.32	0.13
235	0.07	0.09	0.12	0.14	0.17	0.19	0.22	0.24	0.27	0.29	0.32	0.13
240	0.06	0.09	0.11	0.14	0.16	0.19	0.21	0.24	0.26	0.29	0.31	0.12
245	0.06	0.08	0.11	0.13	0.16	0.18	0.21	0.23	0.26	0.28	0.31	0.12
250	0.05	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.30	0.12
255	0.04	0.06	0.09	0.11	0.14	0.16	0.19	0.21	0.24	0.26	0.29	0.12
260	0.03	0.06	0.08	0.11	0.13	0.16	0.18	0.21	0.23	0.26	0.28	0.12
265	0.02	0.05	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.11
270	0.01	0.03	0.06	0.08	0.11	0.13	0.16	0.18	0.21	0.23	0.26	0.11
275	0.00	0.02	0.05	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.11
280	-0.01	0.01	0.04	0.06	0.09	0.11	0.14	0.16	0.19	0.21	0.24	0.10
285	-0.02	0.00	0.03	0.05	0.08	0.10	0.13	0.15	0.18	0.20	0.23	0.10
290	-0.03	-0.01	0.02	0.04	0.07	0.09	0.12	0.14	0.17	0.19	0.22	0.09
295	-0.04	-0.02	0.01	0.03	0.06	0.08	0.11	0.13	0.16	0.18	0.21	0.09
300	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	0.12	0.15	0.17	0.20	0.08
305	-0.06	-0.04	-0.01	0.01	0.04	0.06	0.09	0.11	0.14	0.16	0.19	0.08
310	-0.07	-0.04	-0.02	0.01	0.03	0.06	0.08	0.11	0.13	0.16	0.18	0.07
315	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	0.12	0.15	0.17	0.07
320	-0.09	-0.06	-0.04	-0.01	0.01	0.04	0.06	0.09	0.11	0.14	0.16	0.06
325	-0.09	-0.07	-0.04	-0.02	0.01	0.03	0.06	0.08	0.11	0.13	0.16	0.05
330	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.08	0.10	0.13	0.15	0.05
335	-0.11	-0.08	-0.06	-0.03	-0.01	0.02	0.04	0.07	0.09	0.12	0.14	0.04
340	-0.11	-0.09	-0.06	-0.04	-0.01	0.01	0.04	0.06	0.09	0.11	0.14	0.03
345	-0.12	-0.09	-0.07	-0.04	-0.02	0.01	0.03	0.06	0.08	0.11	0.13	0.03
350	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.08	0.10	0.13	0.02
355	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	0.12	0.01
360	-0.14	-0.11	-0.09	-0.06	-0.04	-0.01	0.01	0.04	0.06	0.09	0.11	0.01
365	-0.14	-0.12	-0.09	-0.07	-0.04	-0.02	0.01	0.03	0.06	0.08	0.11	0.00
370	-0.15	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.08	0.10	-0.01
375	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	-0.01
380	-0.16	-0.13	-0.11	-0.08	-0.06	-0.03	-0.01	0.02	0.04	0.07	0.09	-0.02
385	-0.16	-0.14	-0.11	-0.09	-0.06	-0.04	-0.01	0.01	0.04	0.06	0.09	-0.03
390	-0.17	-0.14	-0.12	-0.09	-0.07	-0.04	-0.02	0.01	0.03	0.06	0.08	-0.04
395	-0.17	-0.15	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.08	-0.05
400	-0.18	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	-0.05







105	-0.20	-0.18	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	-0.34
110	-0.22	-0.19	-0.17	-0.14	-0.12	-0.09	-0.07	-0.04	-0.02	0.01	0.03	-0.32
115	-0.23	-0.20	-0.18	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	-0.29
120	-0.24	-0.22	-0.19	-0.17	-0.14	-0.12	-0.09	-0.07	-0.04	-0.02	0.01	-0.26
125	-0.25	-0.23	-0.20	-0.18	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	-0.24
130	-0.26	-0.24	-0.21	-0.19	-0.16	-0.14	-0.11	-0.09	-0.06	-0.04	-0.01	-0.21
135	-0.28	-0.25	-0.23	-0.20	-0.18	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	-0.19
140	-0.29	-0.26	-0.24	-0.21	-0.19	-0.16	-0.14	-0.11	-0.09	-0.06	-0.04	-0.16
145	-0.30	-0.27	-0.25	-0.22	-0.20	-0.17	-0.15	-0.12	-0.10	-0.07	-0.05	-0.14
150	-0.31	-0.28	-0.26	-0.23	-0.21	-0.18	-0.16	-0.13	-0.11	-0.08	-0.06	-0.11
155	-0.31	-0.29	-0.26	-0.24	-0.21	-0.19	-0.16	-0.14	-0.11	-0.09	-0.06	-0.09
160	-0.32	-0.30	-0.27	-0.25	-0.22	-0.20	-0.17	-0.15	-0.12	-0.10	-0.07	-0.07
165	-0.33	-0.30	-0.28	-0.25	-0.23	-0.20	-0.18	-0.15	-0.13	-0.10	-0.08	-0.04
170	-0.33	-0.30	-0.28	-0.25	-0.23	-0.20	-0.18	-0.15	-0.13	-0.10	-0.08	-0.02
175	-0.33	-0.31	-0.28	-0.26	-0.23	-0.21	-0.18	-0.16	-0.13	-0.11	-0.08	0.00
180	-0.33	-0.31	-0.28	-0.26	-0.23	-0.21	-0.18	-0.16	-0.13	-0.11	-0.08	0.02
185	-0.33	-0.31	-0.28	-0.26	-0.23	-0.21	-0.18	-0.16	-0.13	-0.11	-0.08	0.04
190	-0.33	-0.30	-0.28	-0.25	-0.23	-0.20	-0.18	-0.15	-0.13	-0.10	-0.08	0.06
195	-0.32	-0.30	-0.27	-0.25	-0.22	-0.20	-0.17	-0.15	-0.12	-0.10	-0.07	0.08
200	-0.31	-0.29	-0.26	-0.24	-0.21	-0.19	-0.16	-0.14	-0.11	-0.09	-0.06	0.10
205	-0.30	-0.28	-0.25	-0.23	-0.20	-0.18	-0.15	-0.13	-0.10	-0.08	-0.05	0.12
210	-0.29	-0.27	-0.24	-0.22	-0.19	-0.17	-0.14	-0.12	-0.09	-0.07	-0.04	0.14
215	-0.28	-0.25	-0.23	-0.20	-0.18	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	0.16
220	-0.26	-0.23	-0.21	-0.18	-0.16	-0.13	-0.11	-0.08	-0.06	-0.03	-0.01	0.17
225	-0.24	-0.21	-0.19	-0.16	-0.14	-0.11	-0.09	-0.06	-0.04	-0.01	0.01	0.19
230	-0.22	-0.19	-0.17	-0.14	-0.12	-0.09	-0.07	-0.04	-0.02	0.01	0.03	0.20
235	-0.20	-0.17	-0.15	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.21
240	-0.17	-0.15	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.08	0.22
245	-0.15	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.08	0.10	0.23
250	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	0.12	0.23
255	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	0.12	0.15	0.24
260	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	0.12	0.15	0.17	0.24
265	-0.06	-0.03	-0.01	0.02	0.04	0.07	0.09	0.12	0.14	0.17	0.19	0.24
270	-0.04	-0.01	0.01	0.04	0.06	0.09	0.11	0.14	0.16	0.19	0.21	0.24
275	-0.02	0.01	0.03	0.06	0.08	0.11	0.13	0.16	0.18	0.21	0.23	0.24
280	0.00	0.03	0.05	0.08	0.10	0.13	0.15	0.18	0.20	0.23	0.25	0.24
285	0.02	0.05	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.24
290	0.04	0.06	0.09	0.11	0.14	0.16	0.19	0.21	0.24	0.26	0.29	0.23
295	0.05	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.30	0.23
300	0.06	0.08	0.11	0.13	0.16	0.18	0.21	0.23	0.26	0.28	0.31	0.22
305	0.07	0.09	0.12	0.14	0.17	0.19	0.22	0.24	0.27	0.29	0.32	0.21
310	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.30	0.32	0.20
315	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.30	0.32	0.19
320	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.30	0.32	0.18
325	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.30	0.32	0.17
330	0.07	0.09	0.12	0.14	0.17	0.19	0.22	0.24	0.27	0.29	0.32	0.16
335	0.06	0.09	0.11	0.14	0.16	0.19	0.21	0.24	0.26	0.29	0.31	0.15
340	0.06	0.08	0.11	0.13	0.16	0.18	0.21	0.23	0.26	0.28	0.31	0.14
345	0.05	0.08	0.10	0.13	0.15	0.18	0.20	0.23	0.25	0.28	0.30	0.13
350	0.04	0.07	0.09	0.12	0.14	0.17	0.19	0.22	0.24	0.27	0.29	0.11
355	0.03	0.06	0.08	0.11	0.13	0.16	0.18	0.21	0.23	0.26	0.28	0.10
360	0.02	0.05	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.09
365	0.01	0.04	0.06	0.09	0.11	0.14	0.16	0.19	0.21	0.24	0.26	0.08
370	0.00	0.03	0.05	0.08	0.10	0.13	0.15	0.18	0.20	0.23	0.25	0.06
375	-0.01	0.02	0.04	0.07	0.09	0.12	0.14	0.17	0.19	0.22	0.24	0.05
380	-0.02	0.00	0.03	0.05	0.08	0.10	0.13	0.15	0.18	0.20	0.23	0.03
385	-0.03	-0.01	0.02	0.04	0.07	0.09	0.12	0.14	0.17	0.19	0.22	0.02
390	-0.04	-0.02	0.01	0.03	0.06	0.08	0.11	0.13	0.16	0.18	0.21	0.00
395	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	0.12	0.15	0.17	0.20	-0.01
400	-0.06	-0.04	-0.01	0.01	0.04	0.06	0.09	0.11	0.14	0.16	0.19	-0.03
405	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.08	0.10	0.13	0.15	0.18	-0.04
410	-0.08	-0.06	-0.03	-0.01	0.02	0.04	0.07	0.09	0.12	0.14	0.17	-0.06
415	-0.09	-0.07	-0.04	-0.02	0.01	0.03	0.06	0.08	0.11	0.13	0.16	-0.08
420	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	0.12	0.15	-0.09
425	-0.11	-0.08	-0.06	-0.03	-0.01	0.02	0.04	0.07	0.09	0.12	0.14	-0.11
430	-0.11	-0.09	-0.06	-0.04	-0.01	0.01	0.04	0.06	0.09	0.11	0.14	-0.13

435	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.08	0.10	0.13	-0.14
440	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	0.12	-0.16
445	-0.13	-0.11	-0.08	-0.06	-0.03	-0.01	0.02	0.04	0.07	0.09	0.12	-0.18
450	-0.14	-0.12	-0.09	-0.07	-0.04	-0.02	0.01	0.03	0.06	0.08	0.11	-0.19
455	-0.15	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.08	0.10	-0.21
460	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	-0.23
465	-0.16	-0.13	-0.11	-0.08	-0.06	-0.03	-0.01	0.02	0.04	0.07	0.09	-0.25
470	-0.16	-0.14	-0.11	-0.09	-0.06	-0.04	-0.01	0.01	0.04	0.06	0.09	-0.26
475	-0.17	-0.14	-0.12	-0.09	-0.07	-0.04	-0.02	0.01	0.03	0.06	0.08	-0.28
480	-0.17	-0.15	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.08	-0.30
485	-0.18	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	-0.32
490	-0.18	-0.16	-0.13	-0.11	-0.08	-0.06	-0.03	-0.01	0.02	0.04	0.07	-0.34
495	-0.19	-0.16	-0.14	-0.11	-0.09	-0.06	-0.04	-0.01	0.01	0.04	0.06	-0.35
500	-0.19	-0.17	-0.14	-0.12	-0.09	-0.07	-0.04	-0.02	0.01	0.03	0.06	-0.37





JVS 17 JUL 98

18 July 98

OM CULVERT BR#A500  
OM file: A506LRF4.pol  
OM Date: 17Jul98  
OM Hydraulic Design  
OM Quintuple Box Culvert (No Haunch)  
OM 5-Cell Box 12'x 12' Design as 4-Cell  
OM Load Factor Design  
OM Rigid Frame Method  
OM Top and Bot Slab Different  
OM Exterior and Interior Wall Different  
OM  
OM Maximum Fill Ht Condition (4.0 Ft)  
OM

STDLOD 2, 0, 0, 0, 0  
SWPRES 1, 2, 60, 15, 62.4  
BOXDIM 1, 4, 12, 12, 4, 10  
SLBTHK 1, 11.5, 11.5, 9.5, 8, 1111  
H&SKEW 1, 90, 90, 0, 0, 0  
REEBAR 18, 9, 1, 11, 4, .016  
CONCOV 2, 3, 2, 1.5, .5, .5  
MATPRP 120, 60, 24, 3, 0, 0  
PRTCTL 1, 1, 1, 0  
F&HCTL 1, 1, 1  
DESCTL 1, 0, 1, 0, 0, 9

CONSTANT DATA

STANDARD LIVE LOAD		-	DESIGN METHOD	-	PRINT CONTROL			
TRUCK	OMIT	STRESS	OVERLID	-	SERVICE	LOAD	-	10th Pt INFL LOC. NEG
CODE	L.L.	0-FILL	AXLE	-	LOAD	FACTOR	-	MOMENT LINE MOMENT
HS20	NO	NO	0.	-	NO	YES	-	YES YES 1.00

MATERIAL PROPERTIES						-	THICKNESS
SOIL	STEEL	STEEL	CONCRETE	CONCRETE	CON.SHEAR	-	INCREMENTS
WEIGHT	Fy	Fs	STRENGTH	SHEAR	W/ STIRRUP	-	SLAB WALL
120.	60000.	24000.	3000.	0.	0.	-	0.50 0.50

CONCRETE COVER		-	DESIGN	-	PRINT	-	REINFORCING					
EXTERIOR			INTERIOR	-	SAME	-	BAR	-	BAR SPACING	BAR SIZE		
TOP	BOT	WALL	(ALL)	-	THICKNESS	-	TABLE	-	MAX	MIN	MAX	MIN
SLAB	SLAB			-	SLAB WALL	-		-				
2.00	3.00	2.00	1.50	-	NO	NO	YES	-	18.0	9.0	11	4

CRACK PARAMETER Z = 98.0  
 MODULAR RATIO N = 9.0

SUPERIMPOSED DEAD LOADS						-	SPECIAL LIVE LOADS			
UNIFORM	CONCENTRATED LOAD					-	WHEEL	FILL	OVERSTRESS	
LOAD	WT.	X1	WT.	X2	WT.	X3	-	LOAD	HEIGHT	FACTOR
0.000	0.00	0.0	0.00	0.0	0.00	0.0	-	0.000	0.000	1.00

DATA FOR STRUCTURE NUMBER 1

CULVERT	-	SPAN	-	CLEAR	-	DESIGN	-	CENTERLINE	-	SKEW	-	SKEW	-	FLOOR
TYPE	-	LENGTH	-	HEIGHT	-	FILL	-	LENGTH	-	LEFT	-	RIGHT	-	TYPE
QDRPLE		12.00		12.00		4.00		10.00		90		90		FULL

SLAB THICKNESSES				-	LIVE	-	SOIL	-	WATER	
TOP	BOT.	EXT.	INT.	-	LOAD	-	PRESSURE	-	PRESSURE	
SLAB	SLAB	WALL	WALL	-	SURCHARGE	-	MAX	MIN	-	
11.50F	11.50F	9.50F	8.00F	-	2.00	-	60.0	15.0	-	62.4

TOP HAUNCH	BOTTOM HAUNCH	-	RIGID OR	-	CHECK	-	BAR SPACING
HEIGHT	HEIGHT	-	FLEXIBLE	-	MILITARY	-	INCREMENT
0.0	0.0	-	RIGID	-	NO	-	1 INCH

BOTH HEADWALLS ELIMINATED.

\*\*\*\*\* LOAD FACTOR DESIGN \*\*\*\*\*  
 \*\*\*\*\* STRESSES AT CRITICAL SECTIONS \*\*\*\*\*

\*\*\* MAXIMUM REINFORCEMENT RATIO (As/bd) = .016

MEMBER NUMBER = 1  
 MEMBER THICKNESS = 9.50  
 EXTERIOR WAL

	-MOMENT-	-AXIAL-	-SHEAR-	-Po-	-Mu-	-Mbal-	-Pbal-	-STEEL-	-SHEAR-	-ALL.-	-ALL.-
	FORCE							AREA	STRESS	MOM.	SHEAR
LT	-19.8	2.9	7.3	240.6	19.8	27.0	52.9	1.03	108.7	20.2	125.4
MID	8.2	5.2	2.0	222.7	8.2	24.0	80.3	0.41	27.1	9.2	119.1
MID-	-8.9	7.4	2.0	224.5	8.9	24.0	72.1	0.37	29.0	10.4	119.3
RT	-18.9	6.9	5.7	239.3	18.9	27.0	54.4	0.93	85.3	20.0	123.6

MEMBER NUMBER = 2  
 MEMBER THICKNESS = 11.50  
 TOP SLAB

	-MOMENT-	-AXIAL-	-SHEAR-	-Po-	-Mu-	-Mbal-	-Pbal-	-STEEL-	-SHEAR-	-ALL.-	-ALL.-
	FORCE							AREA	STRESS	MOM.	SHEAR
LT	-19.3	6.2	8.9	277.7	19.3	41.0	92.0	0.74	97.3	20.8	124.7
MID	22.6	-1.1	3.2	282.3	24.7	44.0	92.8	0.72	33.0	24.5	120.0
RT	-23.0	-1.5	9.8	284.3	25.1	43.0	83.6	0.74	107.3	24.8	126.4

MEMBER NUMBER = 3  
 MEMBER THICKNESS = 8.00  
 INTERIOR WAL

	-MOMENT-	-AXIAL-	-SHEAR-	-Po-	-Mu-	-Mbal-	-Pbal-	-STEEL-	-SHEAR-	-ALL.-	-ALL.-
	FORCE							AREA	STRESS	MOM.	SHEAR
LT	-6.8	10.1	1.2	189.6	6.8	15.0	53.6	0.26	24.2	8.3	118.7
MID	1.8	13.8	1.2	186.8	5.0	14.0	56.6	0.19	24.2	7.2	121.3
RT	-8.1	12.5	1.3	191.8	8.1	15.0	51.4	0.32	24.9	9.8	118.8

MEMBER NUMBER = 4  
 MEMBER THICKNESS = 11.50  
 BOTTOM SLAB

	-MOMENT-	-AXIAL-	-SHEAR-	-Po-	-Mu-	-Mbal-	-Pbal-	-STEEL-	-SHEAR-	-ALL.-	-ALL.-
	FORCE							AREA	STRESS	MOM.	SHEAR
LT	-20.3	5.9	7.7	282.0	20.3	38.0	73.6	0.95	94.1	21.7	124.6
MID	16.7	-1.5	1.5	275.5	18.3	41.0	101.4	0.47	15.5	18.0	118.5
RT	-26.3*	-0.9	9.3	290.1	26.3	40.0	63.3	0.81	113.9	26.1	126.4

MEMBER NUMBER = 5  
 MEMBER THICKNESS = 11.50  
 TOP SLAB

	-MOMENT-	-AXIAL-	-SHEAR-	-Po-	-Mu-	-Mbal-	-Pbal-	-STEEL-	-SHEAR-	-ALL.-	-ALL.-
	FORCE							AREA	STRESS	MOM.	SHEAR
LT	-22.2	0.7	9.5	280.9	22.2	42.0	88.0	0.71	103.0	22.3	125.2
MID	19.0	6.5	3.6	276.2	19.0	42.0	100.5	0.63	36.7	20.5	120.0
RT	-19.5	4.5	9.1	277.9	19.5	41.0	91.8	0.65	99.0	20.5	124.8

MEMBER NUMBER = 6  
 MEMBER THICKNESS = 8.00  
 INTERIOR WAL

	-MOMENT-	-AXIAL-	-SHEAR-	-Po-	-Mu-	-Mbal-	-Pbal-	-STEEL-	-SHEAR-	-ALL.-	-ALL.-
	FORCE							AREA	STRESS	MOM.	SHEAR
LT	-8.0	11.7	1.4	191.6	8.0	15.0	51.6	0.31	28.1	9.6	119.0
MID	1.4	13.8	1.4	186.8	5.0	14.0	56.6	0.19	28.1	7.2	123.4
RT	-8.7	12.6	1.4	192.9	8.7	15.0	50.2	0.34	27.4	10.3	118.9

MEMBER NUMBER = 7  
 MEMBER THICKNESS = 11.50  
 BOTTOM SLAB

	-MOMENT-	-AXIAL-	-SHEAR-	-Po-	-Mu-	-Mbal-	-Pbal-	-STEEL-	-SHEAR-	-ALL.-	-ALL.-
	FORCE							AREA	STRESS	MOM.	SHEAR
LT	-26.6	-2.3	8.1	293.9	29.0	41.0	58.5	0.91	99.1	28.5	126.0
MID	12.5	5.3	1.8	269.6	12.5	39.0	108.9	0.37	18.8	13.8	118.6
RT	-23.9	8.1	8.0	286.8	23.9	39.0	67.4	0.73	97.8	25.7	125.0

NOTE: ASTERISK IMPLIES DESIGN VALUES EXCEED CRITICAL VALUES

\*\*\*\*\* ATTENTION: OVERSTRESS DUE TO FIXED THICKNESS

A CORNER BAR(T)				A CORNER BAR(B)				A TSLAB+		A TSLAB-	
H	V	SZ	SPG	H	V	SZ	SPG	SZ	SPG	SZ	SPG
58	51	8	9.0	58	50	8	9.0	8	9.0	8	9.0

A BSLAB+		A BSLAB-		B EXTIN		B EXTOUT		B INTWL		C1
SZ	SPG	SZ	SPG	SZ	SPG	SZ	SPG	SZ	SPG	BAR
7	9.0	9	9.0	5	9.0	8	9.0	6	9.0	192

\*\* THE HEIGHT OF C.H.C.U. \*\* BOTTOM SLAB = 4.75 IN  
 TOP SLAB = 5.75 IN

** T.SLAB	* B.SLAB	* WALL	* INWALL	*** VOLUME	*** STEEL **
IN	IN	IN	IN	CY/FT	LB/FT
11.50	11.50	9.50	8.00	5.254	1271

\*\* REINFORCING STEEL BAR SCHEDULE \*\*

* LOCATN *	BAR	* NO. *	* SZ *	* TYP *	* LNGTH *	* WT. *	* H LEG *	* V LEG
TOP SLAB POSV	MAIN A100	14	8	STR	51- 2	1913		
BOT SLAB POSV	MAIN A200	14	7	STR	51- 2	1464		
TOP SLAB NEGV	MAIN A300	14	8	STR	51- 2	1913		
BOT SLAB NEGV	MAIN A400	14	9	STR	51- 2	2436		
CORNER (TOP)	A1	28	8	6	9- 1	679	4-10	4- 3
CORNER (BOTTOM)	A2	28	8	6	9- 0	673	4-10	4- 2
EXTWALL IN	B1	28	5	STR	13- 5	392		
EXTWALL OUT	B2	28	8	STR	11- 4	847		
INTWALL	B3	42	6	STR	13- 5	846		
LONGTD ( 1)	C1	192	4	STR	9- 8	1240		
TOTAL						12403		

\*\*\*\*\* SPLICE LENGTHS CHART \*\*\*\*\*

BAR	SIZE	SPLICE LENGTH
A200	7	3- 0
A400	9	4-11
B1	5	1- 8
B3	6	2- 3
C1	4	2- 2

\*\* MOMENT \* AXIAL FORCE \* SHEAR FOR LOAD FACTOR DESIGN AT TENTH POINT \*\*

M-PT	+MOMENT	-MOMENT	+A.F.	-A.F.	+SHEAR	-SHEAR
1- 0	7.993	-23.522	5.230	2.925	8.783	-3.753
1- 1	3.624	-13.322	5.230	2.925	6.981	-3.006
1- 2	5.550	-10.760	6.522	1.633	5.310	-2.351
1- 3	7.661	-9.983	6.522	8.073	3.769	-1.790
1- 4	8.176	-8.871	5.208	7.446	2.360	-1.323
1- 5	7.295	-7.543	5.099	7.153	1.950	-1.818
1- 6	7.312	-7.563	2.925	6.582	2.231	-2.965
1- 7	6.553	-8.115	2.925	6.118	2.419	-3.981
1- 8	4.563	-8.572	2.925	6.118	2.513	-4.867
1- 9	6.582	-14.089	1.633	6.945	2.513	-5.621
1-10	9.788	-21.779	1.633	6.945	2.420	-6.245
2- 0	9.788	-21.779	-2.420	6.235	10.266	1.633
2- 1	13.295	-13.800	-1.791	6.245	8.780	0.791
2- 2	18.468	-7.105	-1.791	6.245	7.338	-0.051
2- 3	21.489	-2.967	-1.432	5.947	5.927	-0.893
2- 4	22.635	-0.570	-1.116	5.686	4.547	-2.586
2- 5	21.909	0.248	-0.843	5.533	3.201	-4.080
2- 6	19.371	-0.062	-0.615	4.974	1.894	-5.537
2- 7	15.143	-2.832	-0.430	3.639	0.629	-6.938
2- 8	10.344	-7.986	5.478	-2.380	-0.697	-8.315
2- 9	5.020	-15.409	6.245	-1.651	-2.005	-9.654
2-10	-1.177	-25.704	5.675	-1.408	-3.161	-10.961
3- 0	7.852	-7.334	14.128	10.142	1.221	-1.256
3- 1	6.284	-5.811	14.128	10.142	1.221	-1.256
3- 2	4.739	-4.289	12.997	10.142	1.221	-1.256
3- 3	3.215	-2.767	12.997	10.142	1.221	-1.256
3- 4	1.820	-1.245	13.814	10.142	1.221	-1.256
3- 5	1.413	-0.745	14.387	12.985	1.221	-1.256
3- 6	2.581	-2.164	12.804	12.455	1.221	-1.256
3- 7	4.080	-3.792	12.314	12.455	1.221	-1.256
3- 8	5.631	-5.419	12.314	12.455	1.221	-1.256
3- 9	7.182	-7.047	12.314	12.455	1.221	-1.256
3-10	8.736	-8.675	11.815	12.455	1.221	-1.256
4- 0	7.993	-23.521	-0.854	5.884	8.919	4.020
4- 1	12.758	-13.221	-0.854	5.884	7.432	2.690
4- 2	15.630	-5.113	-1.484	5.884	5.944	1.360
4- 3	16.789	0.127	-1.484	5.884	4.457	0.026
4- 4	16.701	3.740	-1.484	6.803	2.970	-1.461
4- 5	15.776	4.339	-3.061	7.356	1.505	-2.948
4- 6	14.077	2.093	-3.061	8.263	0.041	-4.435
4- 7	11.354	-1.796	-3.061	8.743	-1.423	-5.922
4- 8	6.979	-7.503	2.212	3.347	-2.886	-7.426
4- 9	2.211	-17.288	5.894	-0.895	-4.142	-8.965
4-10	-4.364	-29.534	5.884	-0.854	-5.233	-10.505
5- 0	-0.912	-24.374	5.369	0.949	10.697	3.396
5- 1	5.903	-15.895	5.499	-0.014	9.239	2.384
5- 2	11.428	-10.190	5.619	-1.725	7.783	1.316
5- 3	15.462	-6.624	5.722	-1.951	6.338	0.155
5- 4	18.017	-4.424	6.362	-1.951	4.924	-1.072
5- 5	19.011	-3.297	6.468	-1.951	3.554	-2.421
5- 6	18.202	-3.240	6.531	-1.951	2.225	-4.518
5- 7	15.667	-4.343	2.831	1.914	0.946	-5.945
5- 8	11.950	-7.000	0.719	4.005	-0.277	-7.400



5- 9	6.812	-12.451	0.658	4.463	-1.472	-8.872
5-10	0.436	-21.953	0.562	4.463	-2.616	-10.350
6- 0	8.477	-8.648	12.580	11.860	1.419	-1.380
6- 1	6.689	-6.812	12.580	11.418	1.419	-1.380
6- 2	4.901	-4.986	12.580	11.418	1.419	-1.380
6- 3	3.113	-3.160	12.580	11.418	1.419	-1.380
6- 4	1.395	-1.352	13.806	10.987	1.419	-1.380
6- 5	0.836	-0.882	11.794	12.805	1.419	-1.380
6- 6	2.382	-2.252	11.860	12.580	1.419	-1.380
6- 7	4.220	-4.040	11.860	12.580	1.419	-1.380
6- 8	6.059	-5.829	11.860	12.580	1.419	-1.380
6- 9	7.897	-7.617	11.860	12.580	1.419	-1.380
6-10	9.735	-9.405	11.860	12.580	1.419	-1.380
7- 0	-4.265	-29.488	7.666	-2.441	9.258	5.128
7- 1	2.278	-18.649	7.666	-2.003	7.771	3.798
7- 2	7.171	-10.322	6.893	-1.550	6.284	2.468
7- 3	10.718	-3.998	6.893	-0.600	4.797	1.138
7- 4	12.494	-0.025	5.322	-0.600	3.310	-0.219
7- 5	12.482	1.321	5.124	-0.457	1.823	-1.706
7- 6	10.709	0.730	5.124	-0.457	0.537	-3.193
7- 7	9.124	-2.657	-3.906	8.045	-0.741	-4.680
7- 8	6.388	-8.409	-3.837	8.045	-2.019	-6.167
7- 9	1.766	-16.196	-3.837	7.892	-3.297	-7.662
7-10	-3.703	-26.675	-3.626	8.214	-4.575	-9.161

\*\*\*\*\* INFLUENCE LINES FOR MOMENT \*\*\*\*\*

\*\*\*\*\* MEMBER NO. 1 \*\*\*\*\*

	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9	1.0
100	-1.43	-1.15	-0.87	-0.59	-0.31	-0.03	0.25	0.53	0.81	1.10	1.38
105	-1.31	-1.06	-0.82	-0.58	-0.34	-0.10	0.14	0.38	0.62	0.87	1.11
110	-1.17	-0.97	-0.77	-0.56	-0.36	-0.16	0.05	0.25	0.45	0.66	0.86
115	-1.04	-0.87	-0.70	-0.54	-0.37	-0.20	-0.04	0.13	0.30	0.47	0.63
120	-0.90	-0.77	-0.64	-0.50	-0.37	-0.24	-0.10	0.03	0.16	0.29	0.43
125	-0.77	-0.67	-0.56	-0.46	-0.36	-0.26	-0.16	-0.06	0.04	0.14	0.24
130	-0.63	-0.56	-0.49	-0.42	-0.35	-0.28	-0.21	-0.14	-0.07	0.00	0.07
135	-0.50	-0.45	-0.41	-0.37	-0.33	-0.29	-0.25	-0.20	-0.16	-0.12	-0.08
140	-0.36	-0.35	-0.33	-0.32	-0.30	-0.29	-0.27	-0.26	-0.24	-0.23	-0.21
145	-0.23	-0.24	-0.25	-0.26	-0.27	-0.28	-0.29	-0.30	-0.31	-0.32	-0.33
150	-0.11	-0.14	-0.17	-0.21	-0.24	-0.27	-0.30	-0.33	-0.37	-0.40	-0.43
155	0.01	-0.04	-0.09	-0.15	-0.20	-0.25	-0.31	-0.36	-0.41	-0.47	-0.52
160	0.13	0.05	-0.02	-0.09	-0.16	-0.23	-0.31	-0.38	-0.45	-0.52	-0.59
165	0.24	0.15	0.06	-0.03	-0.12	-0.21	-0.30	-0.39	-0.48	-0.57	-0.66
170	0.34	0.23	0.13	0.02	-0.08	-0.18	-0.29	-0.39	-0.50	-0.60	-0.71
175	0.43	0.31	0.19	0.08	-0.04	-0.16	-0.28	-0.39	-0.51	-0.63	-0.75
180	0.51	0.38	0.26	0.13	0.00	-0.13	-0.26	-0.39	-0.52	-0.65	-0.78
185	0.59	0.45	0.31	0.17	0.03	-0.10	-0.24	-0.38	-0.52	-0.66	-0.80
190	0.65	0.50	0.36	0.21	0.07	-0.08	-0.22	-0.37	-0.52	-0.66	-0.81
195	0.70	0.55	0.40	0.25	0.10	-0.05	-0.21	-0.36	-0.51	-0.66	-0.81
200	0.74	0.59	0.43	0.28	0.12	-0.03	-0.19	-0.34	-0.50	-0.66	-0.81
205	0.77	0.61	0.46	0.30	0.14	-0.02	-0.18	-0.33	-0.49	-0.65	-0.81
210	0.80	0.64	0.48	0.32	0.16	0.00	-0.16	-0.32	-0.48	-0.64	-0.80
215	0.81	0.65	0.49	0.33	0.17	0.01	-0.15	-0.31	-0.48	-0.64	-0.80
220	0.83	0.67	0.50	0.34	0.18	0.02	-0.15	-0.31	-0.47	-0.63	-0.79
225	0.84	0.67	0.51	0.35	0.19	0.02	-0.14	-0.30	-0.47	-0.63	-0.79
230	0.84	0.68	0.51	0.35	0.19	0.03	-0.14	-0.30	-0.46	-0.62	-0.79
235	0.84	0.68	0.51	0.35	0.19	0.03	-0.13	-0.30	-0.46	-0.62	-0.78
240	0.83	0.67	0.51	0.35	0.19	0.03	-0.13	-0.29	-0.45	-0.62	-0.78
245	0.82	0.67	0.51	0.35	0.19	0.03	-0.13	-0.29	-0.45	-0.61	-0.77
250	0.81	0.65	0.50	0.34	0.18	0.02	-0.13	-0.29	-0.45	-0.60	-0.76
255	0.79	0.64	0.49	0.33	0.18	0.02	-0.13	-0.29	-0.44	-0.60	-0.75
260	0.77	0.62	0.47	0.32	0.17	0.02	-0.14	-0.29	-0.44	-0.59	-0.74
265	0.75	0.60	0.45	0.31	0.16	0.01	-0.14	-0.29	-0.43	-0.58	-0.73
270	0.72	0.58	0.44	0.29	0.15	0.00	-0.14	-0.28	-0.43	-0.57	-0.71
275	0.69	0.55	0.42	0.28	0.14	0.00	-0.14	-0.28	-0.42	-0.56	-0.70
280	0.66	0.53	0.39	0.26	0.13	-0.01	-0.14	-0.28	-0.41	-0.54	-0.68
285	0.63	0.50	0.37	0.24	0.11	-0.01	-0.14	-0.27	-0.40	-0.53	-0.66
290	0.59	0.47	0.35	0.22	0.10	-0.02	-0.14	-0.27	-0.39	-0.51	-0.63
295	0.55	0.44	0.32	0.20	0.09	-0.03	-0.14	-0.26	-0.37	-0.49	-0.60
300	0.51	0.40	0.29	0.19	0.08	-0.03	-0.14	-0.25	-0.36	-0.46	-0.57
305	0.47	0.37	0.27	0.17	0.07	-0.04	-0.14	-0.24	-0.34	-0.44	-0.54
310	0.43	0.33	0.24	0.15	0.05	-0.04	-0.13	-0.22	-0.32	-0.41	-0.50
315	0.38	0.30	0.21	0.13	0.04	-0.04	-0.13	-0.21	-0.30	-0.38	-0.47
320	0.34	0.27	0.19	0.11	0.03	-0.04	-0.12	-0.20	-0.28	-0.35	-0.43
325	0.30	0.23	0.16	0.09	0.02	-0.05	-0.11	-0.18	-0.25	-0.32	-0.39
330	0.26	0.20	0.14	0.08	0.01	-0.05	-0.11	-0.17	-0.23	-0.29	-0.35
335	0.22	0.16	0.11	0.06	0.01	-0.05	-0.10	-0.15	-0.20	-0.26	-0.31
340	0.17	0.13	0.09	0.04	0.00	-0.05	-0.09	-0.14	-0.18	-0.22	-0.27
345	0.13	0.10	0.06	0.02	-0.01	-0.05	-0.08	-0.12	-0.15	-0.19	-0.22
350	0.09	0.06	0.03	0.01	-0.02	-0.05	-0.07	-0.10	-0.13	-0.15	-0.18
355	0.04	0.03	0.01	-0.01	-0.03	-0.05	-0.06	-0.08	-0.10	-0.12	-0.13
360	0.00	-0.01	-0.02	-0.03	-0.04	-0.04	-0.05	-0.06	-0.07	-0.08	-0.09
365	-0.05	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04
370	-0.09	-0.08	-0.07	-0.06	-0.05	-0.04	-0.03	-0.02	-0.01	0.00	0.01

375	-0.14	-0.12	-0.10	-0.08	-0.06	-0.04	-0.02	0.00	0.02	0.04	0.06
380	-0.18	-0.15	-0.13	-0.10	-0.07	-0.04	-0.01	0.02	0.05	0.08	0.11
385	-0.23	-0.19	-0.15	-0.11	-0.08	-0.04	0.00	0.04	0.08	0.12	0.16
390	-0.28	-0.23	-0.18	-0.13	-0.08	-0.04	0.01	0.06	0.11	0.16	0.21
395	-0.33	-0.27	-0.21	-0.15	-0.09	-0.03	0.02	0.08	0.14	0.20	0.26
400	-0.38	-0.31	-0.24	-0.17	-0.10	-0.03	0.04	0.10	0.17	0.24	0.31
405	-0.43	-0.35	-0.27	-0.19	-0.11	-0.03	0.05	0.13	0.21	0.28	0.36
410	-0.48	-0.39	-0.30	-0.21	-0.12	-0.03	0.06	0.15	0.24	0.33	0.42
415	-0.53	-0.43	-0.33	-0.23	-0.13	-0.03	0.07	0.17	0.27	0.37	0.47
420	-0.58	-0.47	-0.36	-0.25	-0.14	-0.03	0.08	0.19	0.30	0.41	0.52
425	-0.63	-0.51	-0.39	-0.27	-0.15	-0.03	0.09	0.21	0.33	0.45	0.57
430	-0.68	-0.55	-0.42	-0.29	-0.16	-0.03	0.10	0.23	0.36	0.49	0.63
435	-0.74	-0.59	-0.45	-0.31	-0.17	-0.03	0.11	0.25	0.40	0.54	0.68
440	-0.79	-0.64	-0.48	-0.33	-0.18	-0.03	0.12	0.27	0.43	0.58	0.73
445	-0.84	-0.68	-0.52	-0.35	-0.19	-0.03	0.13	0.30	0.46	0.62	0.78
450	-0.89	-0.72	-0.55	-0.38	-0.20	-0.03	0.14	0.32	0.49	0.66	0.84
455	-0.95	-0.76	-0.58	-0.40	-0.21	-0.03	0.15	0.34	0.52	0.71	0.89
460	-1.00	-0.81	-0.61	-0.42	-0.22	-0.03	0.16	0.36	0.55	0.75	0.94
465	-1.06	-0.85	-0.65	-0.44	-0.23	-0.03	0.18	0.38	0.59	0.79	1.00
470	-1.11	-0.89	-0.68	-0.46	-0.25	-0.03	0.19	0.40	0.62	0.83	1.05
475	-1.16	-0.94	-0.71	-0.48	-0.26	-0.03	0.20	0.42	0.65	0.88	1.10
480	-1.22	-0.98	-0.74	-0.51	-0.27	-0.03	0.21	0.44	0.68	0.92	1.16
485	-1.27	-1.02	-0.78	-0.53	-0.28	-0.03	0.22	0.46	0.71	0.96	1.21
490	-1.33	-1.07	-0.81	-0.55	-0.29	-0.03	0.23	0.49	0.75	1.00	1.26
495	-1.38	-1.11	-0.84	-0.57	-0.30	-0.03	0.24	0.51	0.78	1.05	1.32
500	-1.44	-1.16	-0.88	-0.60	-0.31	-0.03	0.25	0.53	0.81	1.09	1.37

\*\*\*\*\* MEMBER NO. 2 \*\*\*\*\*

	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9	1.0
100	1.38	1.12	0.87	0.62	0.37	0.11	-0.14	-0.39	-0.64	-0.90	-1.15
105	1.11	1.45	1.16	0.87	0.57	0.28	-0.01	-0.30	-0.60	-0.89	-1.18
110	0.86	1.80	1.46	1.13	0.80	0.46	0.13	-0.20	-0.54	-0.87	-1.21
115	0.63	1.53	1.79	1.41	1.04	0.66	0.28	-0.09	-0.47	-0.85	-1.22
120	0.43	1.28	2.13	1.71	1.29	0.87	0.45	0.03	-0.39	-0.81	-1.23
125	0.24	1.05	1.86	2.03	1.57	1.10	0.64	0.17	-0.29	-0.76	-1.22
130	0.07	0.84	1.60	2.36	1.85	1.35	0.84	0.33	-0.18	-0.69	-1.20
135	-0.08	0.64	1.36	2.08	2.16	1.61	1.05	0.50	-0.05	-0.61	-1.16
140	-0.21	0.46	1.14	1.81	2.48	1.89	1.29	0.69	0.09	-0.51	-1.11
145	-0.33	0.30	0.93	1.56	2.19	2.18	1.54	0.89	0.25	-0.39	-1.04
150	-0.43	0.15	0.74	1.32	1.91	2.49	1.81	1.12	0.43	-0.26	-0.94
155	-0.52	0.02	0.56	1.11	1.65	2.19	2.09	1.36	0.63	-0.10	-0.83
160	-0.59	-0.09	0.40	0.90	1.40	1.90	2.40	1.63	0.85	0.08	-0.69
165	-0.66	-0.20	0.26	0.72	1.18	1.63	2.09	1.91	1.10	0.29	-0.53
170	-0.71	-0.29	0.13	0.55	0.97	1.39	1.81	2.22	1.37	0.51	-0.34
175	-0.75	-0.36	0.02	0.40	0.78	1.16	1.54	1.92	1.66	0.77	-0.12
180	-0.78	-0.43	-0.09	0.26	0.60	0.95	1.29	1.64	1.98	1.06	0.13
185	-0.80	-0.48	-0.17	0.14	0.45	0.76	1.07	1.38	1.70	1.37	0.41
190	-0.81	-0.53	-0.25	0.03	0.31	0.59	0.87	1.15	1.43	1.71	0.72
195	-0.81	-0.56	-0.31	-0.06	0.20	0.45	0.70	0.95	1.20	1.46	1.07
200	-0.81	-0.58	-0.36	-0.13	0.10	0.32	0.55	0.78	1.00	1.23	1.46
205	-0.81	-0.60	-0.40	-0.19	0.01	0.22	0.42	0.62	0.83	1.03	1.24
210	-0.80	-0.62	-0.43	-0.25	-0.06	0.12	0.31	0.49	0.67	0.86	1.04
215	-0.80	-0.63	-0.46	-0.30	-0.13	0.04	0.20	0.37	0.54	0.71	0.87
220	-0.79	-0.64	-0.49	-0.34	-0.19	-0.03	0.12	0.27	0.42	0.57	0.73
225	-0.79	-0.65	-0.51	-0.37	-0.24	-0.10	0.04	0.18	0.32	0.46	0.60
230	-0.79	-0.66	-0.53	-0.40	-0.28	-0.15	-0.02	0.11	0.23	0.36	0.49
235	-0.78	-0.66	-0.55	-0.43	-0.31	-0.19	-0.07	0.04	0.16	0.28	0.40
240	-0.78	-0.67	-0.56	-0.45	-0.34	-0.23	-0.12	-0.01	0.10	0.21	0.32
245	-0.77	-0.67	-0.56	-0.46	-0.36	-0.25	-0.15	-0.05	0.05	0.16	0.26
250	-0.76	-0.66	-0.57	-0.47	-0.37	-0.27	-0.18	-0.08	0.02	0.12	0.21
255	-0.75	-0.66	-0.57	-0.47	-0.38	-0.29	-0.20	-0.10	-0.01	0.08	0.18
260	-0.74	-0.65	-0.56	-0.47	-0.39	-0.30	-0.21	-0.12	-0.03	0.06	0.15
265	-0.73	-0.64	-0.56	-0.47	-0.39	-0.30	-0.21	-0.13	-0.04	0.04	0.13
270	-0.71	-0.63	-0.55	-0.47	-0.38	-0.30	-0.22	-0.13	-0.05	0.03	0.12

275	-0.70	-0.62	-0.54	-0.46	-0.38	-0.30	-0.21	-0.13	-0.05	0.03	0.11
280	-0.68	-0.60	-0.52	-0.44	-0.37	-0.29	-0.21	-0.13	-0.05	0.02	0.10
285	-0.66	-0.58	-0.51	-0.43	-0.35	-0.28	-0.20	-0.13	-0.05	0.02	0.10
290	-0.63	-0.56	-0.49	-0.41	-0.34	-0.27	-0.19	-0.12	-0.05	0.02	0.10
295	-0.60	-0.53	-0.46	-0.39	-0.32	-0.26	-0.19	-0.12	-0.05	0.02	0.09
300	-0.57	-0.51	-0.44	-0.37	-0.31	-0.24	-0.18	-0.11	-0.05	0.02	0.09
305	-0.54	-0.48	-0.42	-0.35	-0.29	-0.23	-0.17	-0.11	-0.05	0.01	0.08
310	-0.50	-0.45	-0.39	-0.33	-0.28	-0.22	-0.17	-0.11	-0.05	0.00	0.06
315	-0.47	-0.42	-0.37	-0.32	-0.26	-0.21	-0.16	-0.11	-0.06	-0.01	0.04
320	-0.43	-0.39	-0.34	-0.30	-0.25	-0.21	-0.16	-0.12	-0.07	-0.03	0.02
325	-0.39	-0.35	-0.32	-0.28	-0.24	-0.20	-0.16	-0.13	-0.09	-0.05	-0.01
330	-0.35	-0.32	-0.29	-0.26	-0.23	-0.20	-0.17	-0.14	-0.10	-0.07	-0.04
335	-0.31	-0.29	-0.26	-0.24	-0.22	-0.19	-0.17	-0.15	-0.12	-0.10	-0.08
340	-0.27	-0.25	-0.24	-0.22	-0.21	-0.19	-0.17	-0.16	-0.14	-0.13	-0.11
345	-0.22	-0.22	-0.21	-0.20	-0.19	-0.19	-0.18	-0.17	-0.17	-0.16	-0.15
350	-0.18	-0.18	-0.18	-0.18	-0.18	-0.19	-0.19	-0.19	-0.19	-0.19	-0.19
355	-0.13	-0.14	-0.15	-0.16	-0.17	-0.18	-0.19	-0.20	-0.21	-0.22	-0.23
360	-0.09	-0.11	-0.13	-0.14	-0.16	-0.18	-0.20	-0.22	-0.24	-0.26	-0.28
365	-0.04	-0.07	-0.10	-0.12	-0.15	-0.18	-0.21	-0.24	-0.26	-0.29	-0.32
370	0.01	-0.03	-0.07	-0.10	-0.14	-0.18	-0.21	-0.25	-0.29	-0.33	-0.36
375	0.06	0.01	-0.04	-0.08	-0.13	-0.18	-0.22	-0.27	-0.31	-0.36	-0.41
380	0.11	0.05	0.00	-0.06	-0.12	-0.17	-0.23	-0.28	-0.34	-0.39	-0.45
385	0.16	0.09	0.03	-0.04	-0.10	-0.17	-0.23	-0.30	-0.36	-0.43	-0.49
390	0.21	0.13	0.06	-0.01	-0.09	-0.16	-0.24	-0.31	-0.39	-0.46	-0.53
395	0.26	0.18	0.09	0.01	-0.07	-0.16	-0.24	-0.32	-0.41	-0.49	-0.57
400	0.31	0.22	0.13	0.03	-0.06	-0.15	-0.24	-0.33	-0.43	-0.52	-0.61
405	0.36	0.26	0.16	0.06	-0.04	-0.14	-0.24	-0.34	-0.45	-0.55	-0.65
410	0.42	0.31	0.20	0.09	-0.02	-0.13	-0.24	-0.35	-0.46	-0.57	-0.68
415	0.47	0.35	0.23	0.11	-0.01	-0.12	-0.24	-0.36	-0.48	-0.60	-0.72
420	0.52	0.39	0.27	0.14	0.01	-0.11	-0.24	-0.37	-0.49	-0.62	-0.75
425	0.57	0.44	0.30	0.17	0.03	-0.10	-0.24	-0.37	-0.51	-0.64	-0.78
430	0.63	0.48	0.34	0.20	0.05	-0.09	-0.23	-0.38	-0.52	-0.66	-0.81
435	0.68	0.53	0.38	0.22	0.07	-0.08	-0.23	-0.38	-0.53	-0.68	-0.84
440	0.73	0.57	0.41	0.25	0.09	-0.07	-0.23	-0.39	-0.54	-0.70	-0.86
445	0.78	0.62	0.45	0.28	0.11	-0.05	-0.22	-0.39	-0.56	-0.72	-0.89
450	0.84	0.66	0.49	0.31	0.14	-0.04	-0.21	-0.39	-0.57	-0.74	-0.92
455	0.89	0.71	0.52	0.34	0.16	-0.03	-0.21	-0.39	-0.57	-0.76	-0.94
460	0.94	0.75	0.56	0.37	0.18	-0.01	-0.20	-0.39	-0.58	-0.77	-0.96
465	1.00	0.80	0.60	0.40	0.20	0.00	-0.19	-0.39	-0.59	-0.79	-0.99
470	1.05	0.84	0.64	0.43	0.22	0.02	-0.19	-0.39	-0.60	-0.80	-1.01
475	1.10	0.89	0.68	0.46	0.25	0.03	-0.18	-0.39	-0.61	-0.82	-1.03
480	1.16	0.93	0.71	0.49	0.27	0.05	-0.17	-0.39	-0.61	-0.83	-1.06
485	1.21	0.98	0.75	0.52	0.29	0.07	-0.16	-0.39	-0.62	-0.85	-1.08
490	1.26	1.03	0.79	0.55	0.32	0.08	-0.15	-0.39	-0.63	-0.86	-1.10
495	1.32	1.07	0.83	0.59	0.34	0.10	-0.15	-0.39	-0.63	-0.88	-1.12
500	1.37	1.12	0.87	0.62	0.37	0.12	-0.14	-0.39	-0.64	-0.89	-1.14

\*\*\*\*\* MEMBER NO. 3 \*\*\*\*\*

	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9	1.0
100	-1.00	-0.80	-0.60	-0.40	-0.20	0.01	0.21	0.41	0.61	0.81	1.01
105	-1.01	-0.80	-0.60	-0.39	-0.19	0.02	0.22	0.43	0.63	0.84	1.04
110	-1.01	-0.80	-0.59	-0.39	-0.18	0.03	0.24	0.44	0.65	0.86	1.07
115	-1.00	-0.80	-0.59	-0.38	-0.17	0.04	0.25	0.46	0.67	0.88	1.08
120	-0.99	-0.78	-0.57	-0.37	-0.16	0.05	0.26	0.47	0.68	0.89	1.10
125	-0.97	-0.77	-0.56	-0.35	-0.14	0.06	0.27	0.48	0.69	0.89	1.10
130	-0.95	-0.74	-0.54	-0.34	-0.13	0.07	0.28	0.48	0.69	0.89	1.10
135	-0.92	-0.72	-0.52	-0.32	-0.12	0.08	0.28	0.48	0.69	0.89	1.09
140	-0.88	-0.69	-0.49	-0.30	-0.10	0.09	0.29	0.48	0.68	0.87	1.07
145	-0.84	-0.65	-0.47	-0.28	-0.09	0.10	0.29	0.47	0.66	0.85	1.04
150	-0.79	-0.61	-0.43	-0.26	-0.08	0.10	0.28	0.46	0.64	0.82	1.00
155	-0.74	-0.57	-0.40	-0.23	-0.06	0.11	0.28	0.45	0.62	0.79	0.96
160	-0.69	-0.53	-0.37	-0.21	-0.05	0.11	0.27	0.43	0.59	0.74	0.90
165	-0.62	-0.48	-0.33	-0.19	-0.04	0.11	0.25	0.40	0.55	0.69	0.84
170	-0.56	-0.43	-0.29	-0.16	-0.03	0.10	0.24	0.37	0.50	0.63	0.76

175	-0.49	-0.37	-0.26	-0.14	-0.02	0.10	0.21	0.33	0.45	0.56	0.68
180	-0.42	-0.32	-0.22	-0.12	-0.02	0.08	0.19	0.29	0.39	0.49	0.59
185	-0.34	-0.26	-0.18	-0.09	-0.01	0.07	0.15	0.24	0.32	0.40	0.48
190	-0.26	-0.20	-0.14	-0.07	-0.01	0.05	0.12	0.18	0.24	0.30	0.37
195	-0.18	-0.14	-0.10	-0.05	-0.01	0.03	0.07	0.11	0.16	0.20	0.24
200	-0.09	-0.07	-0.05	-0.03	-0.02	0.00	0.02	0.04	0.06	0.08	0.10
205	-0.01	-0.01	-0.01	-0.02	-0.02	-0.02	-0.02	-0.03	-0.03	-0.03	-0.03
210	0.07	0.05	0.03	0.00	-0.02	-0.04	-0.07	-0.09	-0.11	-0.14	-0.16
215	0.16	0.11	0.07	0.03	-0.02	-0.06	-0.10	-0.15	-0.19	-0.23	-0.28
220	0.23	0.17	0.11	0.05	-0.01	-0.07	-0.13	-0.20	-0.26	-0.32	-0.38
225	0.31	0.23	0.15	0.07	0.00	-0.08	-0.16	-0.24	-0.32	-0.40	-0.47
230	0.38	0.29	0.19	0.10	0.01	-0.09	-0.18	-0.28	-0.37	-0.47	-0.56
235	0.45	0.34	0.23	0.13	0.02	-0.09	-0.20	-0.31	-0.42	-0.53	-0.63
240	0.52	0.39	0.27	0.15	0.03	-0.09	-0.21	-0.33	-0.46	-0.58	-0.70
245	0.58	0.44	0.31	0.18	0.04	-0.09	-0.22	-0.36	-0.49	-0.62	-0.76
250	0.63	0.49	0.35	0.20	0.06	-0.08	-0.23	-0.37	-0.52	-0.66	-0.80
255	0.68	0.53	0.38	0.23	0.07	-0.08	-0.23	-0.38	-0.54	-0.69	-0.84
260	0.73	0.57	0.41	0.25	0.09	-0.07	-0.23	-0.39	-0.55	-0.71	-0.87
265	0.77	0.60	0.44	0.27	0.10	-0.06	-0.23	-0.40	-0.56	-0.73	-0.90
270	0.81	0.63	0.46	0.29	0.12	-0.05	-0.22	-0.40	-0.57	-0.74	-0.91
275	0.84	0.66	0.48	0.31	0.13	-0.04	-0.22	-0.39	-0.57	-0.75	-0.92
280	0.86	0.68	0.50	0.32	0.15	-0.03	-0.21	-0.39	-0.57	-0.75	-0.92
285	0.87	0.69	0.51	0.34	0.16	-0.02	-0.20	-0.38	-0.56	-0.74	-0.92
290	0.88	0.70	0.52	0.34	0.17	-0.01	-0.19	-0.37	-0.55	-0.73	-0.91
295	0.88	0.71	0.53	0.35	0.17	0.00	-0.18	-0.36	-0.54	-0.71	-0.89
300	0.88	0.70	0.53	0.35	0.18	0.00	-0.17	-0.35	-0.52	-0.70	-0.87
305	0.86	0.69	0.52	0.35	0.18	0.01	-0.16	-0.33	-0.50	-0.67	-0.84
310	0.85	0.68	0.52	0.35	0.18	0.01	-0.15	-0.32	-0.49	-0.65	-0.82
315	0.83	0.67	0.51	0.34	0.18	0.02	-0.14	-0.31	-0.47	-0.63	-0.79
320	0.81	0.65	0.50	0.34	0.18	0.02	-0.14	-0.29	-0.45	-0.61	-0.77
325	0.79	0.63	0.48	0.33	0.18	0.02	-0.13	-0.28	-0.43	-0.59	-0.74
330	0.76	0.61	0.47	0.32	0.17	0.03	-0.12	-0.27	-0.41	-0.56	-0.71
335	0.73	0.59	0.45	0.31	0.17	0.03	-0.11	-0.26	-0.40	-0.54	-0.68
340	0.70	0.57	0.43	0.30	0.16	0.03	-0.11	-0.24	-0.38	-0.51	-0.65
345	0.67	0.54	0.41	0.28	0.15	0.03	-0.10	-0.23	-0.36	-0.49	-0.62
350	0.63	0.51	0.39	0.27	0.15	0.03	-0.10	-0.22	-0.34	-0.46	-0.58
355	0.60	0.48	0.37	0.25	0.14	0.02	-0.09	-0.20	-0.32	-0.43	-0.55
360	0.56	0.45	0.34	0.24	0.13	0.02	-0.08	-0.19	-0.30	-0.40	-0.51
365	0.51	0.41	0.32	0.22	0.12	0.02	-0.08	-0.18	-0.28	-0.37	-0.47
370	0.47	0.38	0.29	0.20	0.11	0.02	-0.07	-0.16	-0.25	-0.34	-0.43
375	0.42	0.34	0.26	0.18	0.10	0.02	-0.07	-0.15	-0.23	-0.31	-0.39
380	0.38	0.30	0.23	0.16	0.09	0.01	-0.06	-0.13	-0.20	-0.28	-0.35
385	0.33	0.26	0.20	0.14	0.07	0.01	-0.05	-0.12	-0.18	-0.24	-0.30
390	0.27	0.22	0.17	0.12	0.06	0.01	-0.04	-0.10	-0.15	-0.20	-0.26
395	0.22	0.18	0.14	0.09	0.05	0.01	-0.04	-0.08	-0.12	-0.17	-0.21
400	0.17	0.14	0.10	0.07	0.04	0.00	-0.03	-0.06	-0.09	-0.13	-0.16
405	0.11	0.09	0.07	0.05	0.02	0.00	-0.02	-0.04	-0.06	-0.09	-0.11
410	0.06	0.05	0.03	0.02	0.01	0.00	-0.01	-0.02	-0.03	-0.04	-0.05
415	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
420	-0.05	-0.04	-0.03	-0.02	-0.01	0.00	0.01	0.02	0.03	0.04	0.05
425	-0.11	-0.09	-0.07	-0.04	-0.02	0.00	0.02	0.04	0.06	0.09	0.11
430	-0.17	-0.13	-0.10	-0.07	-0.03	0.00	0.03	0.06	0.10	0.13	0.16
435	-0.22	-0.18	-0.14	-0.09	-0.05	0.00	0.04	0.09	0.13	0.18	0.22
440	-0.28	-0.23	-0.17	-0.11	-0.06	0.00	0.05	0.11	0.17	0.22	0.28
445	-0.34	-0.27	-0.20	-0.14	-0.07	0.00	0.07	0.13	0.20	0.27	0.33
450	-0.40	-0.32	-0.24	-0.16	-0.08	0.00	0.08	0.16	0.23	0.31	0.39
455	-0.45	-0.36	-0.27	-0.18	-0.09	0.00	0.09	0.18	0.27	0.36	0.45
460	-0.51	-0.41	-0.31	-0.21	-0.10	0.00	0.10	0.20	0.31	0.41	0.51
465	-0.57	-0.46	-0.34	-0.23	-0.11	0.00	0.11	0.23	0.34	0.46	0.57
470	-0.63	-0.51	-0.38	-0.25	-0.13	0.00	0.13	0.25	0.38	0.51	0.63
475	-0.69	-0.55	-0.41	-0.28	-0.14	0.00	0.14	0.28	0.42	0.55	0.69
480	-0.75	-0.60	-0.45	-0.30	-0.15	0.00	0.15	0.30	0.45	0.60	0.75
485	-0.81	-0.65	-0.49	-0.32	-0.16	0.00	0.16	0.33	0.49	0.65	0.82
490	-0.87	-0.70	-0.52	-0.35	-0.17	0.00	0.18	0.35	0.53	0.70	0.88
495	-0.94	-0.75	-0.56	-0.37	-0.18	0.00	0.19	0.38	0.57	0.75	0.94
500	-1.00	-0.80	-0.60	-0.40	-0.20	0.00	0.20	0.40	0.61	0.81	1.01

\*\*\*\*\* MEMBER NO. 4 \*\*\*\*\*

	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9	1.0
100	1.43	1.07	0.73	0.43	0.15	-0.09	-0.30	-0.47	-0.62	-0.73	-0.81
105	1.31	0.96	0.65	0.37	0.12	-0.10	-0.28	-0.43	-0.56	-0.65	-0.70
110	1.17	0.85	0.57	0.31	0.09	-0.10	-0.26	-0.39	-0.48	-0.55	-0.58
115	1.04	0.75	0.49	0.26	0.06	-0.10	-0.24	-0.34	-0.41	-0.44	-0.45
120	0.90	0.64	0.41	0.20	0.04	-0.10	-0.21	-0.28	-0.32	-0.33	-0.31
125	0.77	0.53	0.33	0.15	0.01	-0.10	-0.17	-0.22	-0.23	-0.21	-0.16
130	0.63	0.42	0.25	0.10	-0.01	-0.09	-0.13	-0.15	-0.14	-0.09	-0.01
135	0.50	0.32	0.17	0.06	-0.03	-0.08	-0.09	-0.08	-0.04	0.04	0.15
140	0.36	0.21	0.10	0.01	-0.04	-0.06	-0.05	-0.01	0.06	0.17	0.31
145	0.23	0.11	0.03	-0.03	-0.06	-0.05	-0.01	0.06	0.16	0.30	0.47
150	0.11	0.02	-0.04	-0.07	-0.07	-0.03	0.04	0.13	0.27	0.43	0.62
155	-0.01	-0.08	-0.11	-0.11	-0.08	-0.02	0.08	0.21	0.36	0.55	0.78
160	-0.13	-0.16	-0.17	-0.15	-0.09	0.00	0.12	0.28	0.46	0.68	0.93
165	-0.24	-0.25	-0.23	-0.18	-0.10	0.02	0.17	0.34	0.55	0.80	1.07
170	-0.34	-0.33	-0.28	-0.21	-0.10	0.04	0.21	0.41	0.64	0.91	1.21
175	-0.43	-0.40	-0.33	-0.24	-0.11	0.05	0.25	0.47	0.73	1.01	1.33
180	-0.51	-0.46	-0.38	-0.26	-0.11	0.07	0.28	0.53	0.80	1.11	1.45
185	-0.59	-0.52	-0.41	-0.28	-0.11	0.08	0.31	0.57	0.87	1.19	1.55
190	-0.65	-0.57	-0.45	-0.30	-0.12	0.10	0.34	0.62	0.93	1.27	1.64
195	-0.70	-0.60	-0.47	-0.31	-0.12	0.11	0.36	0.65	0.97	1.33	1.71
200	-0.74	-0.63	-0.49	-0.32	-0.12	0.11	0.38	0.68	1.01	1.37	1.77
205	-0.77	-0.66	-0.51	-0.33	-0.12	0.12	0.39	0.69	1.03	1.40	1.80
210	-0.80	-0.68	-0.53	-0.35	-0.13	0.11	0.39	0.70	1.04	1.41	1.81
215	-0.81	-0.69	-0.54	-0.36	-0.15	0.10	0.38	0.69	1.03	1.40	1.81
220	-0.83	-0.71	-0.56	-0.38	-0.16	0.08	0.36	0.67	1.01	1.38	1.79
225	-0.84	-0.72	-0.57	-0.39	-0.18	0.06	0.34	0.64	0.98	1.35	1.75
230	-0.84	-0.73	-0.59	-0.41	-0.20	0.03	0.30	0.61	0.94	1.31	1.70
235	-0.84	-0.73	-0.60	-0.43	-0.23	0.00	0.27	0.56	0.89	1.25	1.64
240	-0.83	-0.74	-0.61	-0.45	-0.25	-0.03	0.23	0.51	0.83	1.19	1.57
245	-0.82	-0.74	-0.62	-0.47	-0.28	-0.07	0.18	0.46	0.77	1.11	1.49
250	-0.81	-0.73	-0.62	-0.48	-0.31	-0.11	0.13	0.40	0.70	1.03	1.40
255	-0.79	-0.73	-0.63	-0.50	-0.34	-0.14	0.08	0.34	0.63	0.95	1.30
260	-0.77	-0.72	-0.63	-0.52	-0.37	-0.18	0.03	0.27	0.55	0.86	1.20
265	-0.75	-0.71	-0.64	-0.53	-0.39	-0.22	-0.02	0.21	0.47	0.77	1.10
270	-0.72	-0.70	-0.64	-0.54	-0.42	-0.26	-0.08	0.14	0.39	0.68	0.99
275	-0.69	-0.68	-0.63	-0.55	-0.44	-0.30	-0.13	0.08	0.32	0.59	0.89
280	-0.66	-0.66	-0.63	-0.56	-0.46	-0.34	-0.18	0.02	0.24	0.50	0.79
285	-0.63	-0.64	-0.62	-0.57	-0.48	-0.37	-0.22	-0.04	0.17	0.41	0.69
290	-0.59	-0.62	-0.61	-0.57	-0.50	-0.40	-0.26	-0.10	0.10	0.33	0.59
295	-0.55	-0.59	-0.59	-0.57	-0.51	-0.42	-0.30	-0.15	0.04	0.25	0.50
300	-0.51	-0.56	-0.58	-0.56	-0.52	-0.44	-0.33	-0.19	-0.02	0.19	0.42
305	-0.47	-0.53	-0.56	-0.56	-0.52	-0.46	-0.36	-0.23	-0.07	0.12	0.35
310	-0.43	-0.50	-0.54	-0.55	-0.52	-0.47	-0.38	-0.26	-0.11	0.07	0.28
315	-0.38	-0.47	-0.52	-0.54	-0.52	-0.48	-0.40	-0.29	-0.15	0.02	0.22
320	-0.34	-0.43	-0.50	-0.52	-0.52	-0.49	-0.42	-0.32	-0.19	-0.03	0.17
325	-0.30	-0.40	-0.47	-0.51	-0.52	-0.49	-0.43	-0.34	-0.22	-0.07	0.12
330	-0.26	-0.37	-0.45	-0.49	-0.51	-0.49	-0.44	-0.36	-0.25	-0.11	0.07
335	-0.22	-0.33	-0.42	-0.48	-0.50	-0.49	-0.45	-0.38	-0.28	-0.14	0.03
340	-0.17	-0.30	-0.40	-0.46	-0.49	-0.49	-0.46	-0.39	-0.30	-0.17	-0.01
345	-0.13	-0.26	-0.37	-0.44	-0.48	-0.48	-0.46	-0.40	-0.32	-0.20	-0.04
350	-0.09	-0.23	-0.34	-0.42	-0.46	-0.48	-0.46	-0.41	-0.33	-0.22	-0.07
355	-0.04	-0.19	-0.31	-0.40	-0.45	-0.47	-0.46	-0.42	-0.35	-0.24	-0.10
360	0.00	-0.16	-0.28	-0.37	-0.43	-0.46	-0.46	-0.42	-0.36	-0.26	-0.13
365	0.05	-0.12	-0.25	-0.35	-0.42	-0.45	-0.45	-0.43	-0.37	-0.28	-0.15
370	0.09	-0.08	-0.22	-0.32	-0.40	-0.44	-0.45	-0.43	-0.38	-0.29	-0.17
375	0.14	-0.04	-0.18	-0.30	-0.38	-0.43	-0.44	-0.43	-0.38	-0.30	-0.19
380	0.18	0.00	-0.15	-0.27	-0.36	-0.41	-0.44	-0.43	-0.39	-0.32	-0.21
385	0.23	0.04	-0.12	-0.24	-0.34	-0.40	-0.43	-0.43	-0.40	-0.33	-0.23
390	0.28	0.08	-0.08	-0.22	-0.32	-0.39	-0.42	-0.43	-0.40	-0.34	-0.25
395	0.33	0.12	-0.05	-0.19	-0.29	-0.37	-0.41	-0.43	-0.41	-0.36	-0.27
400	0.38	0.17	-0.01	-0.16	-0.27	-0.36	-0.41	-0.43	-0.41	-0.37	-0.29

405	0.43	0.21	0.02	-0.13	-0.25	-0.34	-0.40	-0.42	-0.42	-0.38	-0.31
410	0.48	0.25	0.06	-0.10	-0.23	-0.33	-0.39	-0.42	-0.43	-0.40	-0.33
415	0.53	0.30	0.10	-0.07	-0.21	-0.31	-0.38	-0.43	-0.43	-0.41	-0.36
420	0.58	0.34	0.13	-0.04	-0.19	-0.30	-0.38	-0.43	-0.44	-0.43	-0.38
425	0.63	0.38	0.17	-0.01	-0.16	-0.28	-0.37	-0.43	-0.45	-0.44	-0.40
430	0.68	0.43	0.21	0.02	-0.14	-0.27	-0.37	-0.43	-0.46	-0.46	-0.43
435	0.74	0.47	0.24	0.04	-0.12	-0.26	-0.36	-0.43	-0.47	-0.48	-0.46
440	0.79	0.52	0.28	0.07	-0.10	-0.24	-0.36	-0.44	-0.48	-0.50	-0.48
445	0.84	0.56	0.32	0.10	-0.08	-0.23	-0.35	-0.44	-0.49	-0.52	-0.51
450	0.89	0.61	0.35	0.13	-0.06	-0.22	-0.35	-0.44	-0.51	-0.54	-0.54
455	0.95	0.65	0.39	0.16	-0.04	-0.21	-0.34	-0.45	-0.52	-0.56	-0.56
460	1.00	0.70	0.43	0.19	-0.02	-0.19	-0.34	-0.45	-0.53	-0.58	-0.59
465	1.06	0.74	0.47	0.22	0.00	-0.18	-0.33	-0.45	-0.54	-0.60	-0.62
470	1.11	0.79	0.50	0.25	0.02	-0.17	-0.33	-0.46	-0.55	-0.62	-0.65
475	1.16	0.84	0.54	0.28	0.04	-0.16	-0.32	-0.46	-0.56	-0.64	-0.68
480	1.22	0.88	0.58	0.31	0.07	-0.14	-0.32	-0.46	-0.58	-0.66	-0.71
485	1.27	0.93	0.62	0.34	0.09	-0.13	-0.31	-0.47	-0.59	-0.68	-0.74
490	1.33	0.98	0.65	0.37	0.11	-0.12	-0.31	-0.47	-0.60	-0.70	-0.76
495	1.38	1.02	0.69	0.40	0.13	-0.10	-0.30	-0.47	-0.61	-0.72	-0.79
500	1.44	1.07	0.73	0.43	0.15	-0.09	-0.30	-0.48	-0.62	-0.74	-0.82

\*\*\*\*\* MEMBER NO. 5 \*\*\*\*\*

	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9	1.0
100	-0.14	-0.22	-0.29	-0.37	-0.44	-0.52	-0.59	-0.67	-0.74	-0.82	-0.89
105	-0.14	-0.22	-0.29	-0.37	-0.44	-0.52	-0.59	-0.67	-0.75	-0.82	-0.90
110	-0.14	-0.22	-0.29	-0.37	-0.44	-0.52	-0.59	-0.67	-0.74	-0.82	-0.90
115	-0.14	-0.21	-0.29	-0.36	-0.44	-0.51	-0.59	-0.67	-0.74	-0.82	-0.89
120	-0.13	-0.21	-0.28	-0.36	-0.43	-0.51	-0.58	-0.66	-0.74	-0.81	-0.89
125	-0.12	-0.20	-0.27	-0.35	-0.42	-0.50	-0.58	-0.65	-0.73	-0.80	-0.88
130	-0.10	-0.18	-0.26	-0.33	-0.41	-0.49	-0.56	-0.64	-0.72	-0.79	-0.87
135	-0.08	-0.15	-0.23	-0.31	-0.39	-0.47	-0.55	-0.63	-0.70	-0.78	-0.86
140	-0.04	-0.12	-0.20	-0.28	-0.37	-0.45	-0.53	-0.61	-0.69	-0.77	-0.85
145	0.00	-0.08	-0.17	-0.25	-0.33	-0.42	-0.50	-0.59	-0.67	-0.75	-0.84
150	0.06	-0.03	-0.12	-0.21	-0.30	-0.38	-0.47	-0.56	-0.65	-0.74	-0.83
155	0.13	0.03	-0.06	-0.16	-0.25	-0.34	-0.44	-0.53	-0.63	-0.72	-0.82
160	0.21	0.11	0.01	-0.09	-0.20	-0.30	-0.40	-0.50	-0.60	-0.70	-0.81
165	0.31	0.20	0.09	-0.02	-0.13	-0.24	-0.35	-0.47	-0.58	-0.69	-0.80
170	0.43	0.30	0.18	0.06	-0.06	-0.18	-0.30	-0.43	-0.55	-0.67	-0.79
175	0.56	0.43	0.29	0.16	0.02	-0.11	-0.25	-0.38	-0.52	-0.65	-0.79
180	0.71	0.57	0.42	0.27	0.12	-0.03	-0.18	-0.33	-0.48	-0.63	-0.78
185	0.89	0.72	0.56	0.39	0.22	0.05	-0.11	-0.28	-0.45	-0.62	-0.78
190	1.09	0.90	0.71	0.53	0.34	0.15	-0.04	-0.22	-0.41	-0.60	-0.79
195	1.31	1.10	0.89	0.68	0.47	0.26	0.05	-0.16	-0.37	-0.58	-0.79
200	1.56	1.32	1.09	0.85	0.61	0.38	0.14	-0.09	-0.33	-0.57	-0.80
205	1.20	1.57	1.31	1.04	0.78	0.51	0.25	-0.02	-0.28	-0.55	-0.82
210	0.88	1.86	1.56	1.26	0.96	0.67	0.37	0.07	-0.23	-0.53	-0.83
215	0.60	1.54	1.84	1.51	1.17	0.84	0.50	0.17	-0.16	-0.50	-0.83
220	0.34	1.25	2.15	1.77	1.40	1.03	0.66	0.29	-0.08	-0.46	-0.83
225	0.12	0.98	1.84	2.07	1.66	1.24	0.83	0.42	0.01	-0.41	-0.82
230	-0.07	0.75	1.57	2.38	1.93	1.48	1.02	0.57	0.11	-0.34	-0.80
235	-0.24	0.54	1.31	2.09	2.23	1.73	1.23	0.73	0.23	-0.27	-0.76
240	-0.38	0.35	1.08	1.81	2.54	2.00	1.46	0.91	0.37	-0.17	-0.72
245	-0.49	0.19	0.87	1.56	2.24	2.29	1.70	1.11	0.52	-0.07	-0.65
250	-0.59	0.05	0.69	1.32	1.96	2.60	1.97	1.33	0.70	0.06	-0.57
255	-0.67	-0.07	0.52	1.11	1.70	2.30	2.25	1.57	0.89	0.21	-0.47
260	-0.73	-0.18	0.37	0.92	1.46	2.01	2.56	1.83	1.10	0.38	-0.35
265	-0.77	-0.27	0.24	0.74	1.24	1.74	2.25	2.11	1.34	0.57	-0.20
270	-0.80	-0.34	0.12	0.58	1.04	1.50	1.96	2.41	1.60	0.79	-0.03
275	-0.81	-0.40	0.02	0.44	0.85	1.27	1.69	2.10	1.88	1.03	0.17
280	-0.82	-0.44	-0.07	0.31	0.69	1.06	1.44	1.82	2.19	1.30	0.40
285	-0.82	-0.48	-0.14	0.20	0.54	0.88	1.22	1.56	1.90	1.60	0.66
290	-0.81	-0.51	-0.20	0.10	0.41	0.71	1.02	1.32	1.62	1.93	0.96
295	-0.80	-0.53	-0.25	0.02	0.29	0.56	0.84	1.11	1.38	1.65	1.29
300	-0.78	-0.54	-0.29	-0.05	0.19	0.44	0.68	0.93	1.17	1.41	1.66

305	-0.77	-0.55	-0.33	-0.11	0.11	0.33	0.55	0.76	0.98	1.20	1.42
310	-0.76	-0.56	-0.36	-0.17	0.03	0.23	0.42	0.62	0.82	1.02	1.21
315	-0.75	-0.57	-0.40	-0.22	-0.04	0.14	0.32	0.49	0.67	0.85	1.03
320	-0.75	-0.59	-0.43	-0.27	-0.10	0.06	0.22	0.38	0.54	0.70	0.86
325	-0.75	-0.60	-0.45	-0.31	-0.16	-0.01	0.13	0.28	0.43	0.58	0.72
330	-0.75	-0.62	-0.48	-0.35	-0.21	-0.08	0.06	0.20	0.33	0.47	0.60
335	-0.76	-0.63	-0.50	-0.38	-0.25	-0.13	0.00	0.12	0.25	0.37	0.50
340	-0.76	-0.64	-0.53	-0.41	-0.29	-0.18	-0.06	0.06	0.18	0.29	0.41
345	-0.77	-0.66	-0.55	-0.44	-0.33	-0.21	-0.10	0.01	0.12	0.23	0.34
350	-0.77	-0.67	-0.56	-0.46	-0.35	-0.25	-0.14	-0.04	0.07	0.17	0.28
355	-0.78	-0.68	-0.58	-0.48	-0.38	-0.28	-0.17	-0.07	0.03	0.13	0.23
360	-0.79	-0.69	-0.59	-0.49	-0.40	-0.30	-0.20	-0.10	0.00	0.09	0.19
365	-0.79	-0.70	-0.60	-0.51	-0.41	-0.31	-0.22	-0.12	-0.03	0.07	0.16
370	-0.80	-0.70	-0.61	-0.52	-0.42	-0.33	-0.23	-0.14	-0.05	0.05	0.14
375	-0.80	-0.71	-0.62	-0.52	-0.43	-0.34	-0.25	-0.15	-0.06	0.03	0.12
380	-0.80	-0.71	-0.62	-0.53	-0.44	-0.35	-0.25	-0.16	-0.07	0.02	0.11
385	-0.80	-0.71	-0.62	-0.53	-0.44	-0.35	-0.26	-0.17	-0.08	0.01	0.10
390	-0.79	-0.70	-0.62	-0.53	-0.44	-0.35	-0.27	-0.18	-0.09	0.00	0.08
395	-0.78	-0.70	-0.61	-0.53	-0.44	-0.36	-0.27	-0.19	-0.10	-0.01	0.07
400	-0.77	-0.69	-0.61	-0.52	-0.44	-0.36	-0.28	-0.19	-0.11	-0.03	0.05
405	-0.75	-0.68	-0.60	-0.52	-0.44	-0.36	-0.28	-0.20	-0.12	-0.04	0.03
410	-0.74	-0.66	-0.59	-0.51	-0.44	-0.36	-0.29	-0.22	-0.14	-0.07	0.01
415	-0.72	-0.65	-0.58	-0.51	-0.44	-0.37	-0.30	-0.23	-0.16	-0.09	-0.02
420	-0.69	-0.63	-0.57	-0.50	-0.44	-0.37	-0.31	-0.25	-0.18	-0.12	-0.06
425	-0.67	-0.61	-0.55	-0.50	-0.44	-0.38	-0.32	-0.27	-0.21	-0.15	-0.09
430	-0.64	-0.59	-0.54	-0.49	-0.44	-0.39	-0.34	-0.29	-0.24	-0.19	-0.13
435	-0.62	-0.57	-0.53	-0.48	-0.44	-0.40	-0.35	-0.31	-0.27	-0.22	-0.18
440	-0.59	-0.55	-0.51	-0.48	-0.44	-0.41	-0.37	-0.33	-0.30	-0.26	-0.23
445	-0.56	-0.53	-0.50	-0.47	-0.44	-0.42	-0.39	-0.36	-0.33	-0.30	-0.28
450	-0.52	-0.50	-0.48	-0.46	-0.44	-0.43	-0.41	-0.39	-0.37	-0.35	-0.33
455	-0.49	-0.48	-0.47	-0.46	-0.45	-0.44	-0.42	-0.41	-0.40	-0.39	-0.38
460	-0.45	-0.45	-0.45	-0.45	-0.45	-0.45	-0.44	-0.44	-0.44	-0.44	-0.44
465	-0.42	-0.42	-0.43	-0.44	-0.45	-0.46	-0.46	-0.47	-0.48	-0.49	-0.49
470	-0.38	-0.40	-0.41	-0.43	-0.45	-0.47	-0.48	-0.50	-0.52	-0.53	-0.55
475	-0.34	-0.37	-0.39	-0.42	-0.45	-0.47	-0.50	-0.53	-0.56	-0.58	-0.61
480	-0.30	-0.34	-0.37	-0.41	-0.45	-0.48	-0.52	-0.56	-0.59	-0.63	-0.67
485	-0.26	-0.31	-0.35	-0.40	-0.45	-0.49	-0.54	-0.59	-0.63	-0.68	-0.72
490	-0.22	-0.28	-0.33	-0.39	-0.44	-0.50	-0.56	-0.61	-0.67	-0.73	-0.78
495	-0.18	-0.24	-0.31	-0.38	-0.44	-0.51	-0.57	-0.64	-0.71	-0.77	-0.84
500	-0.14	-0.21	-0.29	-0.36	-0.44	-0.51	-0.59	-0.67	-0.74	-0.82	-0.89

\*\*\*\*\* MEMBER NO. 6 \*\*\*\*\*

	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9	1.0
100	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
105	-0.06	-0.05	-0.04	-0.03	-0.02	0.00	0.01	0.02	0.03	0.05	0.06
110	-0.13	-0.10	-0.08	-0.05	-0.03	-0.01	0.02	0.04	0.07	0.09	0.11
115	-0.18	-0.15	-0.11	-0.08	-0.04	-0.01	0.03	0.06	0.10	0.13	0.17
120	-0.24	-0.20	-0.15	-0.10	-0.06	-0.01	0.03	0.08	0.13	0.17	0.22
125	-0.30	-0.24	-0.18	-0.13	-0.07	-0.01	0.04	0.10	0.16	0.21	0.27
130	-0.35	-0.29	-0.22	-0.15	-0.08	-0.02	0.05	0.12	0.18	0.25	0.32
135	-0.40	-0.33	-0.25	-0.17	-0.10	-0.02	0.06	0.14	0.21	0.29	0.37
140	-0.45	-0.37	-0.28	-0.19	-0.11	-0.02	0.07	0.15	0.24	0.33	0.41
145	-0.50	-0.41	-0.31	-0.21	-0.12	-0.02	0.07	0.17	0.26	0.36	0.46
150	-0.55	-0.44	-0.34	-0.23	-0.13	-0.02	0.08	0.19	0.29	0.39	0.50
155	-0.59	-0.48	-0.36	-0.25	-0.14	-0.02	0.09	0.20	0.31	0.43	0.54
160	-0.63	-0.51	-0.39	-0.27	-0.15	-0.02	0.10	0.22	0.34	0.46	0.58
165	-0.67	-0.54	-0.41	-0.28	-0.15	-0.02	0.10	0.23	0.36	0.49	0.62
170	-0.70	-0.57	-0.43	-0.29	-0.16	-0.02	0.11	0.25	0.38	0.52	0.66
175	-0.73	-0.59	-0.45	-0.31	-0.16	-0.02	0.12	0.26	0.41	0.55	0.69
180	-0.76	-0.62	-0.47	-0.32	-0.17	-0.02	0.13	0.28	0.43	0.58	0.73
185	-0.79	-0.64	-0.48	-0.33	-0.17	-0.02	0.14	0.30	0.45	0.61	0.76
190	-0.82	-0.66	-0.49	-0.33	-0.17	-0.01	0.15	0.31	0.47	0.63	0.79
195	-0.84	-0.67	-0.50	-0.34	-0.17	-0.01	0.16	0.33	0.49	0.66	0.83
200	-0.86	-0.69	-0.51	-0.34	-0.17	0.00	0.17	0.34	0.52	0.69	0.86



205	-0.87	-0.69	-0.52	-0.34	-0.17	0.01	0.18	0.36	0.54	0.71	0.89
210	-0.88	-0.70	-0.52	-0.34	-0.16	0.02	0.20	0.37	0.55	0.73	0.91
215	-0.87	-0.69	-0.51	-0.33	-0.15	0.03	0.21	0.39	0.57	0.75	0.93
220	-0.86	-0.68	-0.50	-0.32	-0.14	0.04	0.22	0.40	0.58	0.76	0.94
225	-0.85	-0.67	-0.49	-0.31	-0.13	0.05	0.23	0.40	0.58	0.76	0.94
230	-0.83	-0.65	-0.47	-0.30	-0.12	0.06	0.23	0.41	0.59	0.76	0.94
235	-0.80	-0.62	-0.45	-0.28	-0.11	0.07	0.24	0.41	0.58	0.76	0.93
240	-0.76	-0.60	-0.43	-0.26	-0.09	0.07	0.24	0.41	0.58	0.74	0.91
245	-0.72	-0.56	-0.40	-0.24	-0.08	0.08	0.24	0.40	0.56	0.72	0.88
250	-0.68	-0.52	-0.37	-0.22	-0.07	0.09	0.24	0.39	0.55	0.70	0.85
255	-0.63	-0.48	-0.34	-0.20	-0.05	0.09	0.23	0.38	0.52	0.67	0.81
260	-0.57	-0.44	-0.31	-0.17	-0.04	0.09	0.23	0.36	0.49	0.63	0.76
265	-0.51	-0.39	-0.27	-0.15	-0.03	0.09	0.21	0.34	0.46	0.58	0.70
270	-0.45	-0.34	-0.23	-0.13	-0.02	0.09	0.20	0.31	0.41	0.52	0.63
275	-0.38	-0.29	-0.20	-0.10	-0.01	0.08	0.18	0.27	0.36	0.46	0.55
280	-0.31	-0.23	-0.16	-0.08	0.00	0.08	0.15	0.23	0.31	0.38	0.46
285	-0.24	-0.18	-0.12	-0.06	0.00	0.06	0.12	0.18	0.24	0.30	0.36
290	-0.16	-0.12	-0.08	-0.04	0.00	0.05	0.09	0.13	0.17	0.21	0.25
295	-0.08	-0.06	-0.04	-0.02	0.00	0.03	0.05	0.07	0.09	0.11	0.13
300	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
305	0.08	0.06	0.04	0.02	0.00	-0.03	-0.05	-0.07	-0.09	-0.11	-0.13
310	0.16	0.12	0.08	0.04	0.00	-0.05	-0.09	-0.13	-0.17	-0.21	-0.25
315	0.24	0.18	0.12	0.06	0.00	-0.06	-0.12	-0.18	-0.24	-0.30	-0.36
320	0.31	0.23	0.16	0.08	0.00	-0.08	-0.15	-0.23	-0.31	-0.38	-0.46
325	0.38	0.29	0.20	0.10	0.01	-0.08	-0.18	-0.27	-0.36	-0.46	-0.55
330	0.45	0.34	0.23	0.13	0.02	-0.09	-0.20	-0.31	-0.41	-0.52	-0.63
335	0.51	0.39	0.27	0.15	0.03	-0.09	-0.21	-0.34	-0.46	-0.58	-0.70
340	0.57	0.44	0.31	0.17	0.04	-0.09	-0.23	-0.36	-0.49	-0.63	-0.76
345	0.63	0.48	0.34	0.20	0.05	-0.09	-0.23	-0.38	-0.52	-0.67	-0.81
350	0.68	0.52	0.37	0.22	0.07	-0.09	-0.24	-0.39	-0.55	-0.70	-0.85
355	0.72	0.56	0.40	0.24	0.08	-0.08	-0.24	-0.40	-0.56	-0.72	-0.88
360	0.76	0.60	0.43	0.26	0.09	-0.07	-0.24	-0.41	-0.58	-0.74	-0.91
365	0.80	0.62	0.45	0.28	0.11	-0.07	-0.24	-0.41	-0.58	-0.76	-0.93
370	0.83	0.65	0.47	0.30	0.12	-0.06	-0.23	-0.41	-0.59	-0.76	-0.94
375	0.85	0.67	0.49	0.31	0.13	-0.05	-0.23	-0.40	-0.58	-0.76	-0.94
380	0.86	0.68	0.50	0.32	0.14	-0.04	-0.22	-0.40	-0.58	-0.76	-0.94
385	0.87	0.69	0.51	0.33	0.15	-0.03	-0.21	-0.39	-0.57	-0.75	-0.93
390	0.88	0.70	0.52	0.34	0.16	-0.02	-0.20	-0.37	-0.55	-0.73	-0.91
395	0.87	0.69	0.52	0.34	0.17	-0.01	-0.18	-0.36	-0.54	-0.71	-0.89
400	0.86	0.69	0.51	0.34	0.17	0.00	-0.17	-0.34	-0.52	-0.69	-0.86
405	0.84	0.67	0.50	0.34	0.17	0.01	-0.16	-0.33	-0.49	-0.66	-0.83
410	0.82	0.66	0.49	0.33	0.17	0.01	-0.15	-0.31	-0.47	-0.63	-0.79
415	0.79	0.64	0.48	0.33	0.17	0.02	-0.14	-0.30	-0.45	-0.61	-0.76
420	0.76	0.62	0.47	0.32	0.17	0.02	-0.13	-0.28	-0.43	-0.58	-0.73
425	0.73	0.59	0.45	0.31	0.16	0.02	-0.12	-0.26	-0.41	-0.55	-0.69
430	0.70	0.57	0.43	0.29	0.16	0.02	-0.11	-0.25	-0.38	-0.52	-0.66
435	0.67	0.54	0.41	0.28	0.15	0.02	-0.10	-0.23	-0.36	-0.49	-0.62
440	0.63	0.51	0.39	0.27	0.15	0.02	-0.10	-0.22	-0.34	-0.46	-0.58
445	0.59	0.48	0.36	0.25	0.14	0.02	-0.09	-0.20	-0.31	-0.43	-0.54
450	0.55	0.44	0.34	0.23	0.13	0.02	-0.08	-0.19	-0.29	-0.39	-0.50
455	0.50	0.41	0.31	0.21	0.12	0.02	-0.07	-0.17	-0.26	-0.36	-0.46
460	0.45	0.37	0.28	0.19	0.11	0.02	-0.07	-0.15	-0.24	-0.33	-0.41
465	0.40	0.33	0.25	0.17	0.10	0.02	-0.06	-0.14	-0.21	-0.29	-0.37
470	0.35	0.29	0.22	0.15	0.08	0.02	-0.05	-0.12	-0.18	-0.25	-0.32
475	0.30	0.24	0.18	0.13	0.07	0.01	-0.04	-0.10	-0.16	-0.21	-0.27
480	0.24	0.20	0.15	0.10	0.06	0.01	-0.03	-0.08	-0.13	-0.17	-0.22
485	0.18	0.15	0.11	0.08	0.04	0.01	-0.03	-0.06	-0.10	-0.13	-0.17
490	0.13	0.10	0.08	0.05	0.03	0.01	-0.02	-0.04	-0.07	-0.09	-0.11
495	0.06	0.05	0.04	0.03	0.02	0.00	-0.01	-0.02	-0.03	-0.05	-0.06
500	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

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MEMBER NO. 7

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	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9	1.0
100	0.18	-0.04	-0.24	-0.40	-0.53	-0.63	-0.70	-0.74	-0.74	-0.71	-0.66

105	0.30	0.06	-0.15	-0.33	-0.48	-0.59	-0.68	-0.73	-0.75	-0.74	-0.69
110	0.43	0.17	-0.06	-0.25	-0.42	-0.55	-0.65	-0.71	-0.75	-0.75	-0.73
115	0.55	0.28	0.04	-0.17	-0.35	-0.50	-0.61	-0.70	-0.75	-0.77	-0.76
120	0.68	0.39	0.14	-0.09	-0.29	-0.45	-0.58	-0.68	-0.75	-0.78	-0.79
125	0.81	0.51	0.23	-0.01	-0.22	-0.40	-0.54	-0.66	-0.74	-0.79	-0.81
130	0.94	0.62	0.33	0.07	-0.15	-0.34	-0.51	-0.64	-0.73	-0.80	-0.84
135	1.07	0.73	0.43	0.16	-0.08	-0.29	-0.47	-0.61	-0.72	-0.81	-0.85
140	1.19	0.84	0.52	0.24	-0.02	-0.24	-0.43	-0.58	-0.71	-0.81	-0.87
145	1.31	0.94	0.62	0.32	0.05	-0.18	-0.39	-0.56	-0.70	-0.80	-0.88
150	1.42	1.04	0.70	0.39	0.12	-0.13	-0.34	-0.53	-0.68	-0.79	-0.88
155	1.52	1.14	0.78	0.47	0.18	-0.08	-0.30	-0.49	-0.65	-0.78	-0.88
160	1.61	1.22	0.86	0.53	0.24	-0.03	-0.26	-0.46	-0.63	-0.77	-0.87
165	1.69	1.30	0.93	0.59	0.29	0.02	-0.22	-0.43	-0.60	-0.75	-0.86
170	1.77	1.36	0.99	0.65	0.34	0.07	-0.18	-0.39	-0.57	-0.72	-0.84
175	1.82	1.42	1.04	0.70	0.39	0.11	-0.14	-0.35	-0.54	-0.69	-0.81
180	1.86	1.46	1.08	0.74	0.43	0.15	-0.10	-0.32	-0.50	-0.65	-0.77
185	1.89	1.49	1.11	0.77	0.46	0.18	-0.06	-0.28	-0.46	-0.61	-0.73
190	1.90	1.50	1.13	0.79	0.49	0.21	-0.03	-0.24	-0.42	-0.57	-0.68
195	1.89	1.50	1.13	0.80	0.50	0.24	0.00	-0.20	-0.37	-0.51	-0.62
200	1.86	1.48	1.12	0.80	0.51	0.26	0.03	-0.16	-0.32	-0.45	-0.55
205	1.81	1.44	1.10	0.79	0.52	0.27	0.06	-0.12	-0.27	-0.38	-0.47
210	1.74	1.39	1.06	0.77	0.51	0.29	0.09	-0.07	-0.20	-0.30	-0.37
215	1.65	1.32	1.02	0.75	0.51	0.30	0.12	-0.02	-0.13	-0.21	-0.26
220	1.56	1.24	0.96	0.71	0.50	0.31	0.16	0.04	-0.05	-0.11	-0.14
225	1.44	1.16	0.90	0.68	0.48	0.32	0.19	0.10	0.03	0.00	0.00
230	1.32	1.06	0.83	0.63	0.47	0.33	0.23	0.16	0.12	0.11	0.14
235	1.19	0.96	0.76	0.59	0.45	0.34	0.27	0.22	0.21	0.23	0.29
240	1.05	0.85	0.68	0.53	0.43	0.35	0.30	0.29	0.31	0.36	0.44
245	0.91	0.73	0.59	0.48	0.40	0.35	0.34	0.35	0.40	0.48	0.59
250	0.76	0.62	0.51	0.42	0.37	0.36	0.37	0.42	0.49	0.60	0.75
255	0.62	0.50	0.42	0.37	0.35	0.36	0.40	0.48	0.59	0.73	0.90
260	0.47	0.38	0.33	0.31	0.32	0.36	0.43	0.54	0.68	0.85	1.05
265	0.33	0.27	0.24	0.25	0.29	0.36	0.46	0.60	0.76	0.96	1.19
270	0.19	0.16	0.16	0.19	0.26	0.36	0.49	0.65	0.84	1.07	1.33
275	0.05	0.05	0.08	0.14	0.23	0.36	0.51	0.70	0.92	1.17	1.45
280	-0.07	-0.05	0.00	0.09	0.20	0.35	0.53	0.74	0.99	1.26	1.57
285	-0.19	-0.14	-0.07	0.04	0.17	0.34	0.55	0.78	1.04	1.34	1.67
290	-0.29	-0.23	-0.14	-0.01	0.15	0.34	0.56	0.81	1.09	1.41	1.76
295	-0.38	-0.30	-0.19	-0.05	0.12	0.33	0.56	0.83	1.13	1.46	1.83
300	-0.45	-0.36	-0.24	-0.09	0.10	0.31	0.56	0.84	1.16	1.50	1.88
305	-0.51	-0.42	-0.28	-0.12	0.07	0.30	0.56	0.85	1.17	1.52	1.91
310	-0.57	-0.46	-0.32	-0.16	0.05	0.28	0.54	0.84	1.17	1.53	1.92
315	-0.61	-0.50	-0.36	-0.19	0.02	0.25	0.52	0.82	1.15	1.51	1.91
320	-0.64	-0.54	-0.39	-0.22	-0.02	0.22	0.49	0.79	1.12	1.48	1.88
325	-0.67	-0.56	-0.42	-0.25	-0.05	0.18	0.45	0.75	1.08	1.44	1.83
330	-0.69	-0.59	-0.45	-0.29	-0.09	0.14	0.41	0.70	1.03	1.39	1.77
335	-0.70	-0.61	-0.48	-0.32	-0.12	0.10	0.36	0.65	0.97	1.32	1.70
340	-0.71	-0.62	-0.50	-0.35	-0.16	0.06	0.30	0.59	0.90	1.24	1.62
345	-0.71	-0.63	-0.52	-0.38	-0.20	0.01	0.25	0.52	0.82	1.16	1.52
350	-0.71	-0.64	-0.54	-0.40	-0.24	-0.04	0.19	0.45	0.74	1.07	1.42
355	-0.70	-0.64	-0.55	-0.43	-0.27	-0.09	0.13	0.38	0.66	0.97	1.31
360	-0.68	-0.64	-0.56	-0.45	-0.31	-0.14	0.07	0.30	0.57	0.87	1.20
365	-0.67	-0.63	-0.57	-0.47	-0.35	-0.19	0.00	0.23	0.48	0.77	1.08
370	-0.64	-0.63	-0.58	-0.49	-0.38	-0.24	-0.06	0.15	0.39	0.66	0.97
375	-0.62	-0.61	-0.58	-0.51	-0.41	-0.28	-0.12	0.07	0.30	0.56	0.85
380	-0.59	-0.60	-0.58	-0.53	-0.44	-0.33	-0.18	0.00	0.21	0.45	0.73
385	-0.56	-0.59	-0.58	-0.54	-0.47	-0.37	-0.24	-0.07	0.13	0.35	0.61
390	-0.53	-0.57	-0.58	-0.55	-0.50	-0.41	-0.29	-0.14	0.04	0.26	0.50
395	-0.49	-0.55	-0.57	-0.56	-0.52	-0.44	-0.34	-0.20	-0.03	0.17	0.40
400	-0.46	-0.53	-0.56	-0.56	-0.54	-0.47	-0.38	-0.26	-0.10	0.09	0.31
405	-0.43	-0.50	-0.55	-0.57	-0.55	-0.50	-0.42	-0.31	-0.17	0.01	0.22
410	-0.39	-0.48	-0.54	-0.57	-0.56	-0.53	-0.46	-0.36	-0.22	-0.06	0.14
415	-0.36	-0.46	-0.53	-0.57	-0.57	-0.55	-0.49	-0.40	-0.28	-0.12	0.06
420	-0.33	-0.44	-0.52	-0.57	-0.58	-0.57	-0.52	-0.44	-0.33	-0.18	-0.01
425	-0.29	-0.42	-0.51	-0.56	-0.59	-0.58	-0.54	-0.48	-0.37	-0.24	-0.08
430	-0.26	-0.39	-0.49	-0.56	-0.59	-0.60	-0.57	-0.51	-0.42	-0.29	-0.14

435	-0.23	-0.37	-0.48	-0.55	-0.60	-0.61	-0.59	-0.54	-0.45	-0.34	-0.19
440	-0.20	-0.35	-0.46	-0.55	-0.60	-0.62	-0.61	-0.56	-0.49	-0.38	-0.24
445	-0.17	-0.33	-0.45	-0.54	-0.60	-0.63	-0.62	-0.59	-0.52	-0.42	-0.29
450	-0.14	-0.30	-0.43	-0.53	-0.60	-0.64	-0.64	-0.61	-0.55	-0.46	-0.34
455	-0.11	-0.28	-0.42	-0.52	-0.60	-0.64	-0.65	-0.63	-0.58	-0.49	-0.38
460	-0.08	-0.26	-0.40	-0.51	-0.60	-0.64	-0.66	-0.65	-0.60	-0.52	-0.41
465	-0.05	-0.23	-0.38	-0.50	-0.59	-0.65	-0.67	-0.66	-0.62	-0.55	-0.45
470	-0.02	-0.21	-0.37	-0.49	-0.59	-0.65	-0.68	-0.68	-0.64	-0.58	-0.48
475	0.01	-0.18	-0.35	-0.48	-0.58	-0.65	-0.69	-0.69	-0.66	-0.61	-0.51
480	0.04	-0.16	-0.33	-0.47	-0.57	-0.65	-0.69	-0.70	-0.68	-0.63	-0.54
485	0.08	-0.13	-0.31	-0.45	-0.57	-0.65	-0.70	-0.71	-0.70	-0.65	-0.57
490	0.11	-0.10	-0.29	-0.44	-0.56	-0.64	-0.70	-0.72	-0.71	-0.67	-0.60
495	0.14	-0.08	-0.27	-0.42	-0.55	-0.64	-0.70	-0.73	-0.73	-0.69	-0.63
500	0.18	-0.05	-0.24	-0.41	-0.54	-0.64	-0.70	-0.74	-0.74	-0.72	-0.66









\*\*\*\*\* MEMBER NO. 4 \*\*\*\*\*

	.0	.1	.2	.3	.4	.5	.6	.7	.8	.9	1.0	A.F.
100	-0.30	-0.28	-0.25	-0.23	-0.20	-0.18	-0.15	-0.13	-0.10	-0.08	-0.05	-0.22
105	-0.28	-0.26	-0.23	-0.21	-0.18	-0.16	-0.13	-0.11	-0.08	-0.06	-0.03	-0.19
110	-0.26	-0.24	-0.21	-0.19	-0.16	-0.14	-0.11	-0.09	-0.06	-0.04	-0.01	-0.16
115	-0.24	-0.22	-0.19	-0.17	-0.14	-0.12	-0.09	-0.07	-0.04	-0.02	0.01	-0.13
120	-0.22	-0.20	-0.17	-0.15	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	-0.10
125	-0.20	-0.17	-0.15	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	-0.08
130	-0.18	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	-0.05
135	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	-0.03
140	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	0.12	-0.01
145	-0.11	-0.08	-0.06	-0.03	-0.01	0.02	0.04	0.07	0.09	0.12	0.14	0.01
150	-0.08	-0.06	-0.03	-0.01	0.02	0.04	0.07	0.09	0.12	0.14	0.17	0.02
155	-0.06	-0.04	-0.01	0.01	0.04	0.06	0.09	0.11	0.14	0.16	0.19	0.04
160	-0.04	-0.02	0.01	0.03	0.06	0.08	0.11	0.13	0.16	0.18	0.21	0.06
165	-0.02	0.00	0.03	0.05	0.08	0.10	0.13	0.15	0.18	0.20	0.23	0.07
170	0.00	0.02	0.05	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.08
175	0.01	0.04	0.06	0.09	0.11	0.14	0.16	0.19	0.21	0.24	0.26	0.09
180	0.03	0.05	0.08	0.10	0.13	0.15	0.18	0.20	0.23	0.25	0.28	0.10
185	0.04	0.07	0.09	0.12	0.14	0.17	0.19	0.22	0.24	0.27	0.29	0.11
190	0.05	0.08	0.10	0.13	0.15	0.18	0.20	0.23	0.25	0.28	0.30	0.11
195	0.06	0.09	0.11	0.14	0.16	0.19	0.21	0.24	0.26	0.29	0.31	0.12
200	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.30	0.32	0.12
205	0.08	0.10	0.13	0.15	0.18	0.20	0.23	0.25	0.28	0.30	0.33	0.12
210	0.08	0.11	0.13	0.16	0.18	0.21	0.23	0.26	0.28	0.31	0.33	0.12
215	0.08	0.11	0.13	0.16	0.18	0.21	0.23	0.26	0.28	0.31	0.33	0.12
220	0.08	0.11	0.13	0.16	0.18	0.21	0.23	0.26	0.28	0.31	0.33	0.13
225	0.08	0.10	0.13	0.15	0.18	0.20	0.23	0.25	0.28	0.30	0.33	0.13
230	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.30	0.32	0.13
235	0.07	0.09	0.12	0.14	0.17	0.19	0.22	0.24	0.27	0.29	0.32	0.13
240	0.06	0.09	0.11	0.14	0.16	0.19	0.21	0.24	0.26	0.29	0.31	0.12
245	0.06	0.08	0.11	0.13	0.16	0.18	0.21	0.23	0.26	0.28	0.31	0.12
250	0.05	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.30	0.12
255	0.04	0.06	0.09	0.11	0.14	0.16	0.19	0.21	0.24	0.26	0.29	0.12
260	0.03	0.06	0.08	0.11	0.13	0.16	0.18	0.21	0.23	0.26	0.28	0.12
265	0.02	0.05	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.11
270	0.01	0.03	0.06	0.08	0.11	0.13	0.16	0.18	0.21	0.23	0.26	0.11
275	0.00	0.02	0.05	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.11
280	-0.01	0.01	0.04	0.06	0.09	0.11	0.14	0.16	0.19	0.21	0.24	0.10
285	-0.02	0.00	0.03	0.05	0.08	0.10	0.13	0.15	0.18	0.20	0.23	0.10
290	-0.03	-0.01	0.02	0.04	0.07	0.09	0.12	0.14	0.17	0.19	0.22	0.09
295	-0.04	-0.02	0.01	0.03	0.06	0.08	0.11	0.13	0.16	0.18	0.21	0.09
300	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	0.12	0.15	0.17	0.20	0.08
305	-0.06	-0.04	-0.01	0.01	0.04	0.06	0.09	0.11	0.14	0.16	0.19	0.08
310	-0.07	-0.04	-0.02	0.01	0.03	0.06	0.08	0.11	0.13	0.16	0.18	0.07
315	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	0.12	0.15	0.17	0.07
320	-0.09	-0.06	-0.04	-0.01	0.01	0.04	0.06	0.09	0.11	0.14	0.16	0.06
325	-0.09	-0.07	-0.04	-0.02	0.01	0.03	0.06	0.08	0.11	0.13	0.16	0.05
330	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.08	0.10	0.13	0.15	0.05
335	-0.11	-0.08	-0.06	-0.03	-0.01	0.02	0.04	0.07	0.09	0.12	0.14	0.04
340	-0.11	-0.09	-0.06	-0.04	-0.01	0.01	0.04	0.06	0.09	0.11	0.14	0.03
345	-0.12	-0.09	-0.07	-0.04	-0.02	0.01	0.03	0.06	0.08	0.11	0.13	0.03
350	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.08	0.10	0.13	0.02
355	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	0.12	0.01
360	-0.14	-0.11	-0.09	-0.06	-0.04	-0.01	0.01	0.04	0.06	0.09	0.11	0.01
365	-0.14	-0.12	-0.09	-0.07	-0.04	-0.02	0.01	0.03	0.06	0.08	0.11	0.00
370	-0.15	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.08	0.10	-0.01
375	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	-0.01
380	-0.16	-0.13	-0.11	-0.08	-0.06	-0.03	-0.01	0.02	0.04	0.07	0.09	-0.02
385	-0.16	-0.14	-0.11	-0.09	-0.06	-0.04	-0.01	0.01	0.04	0.06	0.09	-0.03
390	-0.17	-0.14	-0.12	-0.09	-0.07	-0.04	-0.02	0.01	0.03	0.06	0.08	-0.04
395	-0.17	-0.15	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.08	-0.05
400	-0.18	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	-0.05









105	-0.20	-0.18	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	-0.34
110	-0.22	-0.19	-0.17	-0.14	-0.12	-0.09	-0.07	-0.04	-0.02	0.01	0.03	-0.32
115	-0.23	-0.20	-0.18	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	-0.29
120	-0.24	-0.22	-0.19	-0.17	-0.14	-0.12	-0.09	-0.07	-0.04	-0.02	0.01	-0.26
125	-0.25	-0.23	-0.20	-0.18	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	-0.24
130	-0.26	-0.24	-0.21	-0.19	-0.16	-0.14	-0.11	-0.09	-0.06	-0.04	-0.01	-0.21
135	-0.28	-0.25	-0.23	-0.20	-0.18	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	-0.19
140	-0.29	-0.26	-0.24	-0.21	-0.19	-0.16	-0.14	-0.11	-0.09	-0.06	-0.04	-0.16
145	-0.30	-0.27	-0.25	-0.22	-0.20	-0.17	-0.15	-0.12	-0.10	-0.07	-0.05	-0.14
150	-0.31	-0.28	-0.26	-0.23	-0.21	-0.18	-0.16	-0.13	-0.11	-0.08	-0.06	-0.11
155	-0.31	-0.29	-0.26	-0.24	-0.21	-0.19	-0.16	-0.14	-0.11	-0.09	-0.06	-0.09
160	-0.32	-0.30	-0.27	-0.25	-0.22	-0.20	-0.17	-0.15	-0.12	-0.10	-0.07	-0.07
165	-0.33	-0.30	-0.28	-0.25	-0.23	-0.20	-0.18	-0.15	-0.13	-0.10	-0.08	-0.04
170	-0.33	-0.30	-0.28	-0.25	-0.23	-0.20	-0.18	-0.15	-0.13	-0.10	-0.08	-0.02
175	-0.33	-0.31	-0.28	-0.26	-0.23	-0.21	-0.18	-0.16	-0.13	-0.11	-0.08	0.00
180	-0.33	-0.31	-0.28	-0.26	-0.23	-0.21	-0.18	-0.16	-0.13	-0.11	-0.08	0.02
185	-0.33	-0.31	-0.28	-0.26	-0.23	-0.21	-0.18	-0.16	-0.13	-0.11	-0.08	0.04
190	-0.33	-0.30	-0.28	-0.25	-0.23	-0.20	-0.18	-0.15	-0.13	-0.10	-0.08	0.06
195	-0.32	-0.30	-0.27	-0.25	-0.22	-0.20	-0.17	-0.15	-0.12	-0.10	-0.07	0.08
200	-0.31	-0.29	-0.26	-0.24	-0.21	-0.19	-0.16	-0.14	-0.11	-0.09	-0.06	0.10
205	-0.30	-0.28	-0.25	-0.23	-0.20	-0.18	-0.15	-0.13	-0.10	-0.08	-0.05	0.12
210	-0.29	-0.27	-0.24	-0.22	-0.19	-0.17	-0.14	-0.12	-0.09	-0.07	-0.04	0.14
215	-0.28	-0.25	-0.23	-0.20	-0.18	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	0.16
220	-0.26	-0.23	-0.21	-0.18	-0.16	-0.13	-0.11	-0.08	-0.06	-0.03	-0.01	0.17
225	-0.24	-0.21	-0.19	-0.16	-0.14	-0.11	-0.09	-0.06	-0.04	-0.01	0.01	0.19
230	-0.22	-0.19	-0.17	-0.14	-0.12	-0.09	-0.07	-0.04	-0.02	0.01	0.03	0.20
235	-0.20	-0.17	-0.15	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.21
240	-0.17	-0.15	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.08	0.22
245	-0.15	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.08	0.10	0.23
250	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	0.12	0.23
255	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	0.12	0.15	0.24
260	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	0.12	0.15	0.17	0.24
265	-0.06	-0.03	-0.01	0.02	0.04	0.07	0.09	0.12	0.14	0.17	0.19	0.24
270	-0.04	-0.01	0.01	0.04	0.06	0.09	0.11	0.14	0.16	0.19	0.21	0.24
275	-0.02	0.01	0.03	0.06	0.08	0.11	0.13	0.16	0.18	0.21	0.23	0.24
280	0.00	0.03	0.05	0.08	0.10	0.13	0.15	0.18	0.20	0.23	0.25	0.24
285	0.02	0.05	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.24
290	0.04	0.06	0.09	0.11	0.14	0.16	0.19	0.21	0.24	0.26	0.29	0.23
295	0.05	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.30	0.23
300	0.06	0.08	0.11	0.13	0.16	0.18	0.21	0.23	0.26	0.28	0.31	0.22
305	0.07	0.09	0.12	0.14	0.17	0.19	0.22	0.24	0.27	0.29	0.32	0.21
310	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.30	0.32	0.20
315	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.30	0.32	0.19
320	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.30	0.32	0.18
325	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.30	0.32	0.17
330	0.07	0.09	0.12	0.14	0.17	0.19	0.22	0.24	0.27	0.29	0.32	0.16
335	0.06	0.09	0.11	0.14	0.16	0.19	0.21	0.24	0.26	0.29	0.31	0.15
340	0.06	0.08	0.11	0.13	0.16	0.18	0.21	0.23	0.26	0.28	0.31	0.14
345	0.05	0.08	0.10	0.13	0.15	0.18	0.20	0.23	0.25	0.28	0.30	0.13
350	0.04	0.07	0.09	0.12	0.14	0.17	0.19	0.22	0.24	0.27	0.29	0.11
355	0.03	0.06	0.08	0.11	0.13	0.16	0.18	0.21	0.23	0.26	0.28	0.10
360	0.02	0.05	0.07	0.10	0.12	0.15	0.17	0.20	0.22	0.25	0.27	0.09
365	0.01	0.04	0.06	0.09	0.11	0.14	0.16	0.19	0.21	0.24	0.26	0.08
370	0.00	0.03	0.05	0.08	0.10	0.13	0.15	0.18	0.20	0.23	0.25	0.06
375	-0.01	0.02	0.04	0.07	0.09	0.12	0.14	0.17	0.19	0.22	0.24	0.05
380	-0.02	0.00	0.03	0.05	0.08	0.10	0.13	0.15	0.18	0.20	0.23	0.03
385	-0.03	-0.01	0.02	0.04	0.07	0.09	0.12	0.14	0.17	0.19	0.22	0.02
390	-0.04	-0.02	0.01	0.03	0.06	0.08	0.11	0.13	0.16	0.18	0.21	0.00
395	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	0.12	0.15	0.17	0.20	-0.01
400	-0.06	-0.04	-0.01	0.01	0.04	0.06	0.09	0.11	0.14	0.16	0.19	-0.03
405	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.08	0.10	0.13	0.15	0.18	-0.04
410	-0.08	-0.06	-0.03	-0.01	0.02	0.04	0.07	0.09	0.12	0.14	0.17	-0.06
415	-0.09	-0.07	-0.04	-0.02	0.01	0.03	0.06	0.08	0.11	0.13	0.16	-0.08
420	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	0.12	0.15	-0.09
425	-0.11	-0.08	-0.06	-0.03	-0.01	0.02	0.04	0.07	0.09	0.12	0.14	-0.11
430	-0.11	-0.09	-0.06	-0.04	-0.01	0.01	0.04	0.06	0.09	0.11	0.14	-0.13

435	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.08	0.10	0.13	-0.14
440	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	0.12	-0.16
445	-0.13	-0.11	-0.08	-0.06	-0.03	-0.01	0.02	0.04	0.07	0.09	0.12	-0.18
450	-0.14	-0.12	-0.09	-0.07	-0.04	-0.02	0.01	0.03	0.06	0.08	0.11	-0.19
455	-0.15	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.08	0.10	-0.21
460	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	0.10	-0.23
465	-0.16	-0.13	-0.11	-0.08	-0.06	-0.03	-0.01	0.02	0.04	0.07	0.09	-0.25
470	-0.16	-0.14	-0.11	-0.09	-0.06	-0.04	-0.01	0.01	0.04	0.06	0.09	-0.26
475	-0.17	-0.14	-0.12	-0.09	-0.07	-0.04	-0.02	0.01	0.03	0.06	0.08	-0.28
480	-0.17	-0.15	-0.12	-0.10	-0.07	-0.05	-0.02	0.00	0.03	0.05	0.08	-0.30
485	-0.18	-0.15	-0.13	-0.10	-0.08	-0.05	-0.03	0.00	0.02	0.05	0.07	-0.32
490	-0.18	-0.16	-0.13	-0.11	-0.08	-0.06	-0.03	-0.01	0.02	0.04	0.07	-0.34
495	-0.19	-0.16	-0.14	-0.11	-0.09	-0.06	-0.04	-0.01	0.01	0.04	0.06	-0.35
500	-0.19	-0.17	-0.14	-0.12	-0.09	-0.07	-0.04	-0.02	0.01	0.03	0.06	-0.37



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Add  
18 July 98

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\*\*\* CULVERT DESIGN AND OPTIMIZATION - CUDO \*\*\*  
\*\*\*\*\*

INPUT ECHO

BR#A500 FILE A506LRF4.DAT 4 FT FILL

DESIGN CULVERT FOR GIVEN DIMENSIONS

GROUND ELEVATION 118.00 FT.  
CULVERT BOTTOM SLAB ELEVATION 100.00 FT  
WIDTH OF WATERWAY OPENING 60.00 FT.  
DEPTH OF WATERWAY OPENING 12.00 FT

COEF. OF ACTIVE EARTH PRESSURE .50

CONCENTRATED LOADS (KIPS) 16.00 16.00 4.00  
SPACING OF LOADS (FT.) 14.00 14.00

CONCRETE STRENGTH AT 28 DAYS (PSI) = 3000.0

UNIT PRICES			
CONCRETE	REINF.	WALL FORM	SLAB FORM
\$/CU.YDS	\$/LBS	\$/SQ.FT	\$/SQ.FT
300.00	.95	8.00	8.00

NUMBER OF CELLS 5

TOP SLAB THICKNESS 11.50 IN.  
BOTTOM SLAB THICKNESS 11.50 IN.  
EXTERIOR WALL THICKNESS 9.50 IN.  
INTERIOR WALL THICKNESS 8.00 IN.

GENERAL OPTIMUM DESIGN FOR GIVEN OPENING

NUMBER OF CELLS = 5

WATERWAY OPENING

WIDTH = 60.00 FT.

HEIGHT = 12.00 FT.

SPAN = 12.69 FT.

SLAB THICKNESS

TOP SLAB = 11.50 IN.

BOTTOM SLAB = 11.50 IN.

WALL THICKNESS

EXTERIOR = 9.50 IN.

INTERIOR = 8.00 IN.

NOTE: (\*\*)- AREA & SPACING OF POSITIVE REINFORCEMENT  
ARE BASED ON THE MAXIMUM MOMENT DUE TO DESIGN LOADING,  
1.2 TIMES CRACKING MOMENT OR CRACK CONTROL (Z =98)

TOP SLAB - DETAILS FOR NEGATIVE MOMENT  
OUTSIDE FACE AT SUPPORT

LOCATION	MOMENT FT-KIPS	REQD. REINF.	SUGGESTED SPACING
SPAN 1 LEFT	-19.1	.48	# 4 @ 5
RIGHT	-17.9	.48	# 4 @ 5
SPAN 2 LEFT	-18.2	.48	# 4 @ 5
RIGHT	-16.7	.48	# 4 @ 5
SPAN 3 LEFT	-16.2	.40	# 4 @ 6
RIGHT	-16.2	.40	# 4 @ 6
SPAN 4 LEFT	-16.7	.48	# 4 @ 5
RIGHT	-18.2	.48	# 4 @ 5
SPAN 5 LEFT	-17.9	.48	# 4 @ 5
RIGHT	-19.1	.48	# 4 @ 5

TOP SLAB - DETAILS FOR POSITIVE MOMENT  
INSIDE FACE AT MID SPAN (\*\*)

LOCATION	MOMENT FT-KIPS	REQD. REINF.	SUGGESTED SPACING
SPAN 1	9.5	.40	# 4 @ 6
SPAN 2	10.8	.48	# 4 @ 5
SPAN 3	7.0	.40	# 4 @ 6
SPAN 4	10.8	.48	# 4 @ 5
SPAN 5	9.5	.40	# 4 @ 6



BOTTOM SLAB - DETAILS FOR NEGATIVE MOMENT

INSIDE FACE AT SUPPORT

LOCATION	MOMENT FT-KIPS	REQD. REINF.	SUGGESTED SPACING
SPAN 1 LEFT	-22.5	.74	# 5 @ 5
RIGHT	-19.5	.60	# 4 @ 4
SPAN 2 LEFT	-20.1	.60	# 4 @ 4
RIGHT	-18.9	.60	# 4 @ 4
SPAN 3 LEFT	-18.3	.60	# 4 @ 4
RIGHT	-18.3	.60	# 4 @ 4
SPAN 4 LEFT	-18.9	.60	# 4 @ 4
RIGHT	-20.1	.60	# 4 @ 4
SPAN 5 LEFT	-19.5	.60	# 4 @ 4
RIGHT	-22.5	.74	# 5 @ 5

BOTTOM SLAB - DETAILS FOR POSITIVE MOMENT  
INSIDE FACE AT MID SPAN (\*\*)

LOCATION	MOMENT FT-KIPS	REQD. REINF.	SUGGESTED SPACING
SPAN 1	10.1	.40	# 4 @ 6
SPAN 2	11.9	.48	# 4 @ 5
SPAN 3	8.1	.40	# 4 @ 6
SPAN 4	11.9	.48	# 4 @ 5
SPAN 5	10.1	.40	# 4 @ 6

EXTERIOR WALL DETAILS

LOCATION	MOMENT FT-KIPS	REQD. REINF.	SUGGESTED SPACING
OUTSIDE FACE			
BOTTOM	-22.5	.93	# 5 @ 4
TOP	-19.1	.74	# 5 @ 5
INSIDE FACE (**)			
	8.1	.48	# 4 @ 5

INTERIOR WALL DETAILS

LOCATION	MOMENT FT-KIPS	REQD. REINF.	SUGGESTED SPACING
EACH FACE	-1.3	.17	# 4 @ 14

\$ SUMMARY OF COST \$

ITEM	QUANTITY	UNIT	UNIT PRICE	COST \$
CONCRETE	6.45	CU.YDS.	300.00	1934.95
REINFORCEMENT	749.19	LBS.	.95	711.73
SLAB FORM	60.13	SQ.FT.	8.00	481.00
CELL FORM	147.83	SQ.FT.	8.00	1182.67

TOTAL COST OF 5 CELL CULVERT \$4310.35

\*\*\*\*\*  
\*\*\* CULVERT DESIGN AND OPTIMIZATION - CUDO \*\*\*  
\*\*\*\*\*

INPUT ECHO

BR#A500 FILE A506LRF1.DAT 1 FT FILL

DESIGN CULVERT FOR GIVEN DIMENSIONS

GROUND ELEVATION 115.00 FT.  
CULVERT BOTTOM SLAB ELEVATION 100.00 FT  
WIDTH OF WATERWAY OPENING 60.00 FT.  
DEPTH OF WATERWAY OPENING 12.00 FT

COEF. OF ACTIVE EARTH PRESSURE .50

CONCENTRATED LOADS (KIPS) 16.00 16.00 4.00  
SPACING OF LOADS (FT.) 14.00 14.00

CONCRETE STRENGTH AT 28 DAYS (PSI) = 3000.0

PRICES			
CONCRETE	REINF.	WALL FORM	SLAB FORM
\$/CU.YDS	\$/LBS	\$/SQ.FT	\$/SQ.FT
300.00	.95	8.00	8.00

NUMBER OF CELLS 5

TOP SLAB THICKNESS 11.50 IN.  
BOTTOM SLAB THICKNESS 11.50 IN.  
EXTERIOR WALL THICKNESS 9.50 IN.  
INTERIOR WALL THICKNESS 8.00 IN.

ALL OPTIMUM DESIGN FOR GIVEN OPENING

NUMBER OF CELLS = 5

WATERWAY OPENING

WIDTH = 60.00 FT.

HEIGHT = 12.00 FT.

SPAN = 12.69 FT.

SLAB THICKNESS

TOP SLAB = 11.50 IN.

BOTTOM SLAB = 11.50 IN.

WALL THICKNESS

EXTERIOR = 9.50 IN.

INTERIOR = 8.00 IN.

NOTE: (\*\*)- AREA & SPACING OF POSITIVE REINFORCEMENT  
ARE BASED ON THE MAXIMUM MOMENT DUE TO DESIGN LOADING,  
1.2 TIMES CRACKING MOMENT OR CRACK CONTROL ( $Z = 98$ )

TOP SLAB - DETAILS FOR NEGATIVE MOMENT  
OUTSIDE FACE AT SUPPORT

LOCATION	MOMENT FT-KIPS	REQD. REINF.	SUGGESTED SPACING
SPAN 1 LEFT	-15.1	.40	# 4 @ 6
RIGHT	-16.8	.48	# 4 @ 5
SPAN 2 LEFT	-17.4	.48	# 4 @ 5
RIGHT	-13.7	.34	# 4 @ 7
SPAN 3 LEFT	-12.5	.34	# 4 @ 7
RIGHT	-12.5	.34	# 4 @ 7
SPAN 4 LEFT	-13.7	.34	# 4 @ 7
RIGHT	-17.4	.48	# 4 @ 5
SPAN 5 LEFT	-16.8	.48	# 4 @ 5
RIGHT	-15.1	.40	# 4 @ 6

TOP SLAB - DETAILS FOR POSITIVE MOMENT  
INSIDE FACE AT MID SPAN (\*\*)

LOCATION	MOMENT FT-KIPS	REQD. REINF.	SUGGESTED SPACING
SPAN 1	12.6	.48	# 4 @ 5
SPAN 2	12.6	.48	# 4 @ 5
SPAN 3	4.6	.40	# 4 @ 6
SPAN 4	12.6	.48	# 4 @ 5
SPAN 5	12.6	.48	# 4 @ 5

BOTTOM SLAB - DETAILS FOR NEGATIVE MOMENT

INSIDE FACE AT SUPPORT

LOCATION	MOMENT FT-KIPS	REQD. REINF.	SUGGESTED SPACING
SPAN 1 LEFT	-18.5	.60	# 4 @ 4
RIGHT	-18.4	.60	# 4 @ 4
SPAN 2 LEFT	-19.3	.60	# 4 @ 4
RIGHT	-15.8	.48	# 4 @ 5
SPAN 3 LEFT	-14.6	.48	# 4 @ 5
RIGHT	-14.6	.48	# 4 @ 5
SPAN 4 LEFT	-15.8	.48	# 4 @ 5
RIGHT	-19.3	.60	# 4 @ 4
SPAN 5 LEFT	-18.4	.60	# 4 @ 4
RIGHT	-18.5	.60	# 4 @ 4

BOTTOM SLAB - DETAILS FOR POSITIVE MOMENT  
INSIDE FACE AT MID SPAN (\*\*)

LOCATION	MOMENT FT-KIPS	REQD. REINF.	SUGGESTED SPACING
SPAN 1	13.2	.60	# 4 @ 4
SPAN 2	13.7	.60	# 4 @ 4
SPAN 3	5.6	.40	# 4 @ 6
SPAN 4	13.7	.60	# 4 @ 4
SPAN 5	13.2	.60	# 4 @ 4

EXTERIOR WALL DETAILS

LOCATION	MOMENT FT-KIPS	REQD. REINF.	SUGGESTED SPACING
OUTSIDE FACE			
BOTTOM	-18.5	.62	# 5 @ 6
TOP	-15.1	.60	# 4 @ 4
INSIDE FACE (**)			
	7.0	.48	# 4 @ 5

INTERIOR WALL DETAILS

LOCATION	MOMENT FT-KIPS	REQD. REINF.	SUGGESTED SPACING
EACH FACE	-1.4	.17	# 4 @ 14

\$ SUMMARY OF COST \$

ITEM	QUANTITY	UNIT	UNIT PRICE	COST \$
CONCRETE	6.45	CU.YDS.	300.00	1934.95
REINFORCEMENT	729.28	LBS.	.95	692.82
SLAB FORM	60.13	SQ.FT.	8.00	481.00
WALL FORM	147.83	SQ.FT.	8.00	1182.67

TOTAL COST OF 5 CELL CULVERT \$4291.44



15 13 JUL 98  
KSW 14 JULY 98

WINGHAVEN BEARING PRESSURES (MAX FILL) (MIN FILL)  
BRIDGE # A3210012 A3210013 A3210014 A3210015 A3210016 A3210012 A3210013 A3210014 A3210015 A3210016  
1 CELL 1 CELL 4 CELL 5 CELL 2 CELL 1 CELL 1 CELL 4 CELL 5 CELL 2 CELL

CULVERTP 13-Jul-98

	64000	64000	64000	64000	64000	64000	64000	64000	64000	64000
LIVE LOAD TWO HS20 AXLE	64000	64000	64000	64000	64000	64000	64000	64000	64000	64000
LBS PER SQ FT	57	57	44	31	43	92	92	60	47	96
LANE LOAD	64	64	64	64	64	64	64	64	64	64
FILL HEIGHT (FT)	5	5	4	6	8	1	1	1	1	1

CULVERT DIMENSIONS

NUMBER OF CELLS N =	1	1	4	5	2	1	1	4	5	2
OPENING WIDTH (FT) S =	10	10	12	12	8	10	10	12	12	8
OPENING HEIGHT (FT) H =	7	7	10	12	7	7	7	10	12	7
TOP SLAB THICK (IN) D1 =	11.5	11.5	11.5	11.5	10.5	11.5	11.5	11.5	11.5	10.5
BOTTOM SLAB THICK (IN) D2 =	11	11	12.5	11.5	9.5	11	11	12.5	11.5	9.5
EXTERIOR WALL THICK (IN) T =	8	8	8	8.5	7	8	8	8	8.5	7
INTERIOR WALL THICK (IN) TI =	0	0	8	7	6	0	0	8	7	6
TOTAL WIDTH (IN) C =	136	136	616	765	212	136	136	616	765	212
TOTAL WIDTH (FT) C =	11.333	11.333	51.333	63.750	17.667	11.333	11.333	51.333	63.750	17.667

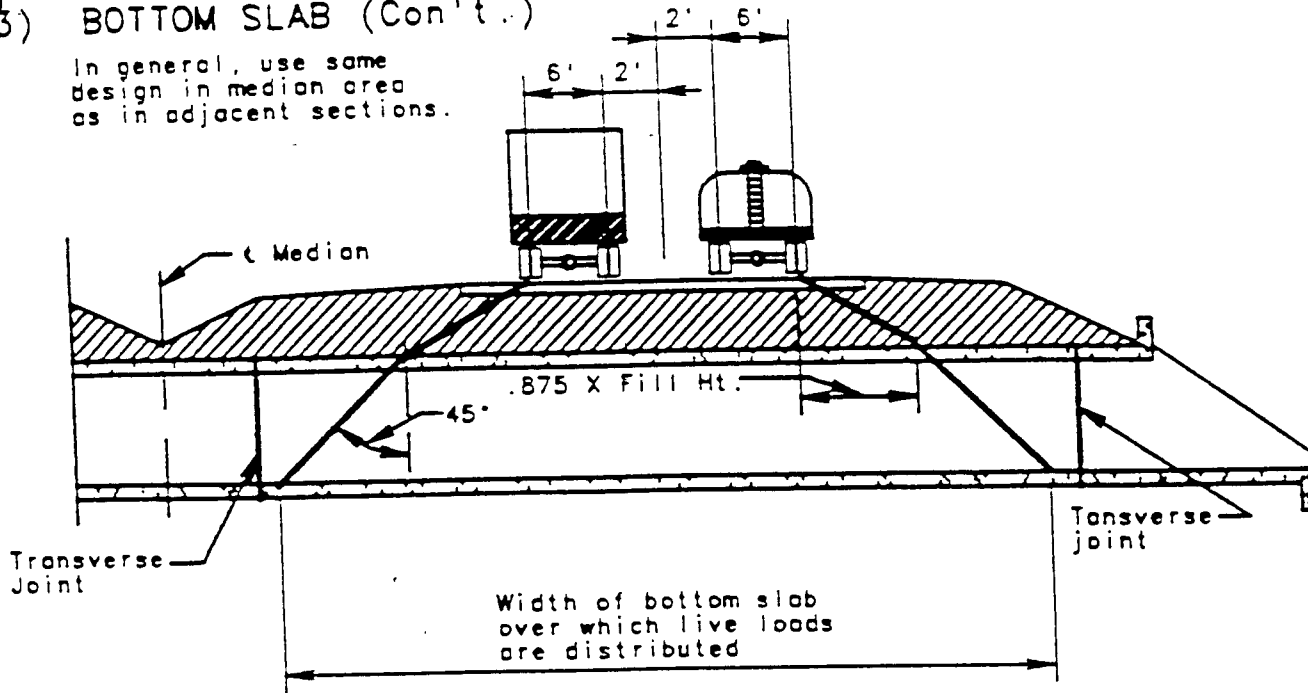
WEIGHT PER FT OF LENGTH

LIVE LOAD	64	64	64 ✓	64 ✓	64 ✓	92 ✓	92	64	64	96
FILL	600	600	480 ✓	720 ✓	960 ✓	120 ✓	120 ✓	120 ✓	120 ✓	120 ✓
CULVERT	405	405	397	393	349 ✓	405 ✓	405	397	393	349
TOTAL	1069	1069	941	1177	1373	617 ✓	617	581	577	565

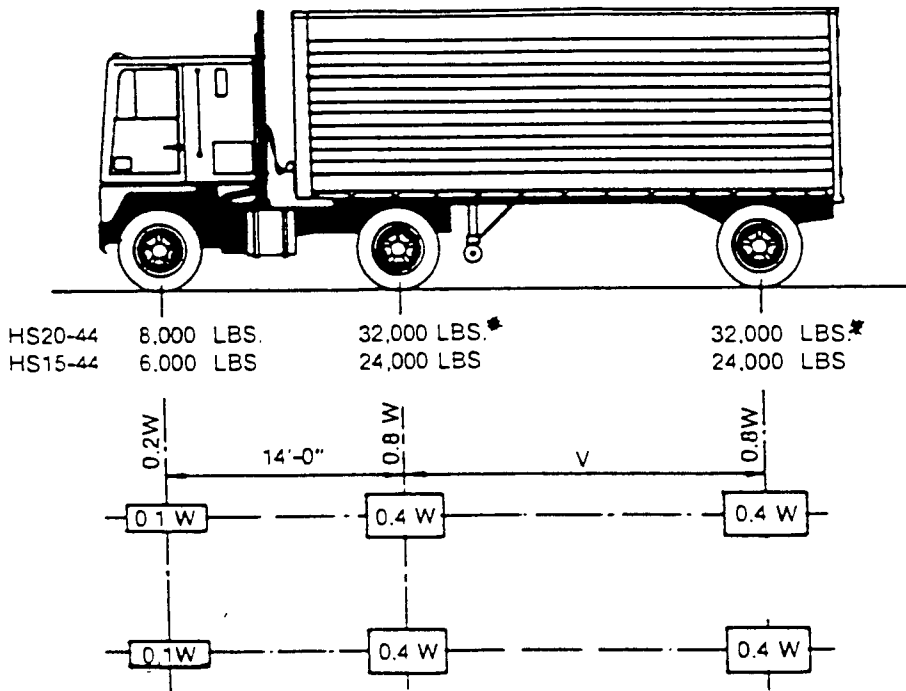
# DISTRIBUTION OF LOADS

## 3) BOTTOM SLAB (Con't.)

In general, use same design in median area as in adjacent sections.



LOADING CONDITION - INTERIOR SECTION OF BOXES WITH TRANSVERSE JOINTS



W = COMBINED WEIGHT ON THE FIRST TWO AXLES WHICH IS THE SAME AS FOR THE CORRESPONDING H. TRUCK.  
 V = VARIABLE SPACING — 14 FEET TO 30 FEET INCLUSIVE. SPACING TO BE USED IS THAT WHICH PRODUCES MAXIMUM STRESSES.

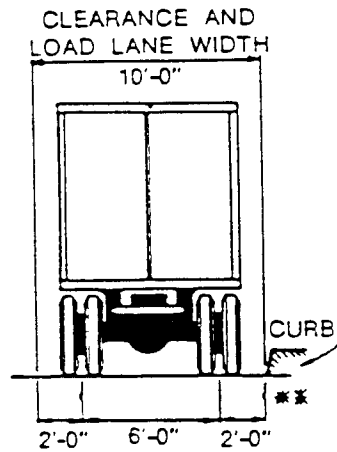
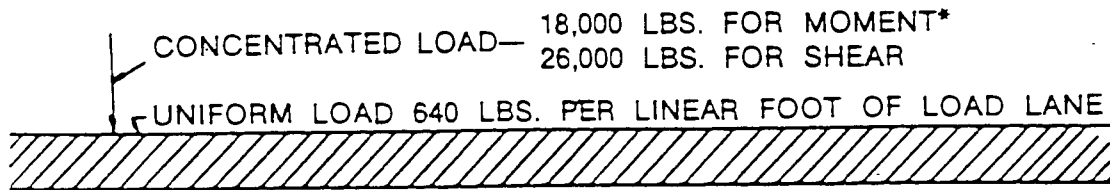


FIGURE 3.7.7A. Standard HS Trucks

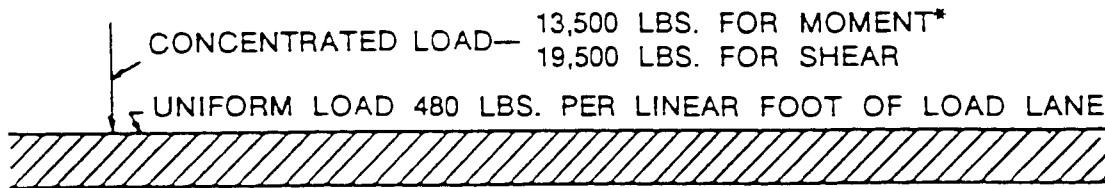
\*In the design of timber floors and orthotropic steel decks (excluding transverse beams) for H 20 loading, one axle load of 24,000 pounds or two axle loads of 16,000 pounds each, spaced 4 feet apart may be used, whichever produces the greater stress, instead of the 32,000-pound axle shown.

\*\*For slab design, the center line of wheels shall be assumed to be 1 foot from face of curb. (See Article 3.24.2.)





H20-44 LOADING  
HS20-44 LOADING



H15-44 LOADING  
HS15-44 LOADING

FIGURE 3.7.6B. Lane Loading

\*For the loading of continuous spans involving lane loading refer to Article 3.11.3 which provides for an additional concentrated load.

L = length in feet of the portion of the span that is loaded to produce the maximum stress in the member.

3.8.2.2 For uniformity of application, in this formula, the loaded length, L, shall be as follows:

- (a) For roadway floors: the design span length.
- (b) For transverse members, such as floor beams: the span length of member center to center of supports.
- (c) For computing truck load moments: the span length, or for cantilever arms the length from the moment center to the farthest axle.
- (d) For shear due to truck loads: the length of the loaded portion of span from the point under consideration to the far reaction; except, for cantilever arms, use a 30 percent impact factor.
- (e) For continuous spans: the length of span under consideration for positive moment, and the average of two adjacent loaded spans for negative moment.

3.8.2.3 For culverts with cover

0'0" to 1'-0" inc. I = 30%  
1'-1" to 2'-0" inc. I = 20%  
2'-1" to 2'-11" inc. I = 10%

### 3.9 LONGITUDINAL FORCES

Provision shall be made for the effect of a longitudinal force of 5 percent of the live load in all lanes carrying traffic headed in the same direction. All lanes shall be loaded for bridges likely to become one directional in the future. The load used, without impact, shall be the lane load plus the concentrated load for moment specified in Article 3.7, with reduction for multiple-loaded lanes as specified in Article 3.12. The center of gravity of the longitudinal force shall be assumed to be located 6 feet above the floor slab and to be transmitted to the substructure through the superstructure.

VS 13 JUL 98  
KSW 14 JULY 98

WINGHAVEN BEARING PRESSURES (MAX FILL) (MIN FILL)  
BRIDGE # A3210012 A3210013 A3210014 A3210015 A3210016 A3210012 A3210013 A3210014 A3210015 A3210016  
1 CELL 1 CELL 4 CELL 5 CELL 2 CELL 1 CELL 1 CELL 4 CELL 5 CELL 2 CELL

CULVERTP 13-JUL-98

LIVE LOAD	TWO HS20 AXLE	64000	64000	64000	64000	64000	64000	64000	64000	64000	64000
	LBS PER SQ FT	57	57	44	31	43	92	92	60	47	96
	LANE LOAD	64	64	64	64	64	64	64	64	64	64
FILL HEIGHT (FT)		5	5	4	6	8	1	1	1	1	1

CULVERT DIMENSIONS

NUMBER OF CELLS N =		1	1	4	5	2	1	1	4	5	2
OPENING WIDTH (FT) S =		10	10	12	12	8	10	10	12	12	8
OPENING HEIGHT (FT) H =		7	7	10	12	7	7	7	10	12	7
TOP SLAB THICK (IN) D1 =		11.5	11.5	11.5	11.5	10.5	11.5	11.5	11.5	11.5	10.5
BOTTOM SLAB THICK (IN) D2 =		11	11	12.5	11.5	9.5	11	11	12.5	11.5	9.5
EXTERIOR WALL THICK (IN) T =		8	8	8	8.5	7	8	8	8	8.5	7
INTERIOR WALL THICK (IN) TI =		0	0	8	7	6	0	0	8	7	6
TOTAL WIDTH(IN) C =		136	136	616	765	212	136	136	616	765	212
TOTAL WIDTH(FT) C =		11.333	11.333	51.333	63.750	17.667	11.333	11.333	51.333	63.750	17.667

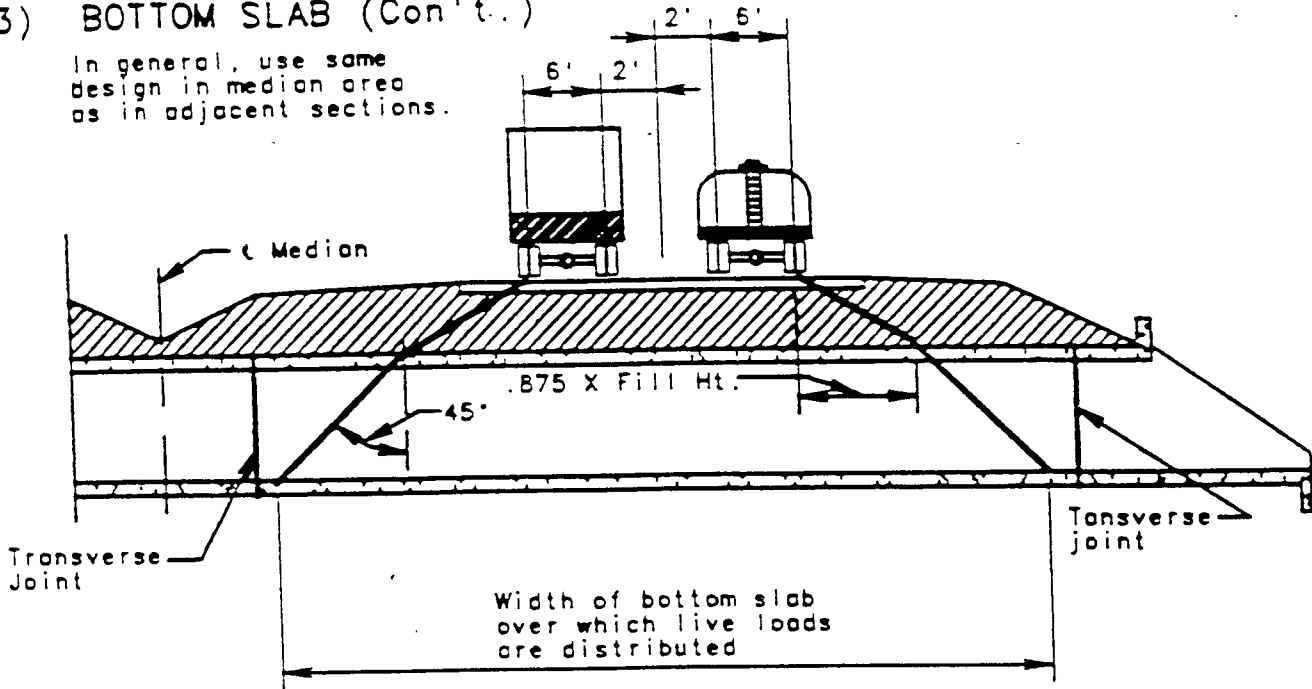
WEIGHT PER FT OF LENGTH

LIVE LOAD		64	64	64 ✓	64 ✓	64 ✓	92 ✓	92	64	64	96
FILL		600	600	480 ✓	720 ✓	960 ✓	120 ✓	120 ✓	120 ✓	120 ✓	120 ✓
CULVERT		405	405	397	393	349 ✓	405 ✓	405	397	393	349
TOTAL	LBS PER SQ FT	1069	1069	941	1177	1373	617 ✓	617	581	577	565

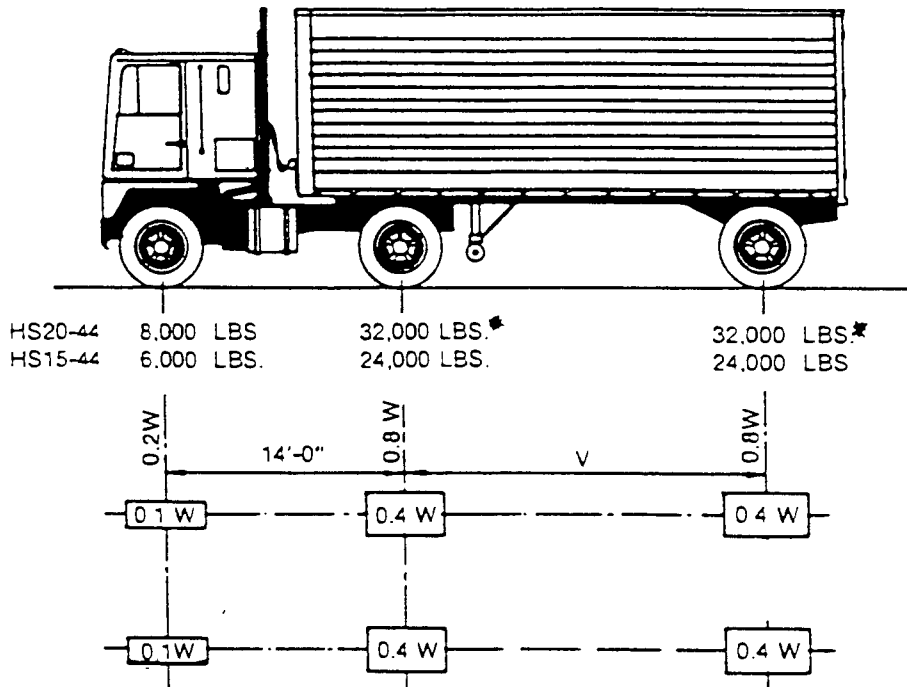
# DISTRIBUTION OF LOADS

## 3) BOTTOM SLAB (Con't..)

In general, use same design in median area as in adjacent sections.



LOADING CONDITION - INTERIOR SECTION OF BOXES WITH TRANSVERSE JOINTS



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 V = VARIABLE SPACING — 14 FEET TO 30 FEET INCLUSIVE. SPACING TO BE USED IS THAT WHICH PRODUCES MAXIMUM STRESSES.

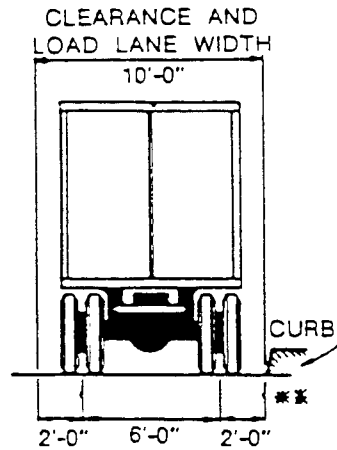
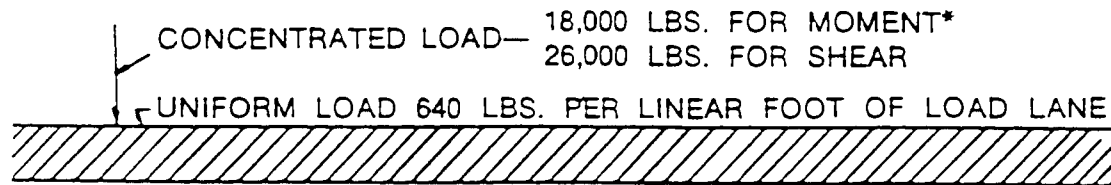


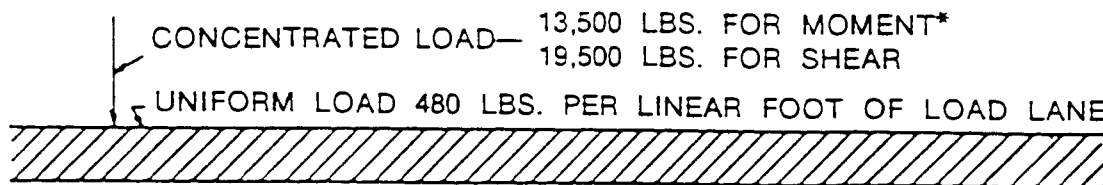
FIGURE 3.7.7A. Standard HS Trucks

\*In the design of timber floors and orthotropic steel decks (excluding transverse beams) for H 20 loading, one axle load of 24,000 pounds or two axle loads of 16,000 pounds each, spaced 4 feet apart may be used, whichever produces the greater stress, instead of the 32,000-pound axle shown.

\*\*For slab design, the center line of wheels shall be assumed to be 1 foot from face of curb. (See Article 3.24.2.)



H20-44 LOADING  
HS20-44 LOADING



H15-44 LOADING  
HS15-44 LOADING

FIGURE 3.7.6B. Lane Loading

\*For the loading of continuous spans involving lane loading refer to Article 3.11.3 which provides for an additional concentrated load

L = length in feet of the portion of the span that is loaded to produce the maximum stress in the member.

3.8.2.2 For uniformity of application, in this formula, the loaded length, L, shall be as follows:

- (a) For roadway floors: the design span length.
- (b) For transverse members, such as floor beams: the span length of member center to center of supports.
- (c) For computing truck load moments: the span length, or for cantilever arms the length from the moment center to the farthest axle.
- (d) For shear due to truck loads: the length of the loaded portion of span from the point under consideration to the far reaction; except, for cantilever arms, use a 30 percent impact factor.
- (e) For continuous spans: the length of span under consideration for positive moment, and the average of two adjacent loaded spans for negative moment.

3.8.2.3 For culverts with cover

0'0" to 1'-0" inc. I = 30%  
1'-1" to 2'-0" inc. I = 20%  
2'-1" to 2'-11" inc. I = 10%

### 3.9 LONGITUDINAL FORCES

Provision shall be made for the effect of a longitudinal force of 5 percent of the live load in all lanes carrying traffic headed in the same direction. All lanes shall be loaded for bridges likely to become one directional in the future. The load used, without impact, shall be the lane load plus the concentrated load for moment specified in Article 3.7, with reduction for multiple-loaded lanes as specified in Article 3.12. The center of gravity of the longitudinal force shall be assumed to be located 6 feet above the floor slab and to be transmitted to the substructure through the superstructure.

WYOMING DEPARTMENT OF TRANSPORTATION  
Program for the Design of Reinforced  
Concrete Box Culverts

BRASS - CULVERT

Version 1

User Manual  
January, 1995

BRASS-CULVERT		COMMAND DESCRIPTION										
COMMAND NAME	STDLOD											
PURPOSE	STDLOD defines the standard truck loads to be used.											
<b>5 COMMAND PARAMETERS</b>												
2 Truck Code (1-8)	<p>Enter the code for the desired truck load to be applied. The codes are:</p> <table border="0"> <tr> <td>1) HS 25</td> <td>6) HS 10</td> </tr> <tr> <td>2) HS 20</td> <td>7) H 10</td> </tr> <tr> <td>3) H 20</td> <td>8) Special Live Load Only</td> </tr> <tr> <td>4) HS 15</td> <td>9) No Live Load</td> </tr> <tr> <td>5) H 15</td> <td></td> </tr> </table> <p>Special live loads are defined with the SPLLOD command.</p>		1) HS 25	6) HS 10	2) HS 20	7) H 10	3) H 20	8) Special Live Load Only	4) HS 15	9) No Live Load	5) H 15	
1) HS 25	6) HS 10											
2) HS 20	7) H 10											
3) H 20	8) Special Live Load Only											
4) HS 15	9) No Live Load											
5) H 15												
1 Check Military Load (0,1)	<p>When HS 25 or HS 20 truck loading is specified, the standard military load in two adjacent lanes will be checked if specified here. Enter 1 to check military load as a separate load case, else enter 0.</p>											
0 Neglect Live Load (0,1)	<p>Live load may be neglected for single culverts if fill depth is more than 8 feet and exceeds barrel span length. For multiple culverts, it may be neglected if fill depth exceeds the distance between end supports or abutments. (See AASHTO 6.4.2.)</p> <p>Enter 1 to neglect live load according to AASHTO 6.4.2.</p> <p>Enter 0 to use live load regardless of fill height.</p>											
0 Stress at Zero Fill (0,1)	<p>Enter 1 for stress check at zero fill (top of top slab) to be performed, else enter 0.</p>											
0 Overload Axle Weight, kip	<p>Enter the axle weight for the overload standard truck, kips.</p>											

## EXAMPLE

To define an HS 25 truck load to be applied to the culvert with live load distribution based on AASHTO 6.4.2, no stress check at zero fill or overload truck effects to be calculated, and military load will not be checked as a separate load case, code:

STDLOD 1, 0, 0, 0, 0

## FIGURES

## NOTES



BRASS-CULVERT		COMMAND DESCRIPTION
COMMAND NAME	SWPRES	
PURPOSE	SWPRES defines soil and water pressure parameters.	
5 COMMAND PARAMETERS		
1 Structure Number (1-10)	Enter the reference number for the culvert to be described by the following data. Culverts must be numbered sequentially beginning with 1, 2, 3 ...etc.	
2 Live Load Surcharge, ft.	Enter the depth of surcharge to be used for calculating the effects of lateral earth pressure. Surcharge load is applied as a uniform load on the exterior walls and is calculated as the depth of surcharge times the maximum or minimum soil pressure as applicable.	
45 Maximum Soil Pressure, pcf	Enter the maximum soil equivalent fluid pressure for lateral earth pressure calculations. Standard maximum is 30 pcf by AASHTO 6.2.1.	
15 Minimum Soil Pressure, pcf	Enter the minimum soil equivalent fluid pressure for lateral earth pressure calculations. A minimum of 15 pcf is used for checking positive moments unless otherwise defined.	
62.4 Water Pressure, pcf	Enter the unit weight of water (62.4 pcf standard). Enter 0 for no water pressure to be considered. When considered, BRASS-CULVERT uses full height of water and no water as two loading cases.	

EXAMPLE

For standard values:

SWPRES 1, 2.0, 30.0, 15.0, 62.4

FIGURES

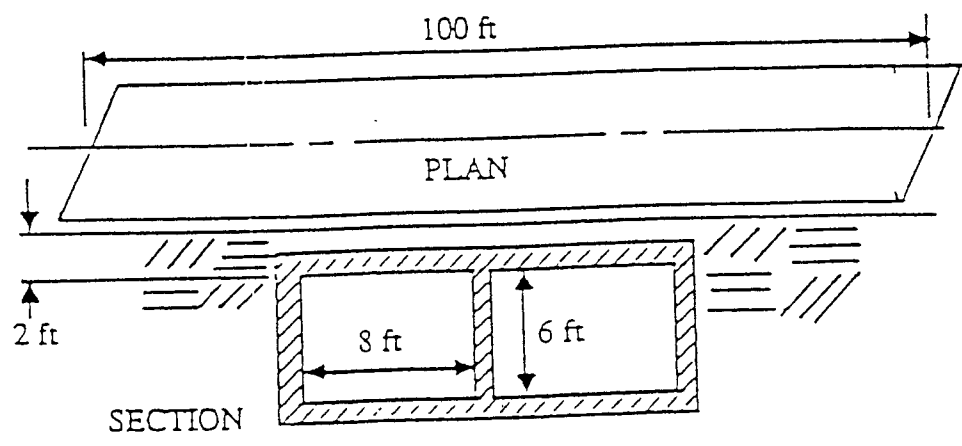
NOTES

BRASS-CULVERT		COMMAND DESCRIPTION
COMMAND NAME	BOXDIM	
PURPOSE	BOXDIM defines the geometry of the box culvert.	
6 COMMAND PARAMETERS		
1 Structure Number (1-10)	Enter the reference number for the culvert to be described by the following data. Culverts must be numbered sequentially beginning with 1, 2, 3 ...etc.	
1, 1, 2, 4, 5 Number of Barrels (1-4)	Enter the number of barrels for the culvert, four maximum.	
10, 10, 8, 12, 12 Clear Span, ft.	Enter the clear span of the barrels, feet. All barrels have the same span.	
7, 7, 10, 12 Clear Height, ft.	Enter the clear height of the barrels, feet. All barrels have the same height.	
4, 10, 8, 8, 6 Design Fill, ft.	Enter the depth of fill to be used for design. Fill is measured from the bottom of the top slab to the top of fill, feet. Live loads will be applied to the top of this fill.	
30, 105, 108, 150, 78 Centerline Length, ft.	Enter the length of the culvert along its centerline, feet.	

EXAMPLE

BOXDIM 1, 2, 8, 6, 2, 100

FIGURES



NOTES

BRASS-CULVERT		COMMAND DESCRIPTION
COMMAND NAME	SLBTHK	
PURPOSE	SLBTHK defines the thickness for the top and bottom slabs, and the exterior and interior walls.	
6 COMMAND PARAMETERS		
1	Structure Number (1-10)	Enter the reference number for the culvert to be defined by the following data. Culverts must be numbered sequentially beginning with 1, 2, 3 ...etc.
6	Top Slab Thickness, in.	Enter the thickness for the top slab. Unless this value is specified as fixed value (see below), BRASS-CULVERT uses this value as minimum thickness.
6	Bottom Slab Thickness, in.	Enter the thickness for the bottom slab. Unless this value is specified as fixed value (see below), BRASS-CULVERT uses this value as minimum thickness.
6	Exterior Wall Thickness, in.	Enter the thickness for the exterior wall. Unless this value is specified as fixed value (see below), BRASS-CULVERT uses this value as minimum thickness.
6	Interior Wall Thickness, in.	Enter the thickness for the interior wall. Unless this value is specified as fixed value (see below), BRASS-CULVERT uses this value as minimum thickness.
0000	Fixed Thickness Code (0 - 1111)	BRASS-CULVERT will use the thicknesses defined above as minimum values unless otherwise specified here. Each digit of the code is for the top slab, bottom slab, exterior walls, and interior walls respectively. Enter 1 to fix the thickness, else enter 0. For example to fix the top slab and exterior wall thicknesses only, enter a code of 1010.

## EXAMPLE

For a culvert with a fixed slab and wall thickness of 7 inches, code:

SLBTHK 1, 7, 7, 7, 7, 1111

For a culvert with a fixed top slab of 8 inches and fixed exterior walls of 10 inches, bottom slab and interior wall thicknesses are used as minimum values, code:

SLBTHK 1, 8, 8, 10, 10, 1010

For a culvert with no fixed thicknesses and it is desired for the program to set the thicknesses as required, code:

SLBTHK 1, 0, 0, 0, 0, 0000

## FIGURES

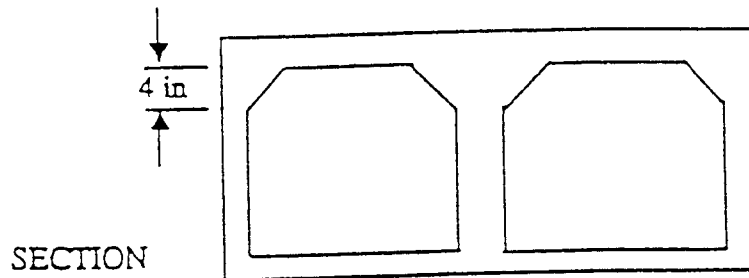
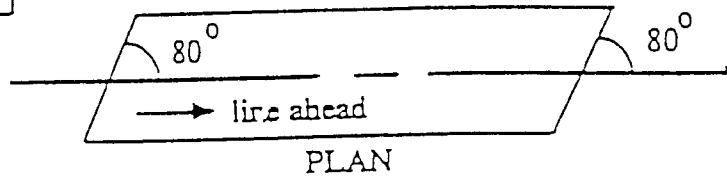
## NOTES

BRASS-CULVERT		COMMAND DESCRIPTION
COMMAND NAME	H&SKEW	
PURPOSE	H&SKEW defines haunches and end skews.	
6 COMMAND PARAMETERS		
1 Structure Number (1-10)	Enter the reference number for the culvert to be described by the following data. Culverts must be numbered sequentially beginning with 1, 2, 3 ...etc.	
90 Skew Angle Left, deg.	Enter the skew angle at the left end of the culvert, degrees. See Note.	
90 Skew Angle Right, deg.	Enter the skew angle at the right end of the culvert, degrees. See Note.	
0 Top Haunch Height, in.	Enter the height of the top haunch, inches. Enter 0 for no top haunch.	
0 Bottom Haunch Height, in.	Enter the height of the bottom haunch, inches. Enter 0 for no bottom haunch.	
0 Haunches by AASHTO 0 or 1	Enter 1 for haunches to be considered in effective span length calculations, as per AASHTO Section 8.8, else enter 0.	

EXAMPLE

H&SKEW 80, 80, 4, 0, 1

FIGURES



NOTES

Skew angles are measured from line ahead to skew as shown above. Positive angles only.



BRASS-CULVERT		COMMAND DESCRIPTION
COMMAND NAME	REEBAR	
PURPOSE	REEBAR defines allowable bar sizes and spacings, and maximum steel ratio.	
6 COMMAND PARAMETERS		
12 Maximum Bar Spacing, in. Default = 12	Enter the maximum allowable bar spacing.	
9 Minimum Bar Spacing, in. Default = 12	Enter the minimum allowable bar spacing.	
1 Bar Spacing Increment (0,1)	Steel design bar spacings will be rounded to the increment defined here. Enter 1 to round spacings to 1 inch increments, or enter 0 to round bar spacings to 1/2 inch increments.	
11 Maximum Bar Size (#) Default = 11	Enter the maximum bar size to be used in design.	
4 Minimum Bar Size (#) Default = 4	Enter the minimum bar size to be used in design.	
.016 Maximum Steel Ratio Default = 0.012	Enter the maximum ratio of area of steel to area for concrete ( $A_s / bd$ ) in decimal form.  $p_{max} = .75 p_b = \frac{.85(.85)3000}{60000} \left( \frac{87000}{87000 + 60000} \right)$ $= .016$	

EXAMPLE

For a culvert with a maximum bar spacing of 12 inches, a minimum bar spacing of 4 inches, bar spacing increments of 1/2 inch, a maximum bar size of #11, a minimum bar size of #4, and a maximum reinforcement ratio of 0.012, code:

REEBAR 12, 4, 0, 4, 0.012  
12 0.016

FIGURES

NOTES

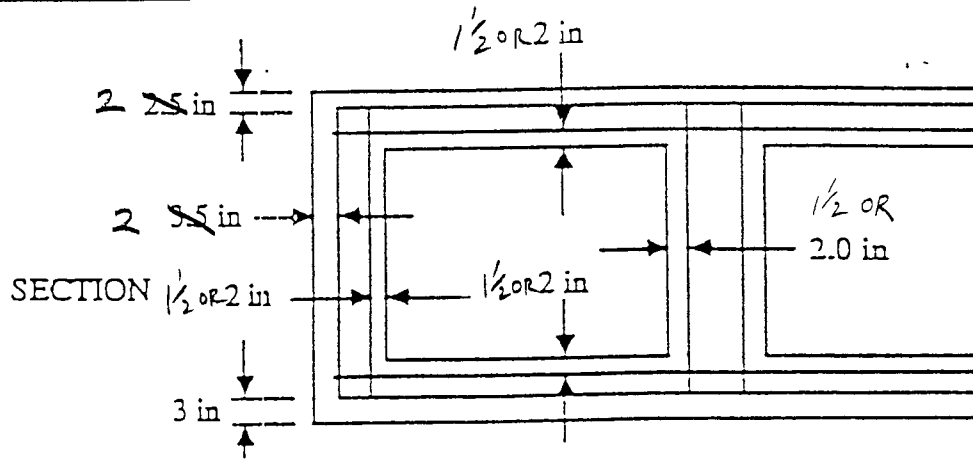
BRASS-CULVERT		COMMAND DESCRIPTION
COMMAND NAME	CONCOV	
PURPOSE	CONCOV defines the depth of concrete cover for reinforcement and the slab thickness round off increment.	
6 COMMAND PARAMETERS		
2	Exterior Top Slab, in.	Enter the distance from the face of steel bars to the face of concrete for the top steel of the top slab, inches. See Note.
3	Exterior Bottom Slab, in.	Enter the distance from the face of steel bars to the face of concrete for the bottom steel of the bottom slab, inches. See Note.
2	Exterior Wall, in.	Enter the distance from the face of steel bars to the exterior face of the exterior walls, inches. See Note.
HYDR (2), 2	GOLF Interior Cover, in.	Enter the distance from the face of steel bars to the face of concrete for the interior faces of slabs and walls, inches. See Note.  NOTE: Default values are 3 inches for bottom slab cover and 2 inches for all other covers.
1/2	Slab Thickness Increment, in.	BRASS-CULVERT "rounds up" slab thickness to the nearest increment defined. Default values are 1/2 inch.
1/2	Wall Thickness Increment, in.	BRASS-CULVERT "rounds up" wall thickness to the nearest increment defined. Default values are 1/2 inch.

EXAMPLE

2.0 2.0  
CONCOV ~~2.5~~, 3.0, ~~3.5~~, 2.0, 0.5, 0.5

HYDR → 1.5  
ONLY

FIGURES



NOTES

All covers are measured from the outer face of steel to face of slab.

BRASS-CULVERT		COMMAND DESCRIPTION
COMMAND NAME	MATPRP	
PURPOSE	MATPRP defines material properties for steel and concrete.	
6 COMMAND PARAMETERS		
120 Soil Unit Weight, pcf	Enter the unit weight of the soil fill in pounds per cubic foot. BRASS-CULVERT uses 100% of soil weight for both rigid and flexible box designs.	
60 Reinforcing Yield, Fy, ksi	Enter the yield strength for steel reinforcement, ksi.	
24 Allowable Steel Stress, ksi	Enter the allowable steel stress, ksi.	
3 Concrete Strength, ksi	Enter the 28 day compressive strength for concrete, ksi.	
0 Allowable Concrete Shear, ksi	Enter the allowable concrete shear stress, ksi. Enter 0 for BRASS-CULVERT to calculate the concrete shear strength according to AASHTO 8.16.	
0 Allowable Concrete Shear, with Stirrups, ksi	Enter the allowable concrete shear stress when stirrups are used. <u>Enter 0 for no stirrups.</u>	

## EXAMPLE

For a culvert with a soil unit weight of 120 pcf, 40 ksi reinforcing steel, an allowable steel stress of 20 ksi, a concrete strength of 3000 psi, and to have the program calculate the allowable concrete shear stress, code:

MATPRP 120, 40, 20, 3, 0, 0

60 24

## FIGURES

## NOTES

BRASS-CULVERT		COMMAND DESCRIPTION
COMMAND NAME	PRTCTL	
PURPOSE	PRTCTL controls the output produced.	
4 COMMAND PARAMETERS		
0	1	Bar Schedule (0,1) Enter 1 for printing the bar schedule, <u>else enter 0.</u>
0	1	Tenth Point Actions (0,1) Enter <u>1 for printing moments</u> , shears, and axial forces at tenth points, <u>else enter 0.</u> These are factored actions for ultimate strength design.
0	1	Influence Lines (0,1) Enter 1 for printing live load influence line ordinates at tenth points, <u>else enter 0.</u>
0	0	Debug Printout (0,1) This parameter is to be used for debugging purposes only. Enter 1 for special printout of dead load, soil pressure, and live load moments and shears, <u>else enter 0.</u> These are unfactored actions for ultimate strength design.

↑  
FINAL  
RUN

EXAMPLE

To print the bar schedule, tenth point actions, and influence line ordinates, code:

```
PRTCTL 1, 1, 1, 0  
      0 0 0
```

FIGURES

NOTES



BRASS-CULVERT		COMMAND DESCRIPTION
COMMAND NAME	F&HCTL	
PURPOSE	F&HCTL defines floor type and headwall configuration.	
3 COMMAND PARAMETERS		
1 Structure Number (1-10)	Enter the reference number for the culvert to be described by the following data. Culverts must be numbered sequentially beginning with 1, 2, 3 ...etc.	
1 Floor Type (1,2,3)	Enter <u>1</u> for full floor. Enter 2 for no floor with fixed end supports. Enter 3 for no floor with pinned end supports.	
2 Headwall Steel (0-3)	Enter 0 to generate headwall steel as per North Carolina standard. Enter 1 to suppress headwall steel generation. Enter <u>2</u> to generate left headwall steel only. Enter 3 to generate right headwall steel only.	

EXAMPLE

To suppress a full floor and headwall steel design, code:

F&HCTL 1, 1, ~~2~~  
2

FIGURES

NOTES

BRASS-CULVERT		COMMAND DESCRIPTION
COMMAND NAME	DESCTL	
PURPOSE	DESCTL defines design control parameters.	
6 COMMAND PARAMETERS		
0, 1 Design Method (0,1)	Enter 0 for service load design method, or enter 1 for load factor design method.	
1, 0 Rigid or Flexible (0,1)	Enter 0 for rigid box culvert design, else enter 1 for flexible box culvert design.	
0 Design Negative Moment Position (0.0 - 1.0)	The position of design negative moment is defined by a value from zero to one where <u>0.0 represents the centerline of the wall or slab</u> , 0.5 represents half way between center of the wall or slab and face of the wall or slab, and 1.0 represents the face of the wall or slab.	
0 Design Same Slabs (0,1)	Enter 1 for BRASS-CULVERT to design the same thicknesses and steel for top and bottom slabs, <u>else enter 0</u> . See Note.	
0 Design Same Walls (0,1)	Enter 1 for BRASS-CULVERT to design the same exterior and interior wall thicknesses, <u>else enter 0</u> . See Note.	
9 Modular Ratio (N) Default = 9	Enter the ratio of the modules of elasticity of steel to that of concrete.	

# QUANTITIES

CONCRETE QUANTITIES

DESCRIPTION	QUANT.	WIDTH	LENGTH	DEPTH	FACTOR	TOTAL (CU. FT.)	TOTAL (CU. YD.)
TOP SLAB	1.00	64.25	89.00	0.96	1.00	5479.99	202.96
EXTERIOR WALL	2.00	0.79	89.00	12.00	1.00	1691.00	62.63
INTERIOR WALL	4.00	0.67	89.00	12.00	1.00	2848.00	105.48
BOTTOM SLAB	1.00	64.25	160.00	0.96	1.00	9851.67	364.88
BOTTOM SLAB TRIANGLE	0.00	0.00	0.00	0.00	0.00	0.00	0.00
HEADWALL	2.00	64.25	1.50	0.50	1.00	96.38	3.57
CUT OFF WALL DOWNSTREAM	1.00	64.25	0.83	2.04	1.00	109.31	4.05
CUT OFF WALL UPSTREAM	1.00	64.25	0.83	1.04	1.00	55.77	2.07
INT WING DOWNSTREAM	4.00	0.67	35.50	12.96	1.00	1226.72	45.43
INT WING DOWNSTREAM DEDUCT	4.00	0.67	35.25	11.96	-0.50	-562.04	-20.82
EXT WING DOWNSTREAM	2.00	0.79	35.50	12.96	1.00	728.37	26.98
EXT. WING DOWNSTREAM DEDUCT	2.00	0.79	35.25	11.96	-0.50	-333.71	-12.36
INT WING UPSTREAM	4.00	0.67	35.50	12.96	1.00	1226.72	45.43
INT. WING UPSTREAM DEDUCT	4.00	0.67	35.25	11.96	-0.50	-562.04	-20.82
EXT. WING UPSTREAM	2.00	0.79	35.50	12.96	1.00	728.37	26.98
EXT. WING UPSTREAM DEDUCT	2.00	0.79	35.25	11.96	-0.50	-333.71	-12.36
						22250.79	824.10
EXCAVATION	1.00	67.25	160.00	17.92	1.00	192783.33	7140.12

# SPECIFICATIONS

See Plan Sheets